

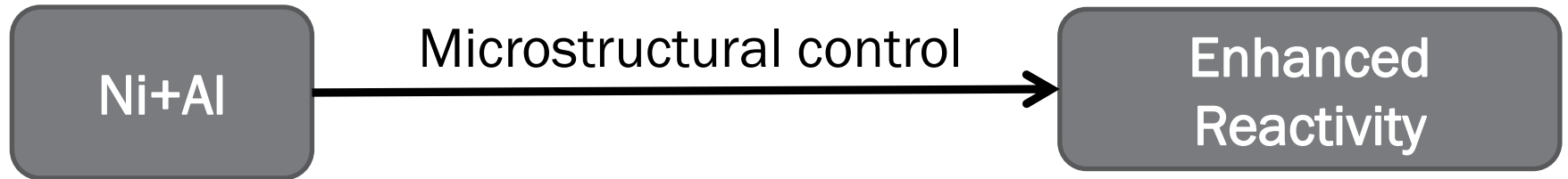
***INFLUENCE OF HIGH ENERGY BALL  
MILLING ON REACTIVITY IN NI-AL  
GASLESS HETEROGENEOUS SYSTEM***



# Motivation of the Research

Reactive exothermic mixtures of **nickel and aluminum** may be applied for

- chemical energy storage,
- nano-scale energetic devices
- materials synthesis and other applications

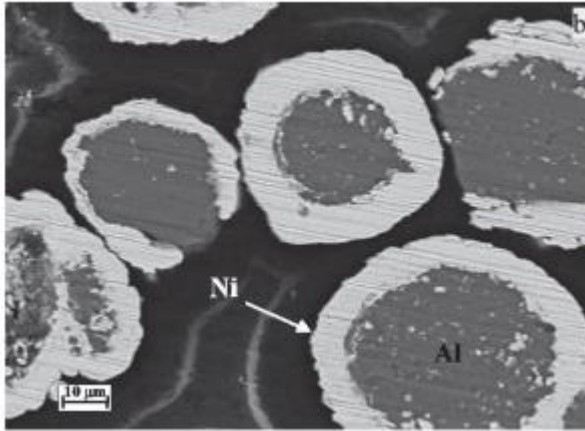


Microstructural control

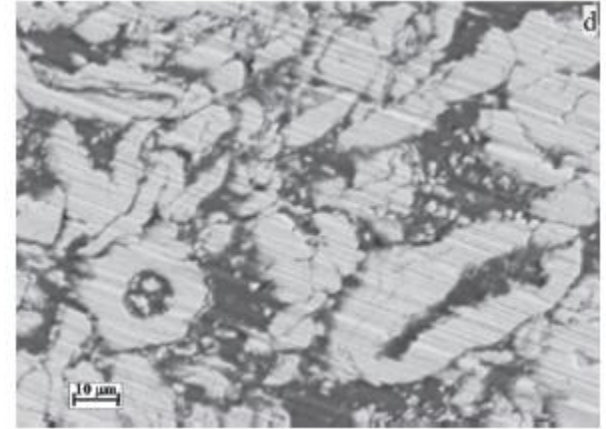
- high energy ball milling (HEBM)
- production of multilayer nano-foils, etc

**Ignition temperature ( $T_{ig}$ )** - the lowest ambient temperature at which the self-propagating reaction initiates.

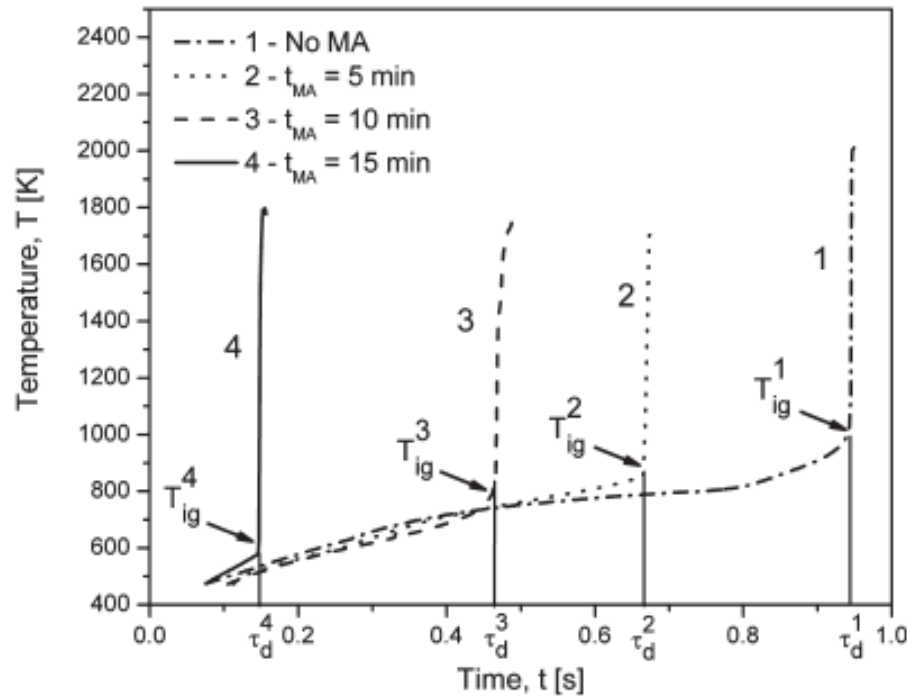
# Effect of HEBM on the reactivity of Ni-Al system



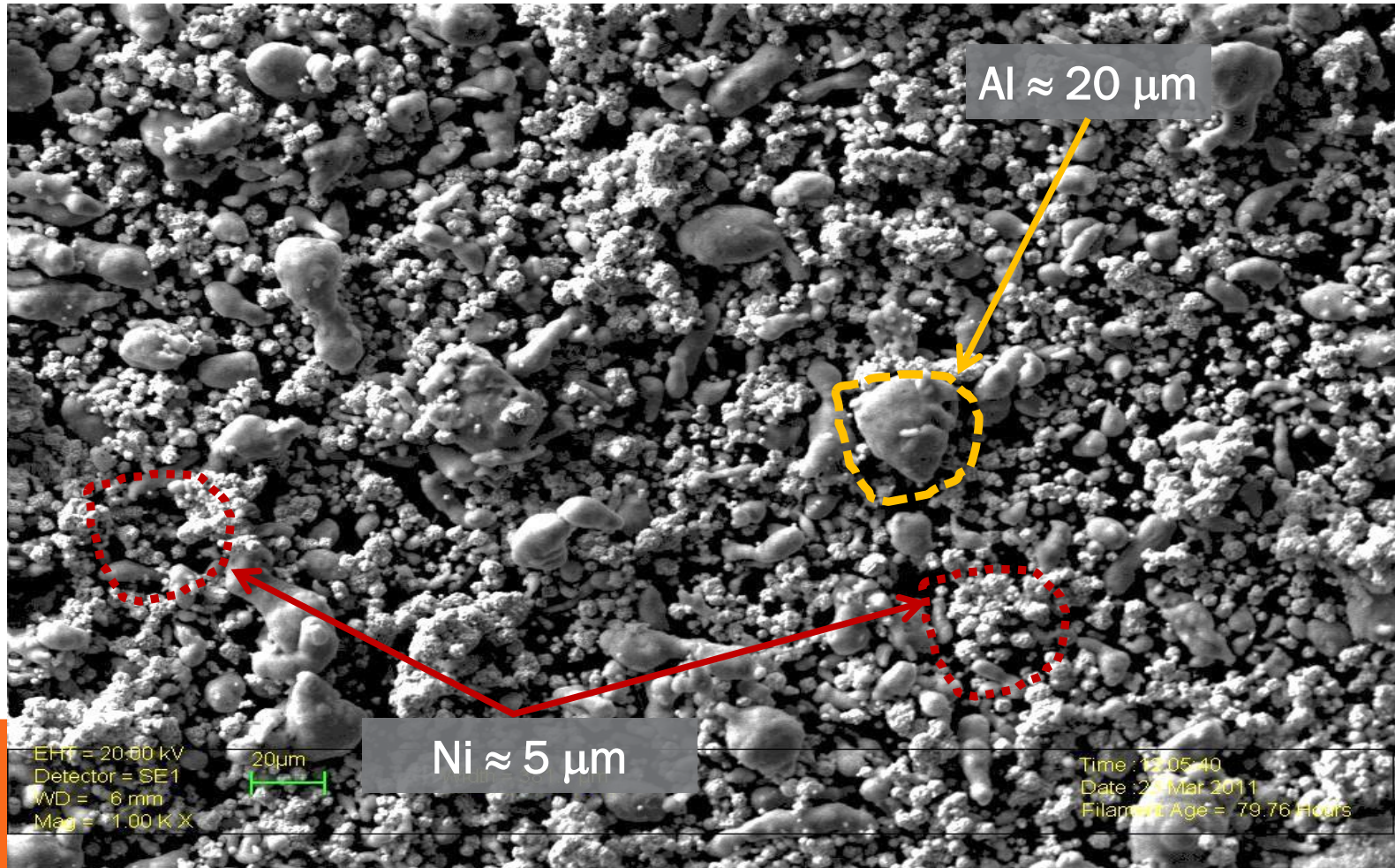
Ni-Al clad particles



Ball milled material



# Initial Ni + Al mixture



# High-Energy Ball Milling

## Milling conditions

Planetary mill	Retsch P100
Stainless steel vial	250ml
Ball / powder ratio	5:1
Ball (stainless steel) size	10 mm
Total wt. of ball during milling	170g
Rotational speed	300 rpm
Environment	argon

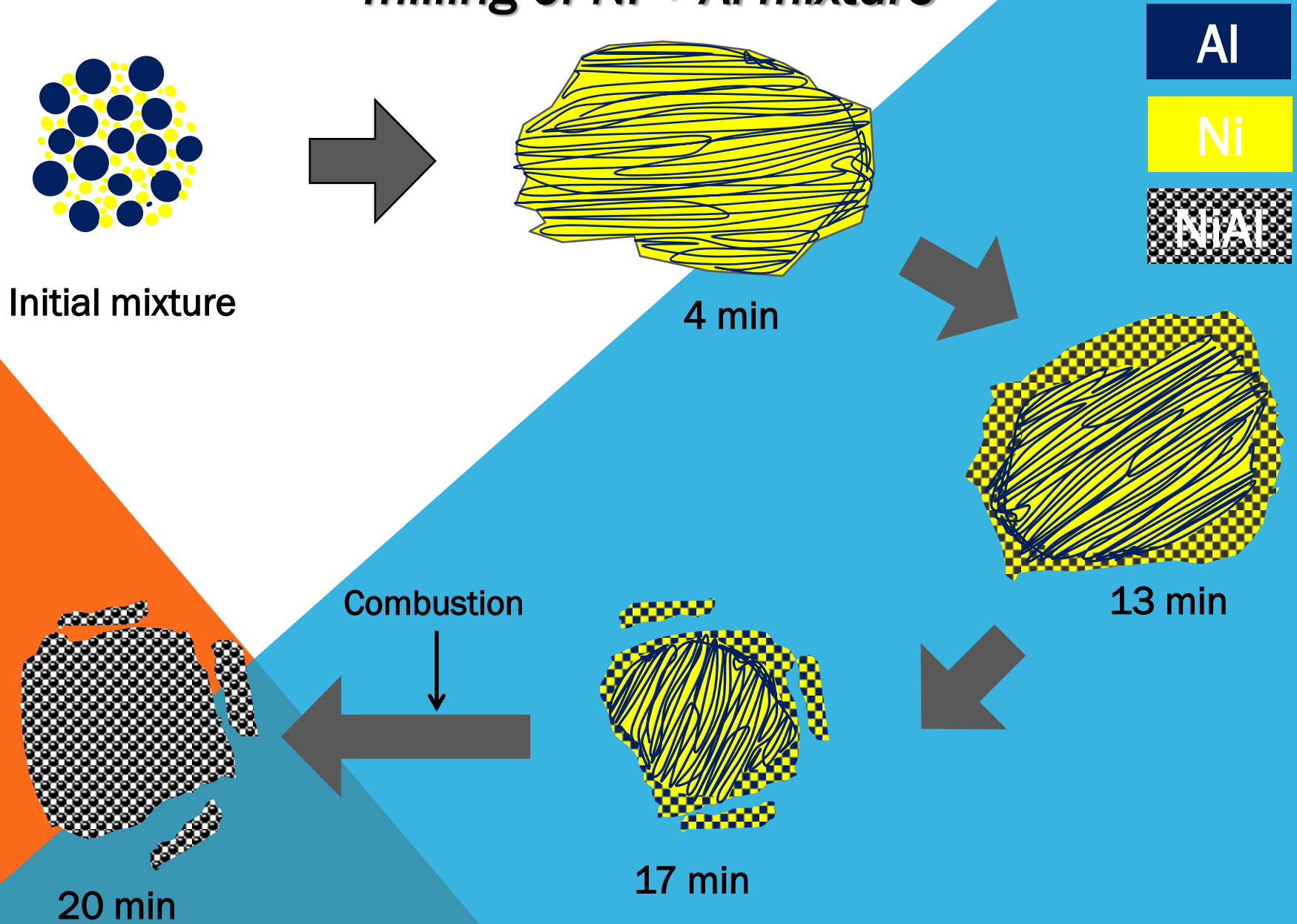


	Time, min					
Dry Milling	0	4	8	13	17	20 (Reacted)
Dry + Wet Milling	0 + 10	4 + 10	4 + 10	13 + 10	17 + 10	
Process controlling agent – Hexane						

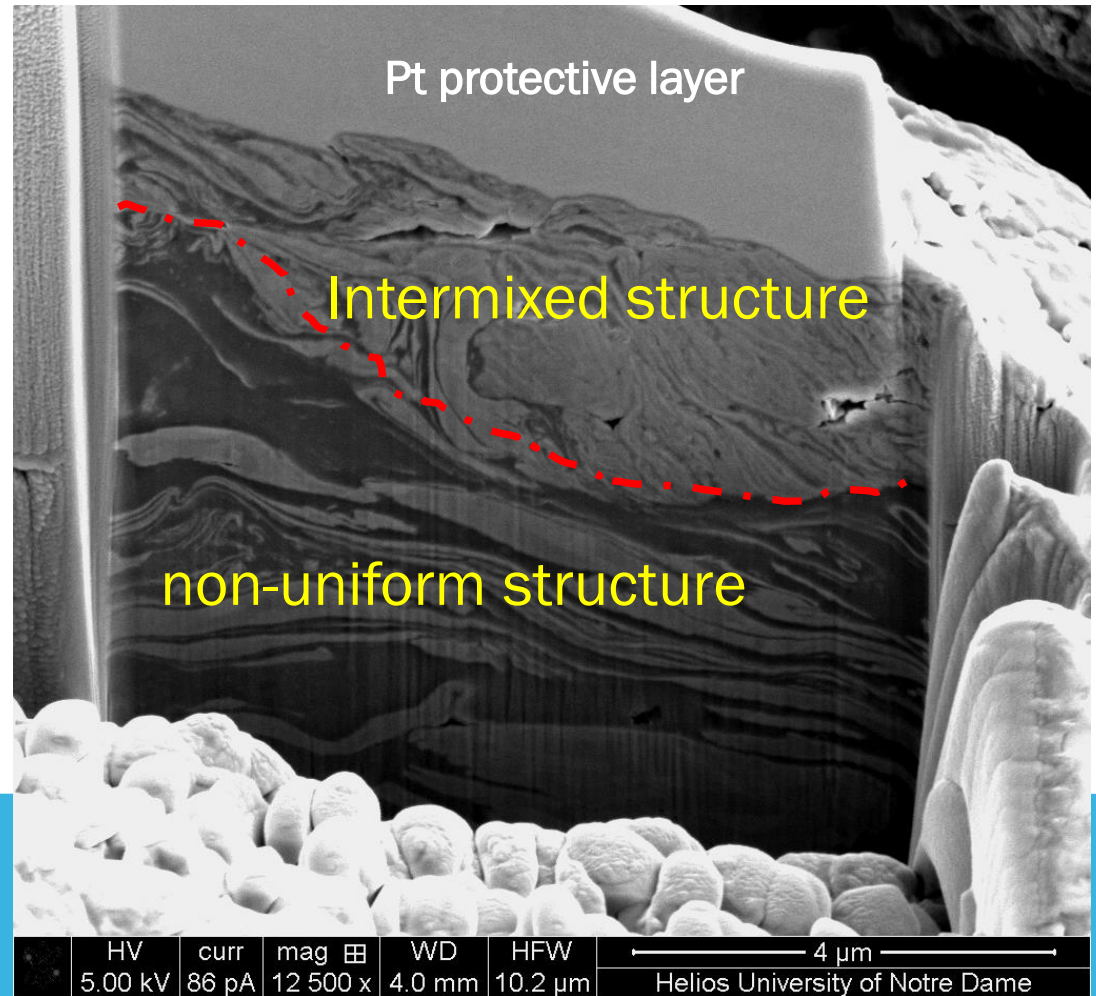


***Microstructural transformations in Ni + Al  
mechanically treated mixtures***

# Structural transformation during the Dry ball milling of Ni + Al mixture



# Two microstructures in Dry Ball Milled materials





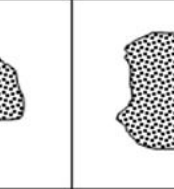
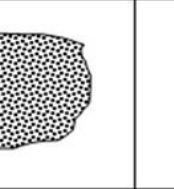




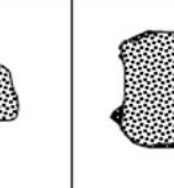
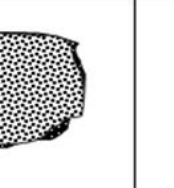


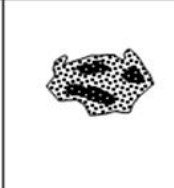

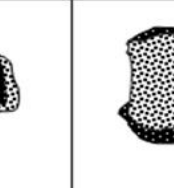
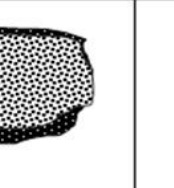




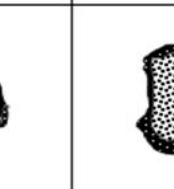
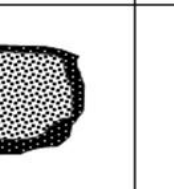



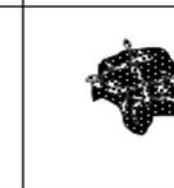
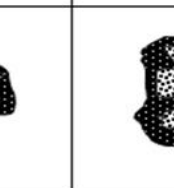
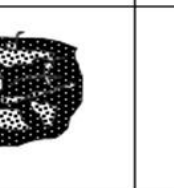




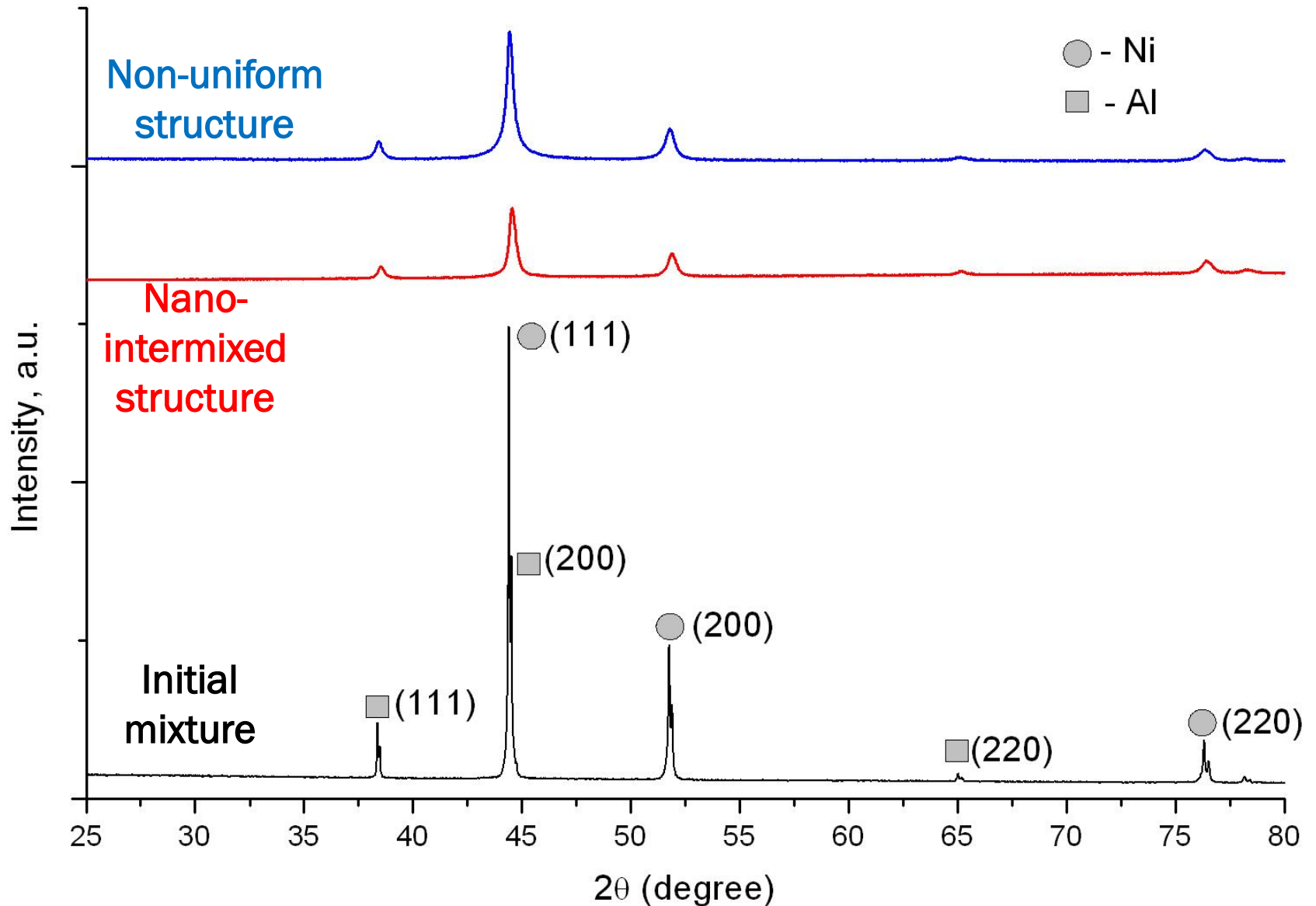
# Two microstructures in Dry + Wet Millings Ni+Al mixtures

 intermixed structure

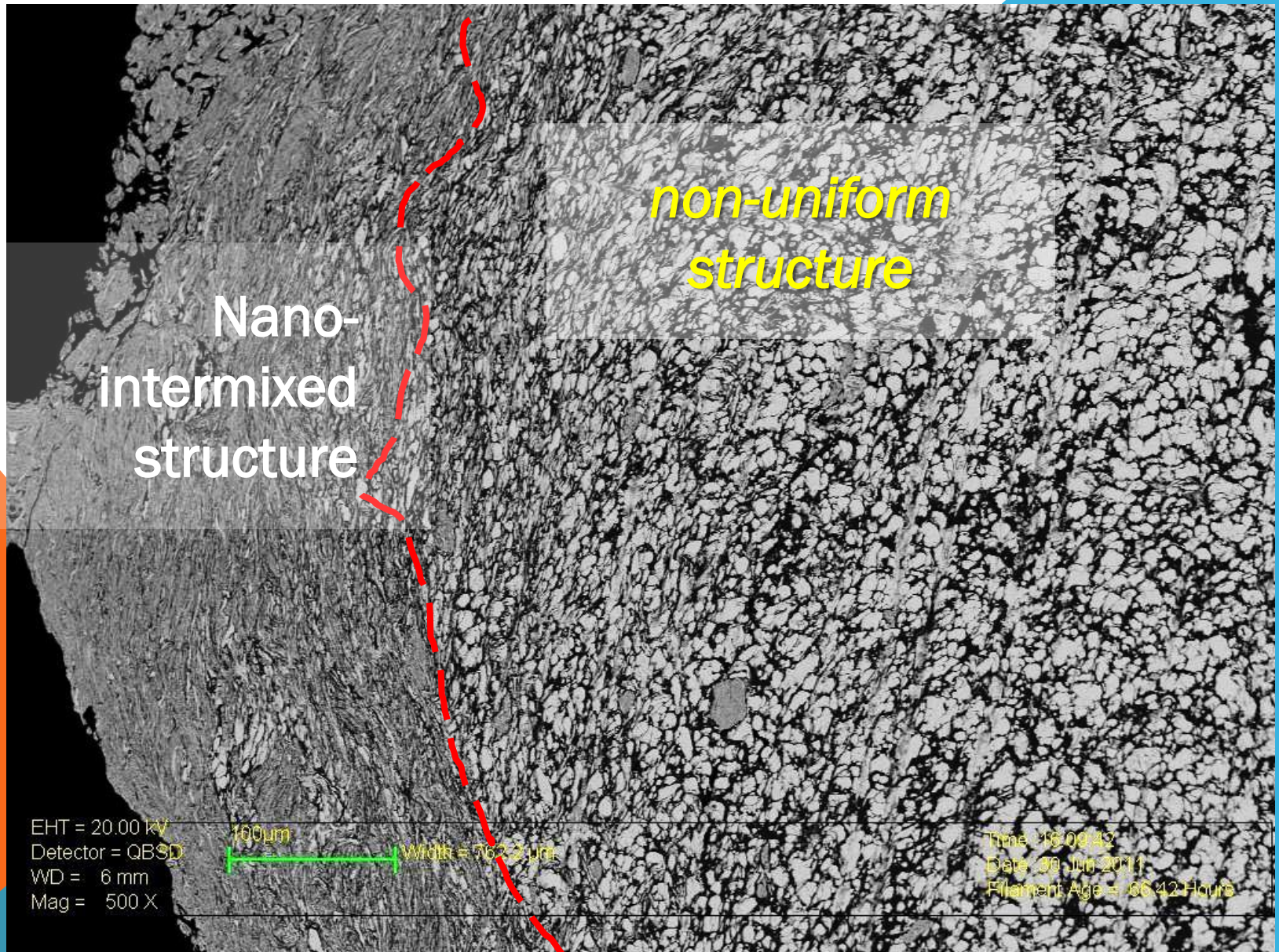
 non-uniform structure

Mechanical treatment conditions	Particle sizes by fractions					
	F1 Below 25 $\mu\text{m}$	F2 25-53 $\mu\text{m}$	F3 53-106 $\mu\text{m}$	F4 106-355 $\mu\text{m}$	F5 355-850 $\mu\text{m}$	F6 More than 850 $\mu\text{m}$
0 min DM + 10 min WM						
4 min DM + 10 min WM						
8 min DM + 10 min WM						
13 min DM + 10 min WM						
17 min DM + 10 min WM						

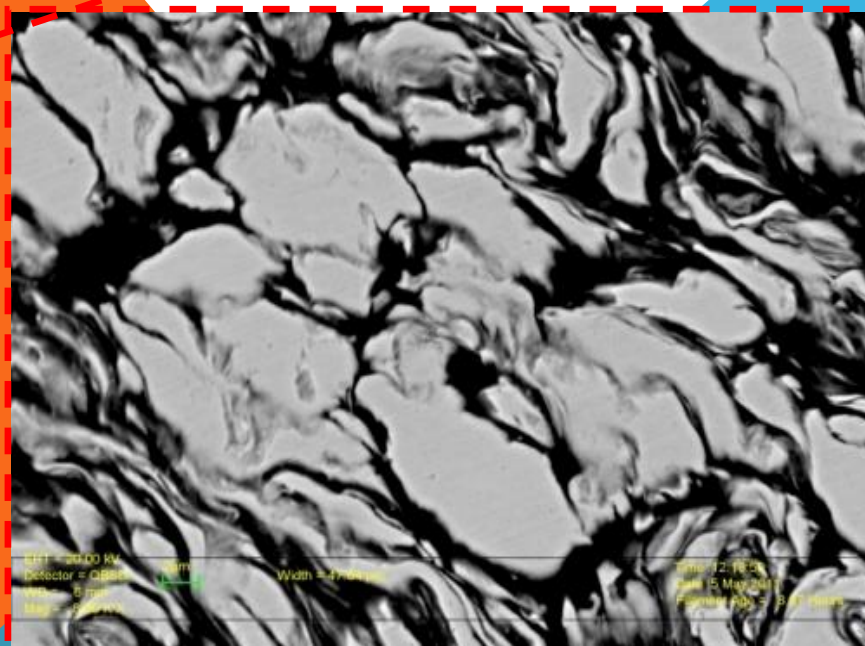
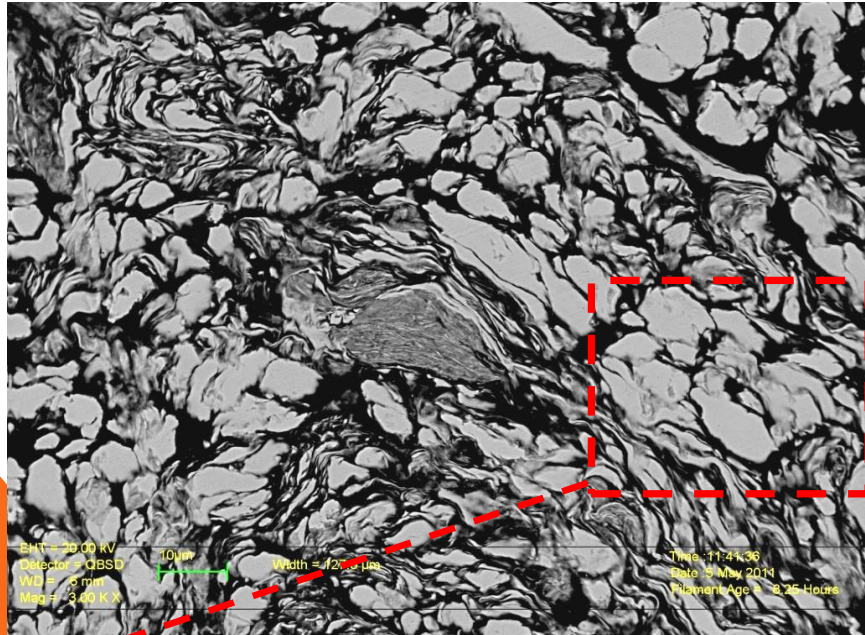
# Phase Compositions of Ni + Al mixtures



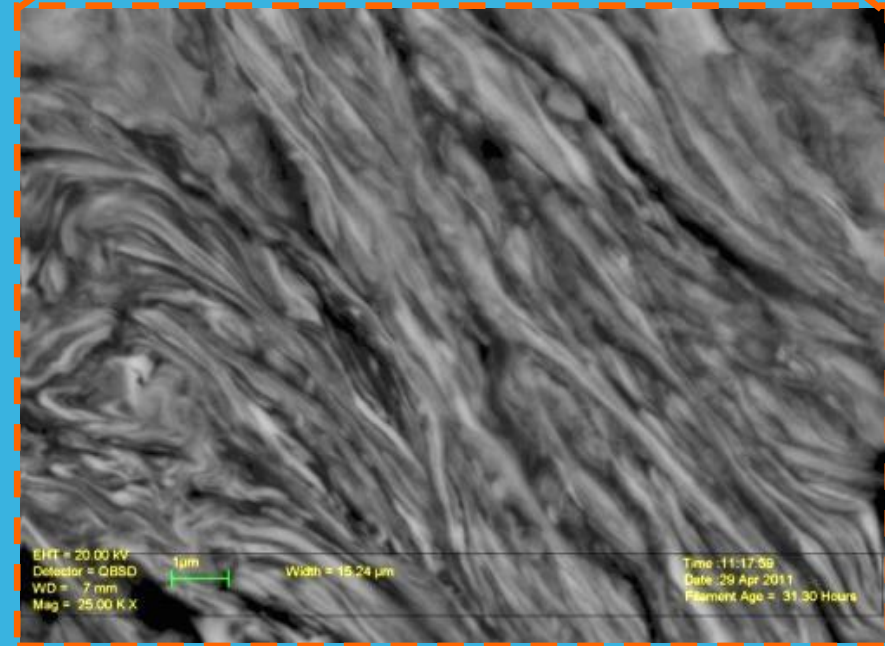
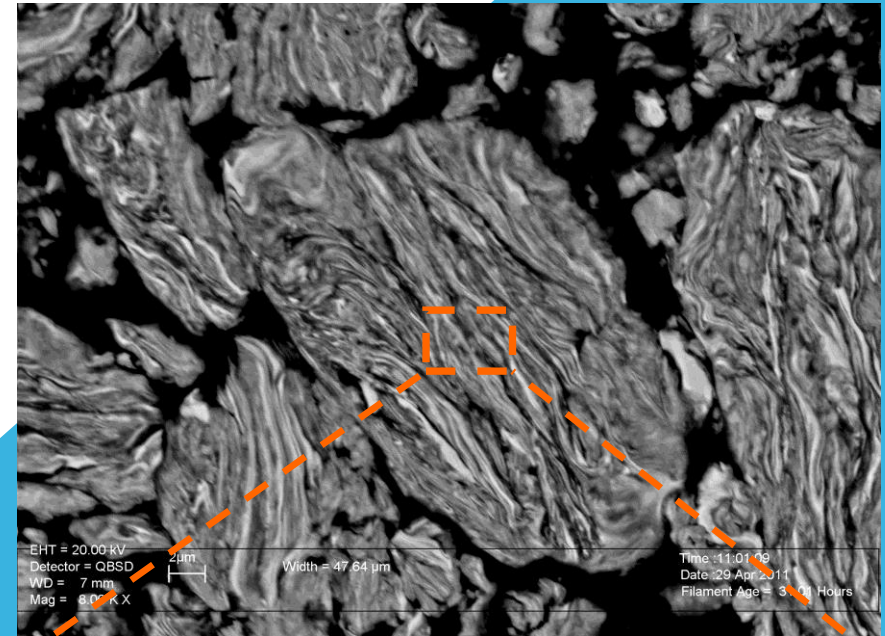
# Microstructure of the Ni-Al composite particle



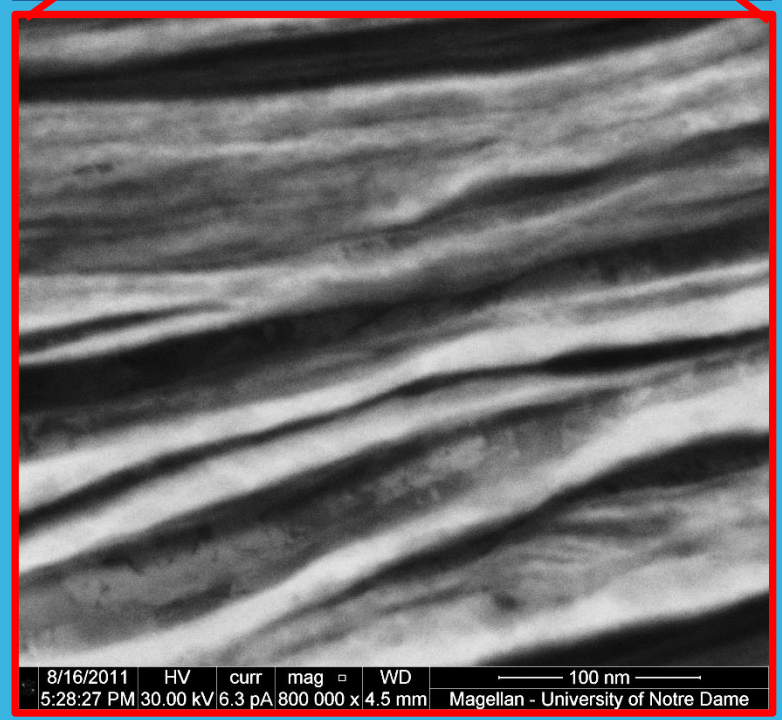
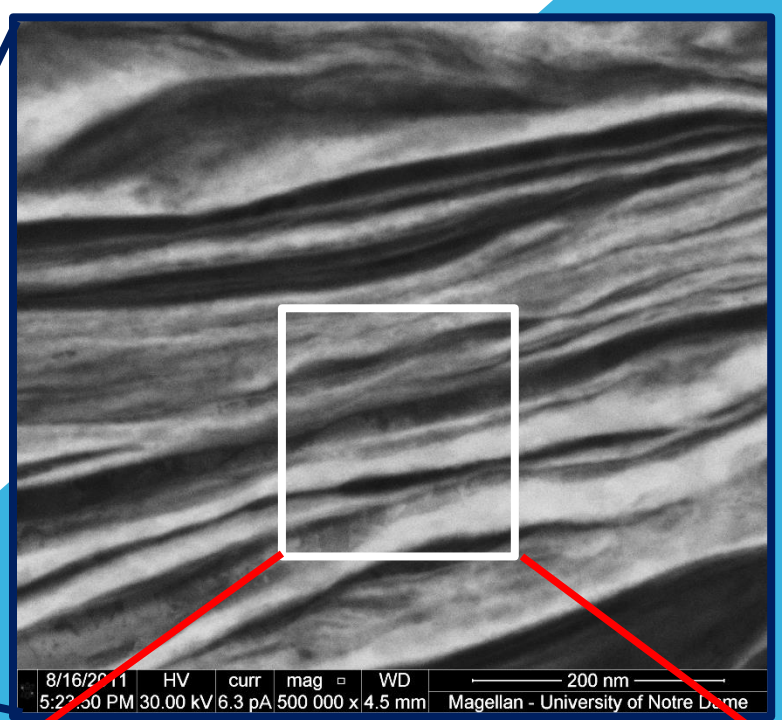
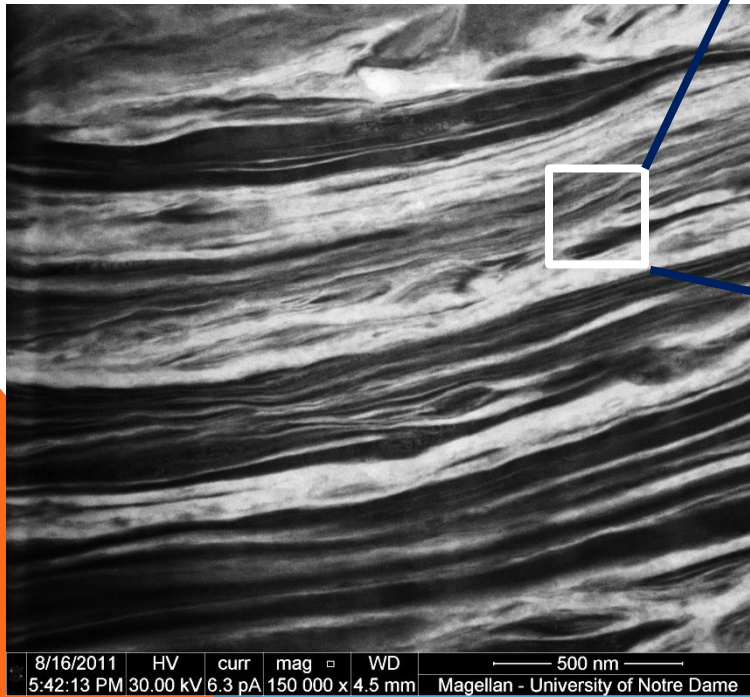
# Non-uniform structure



# Nano-intermixed structure

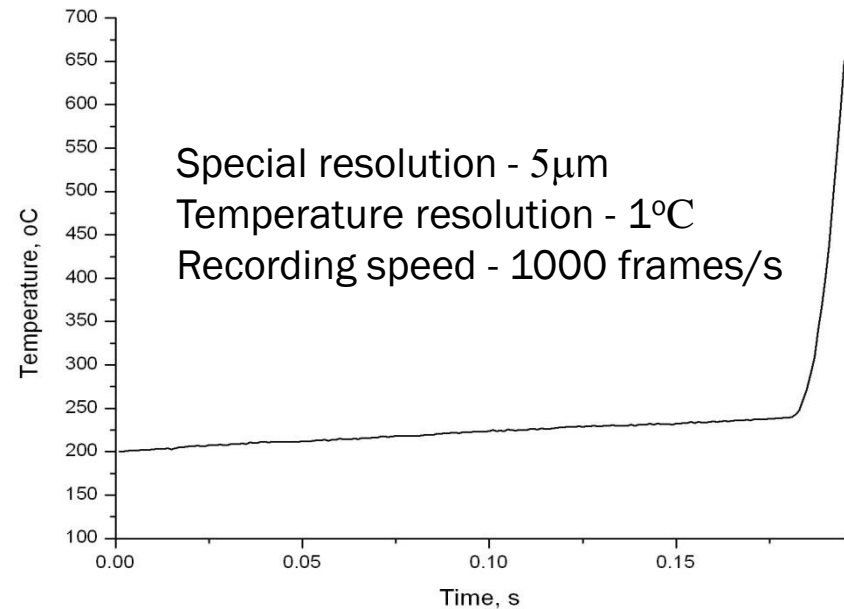
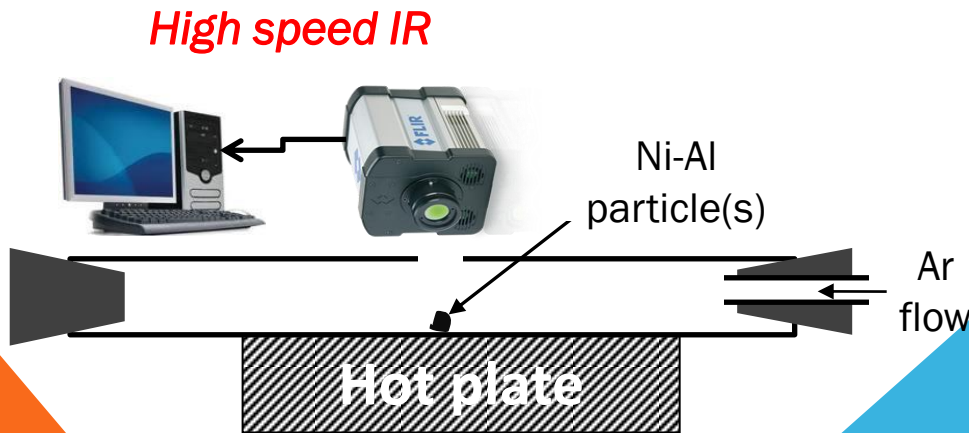


# STEM images of Nano-intermixed structure

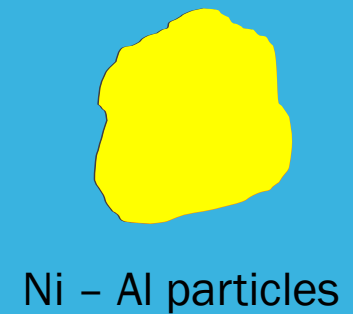
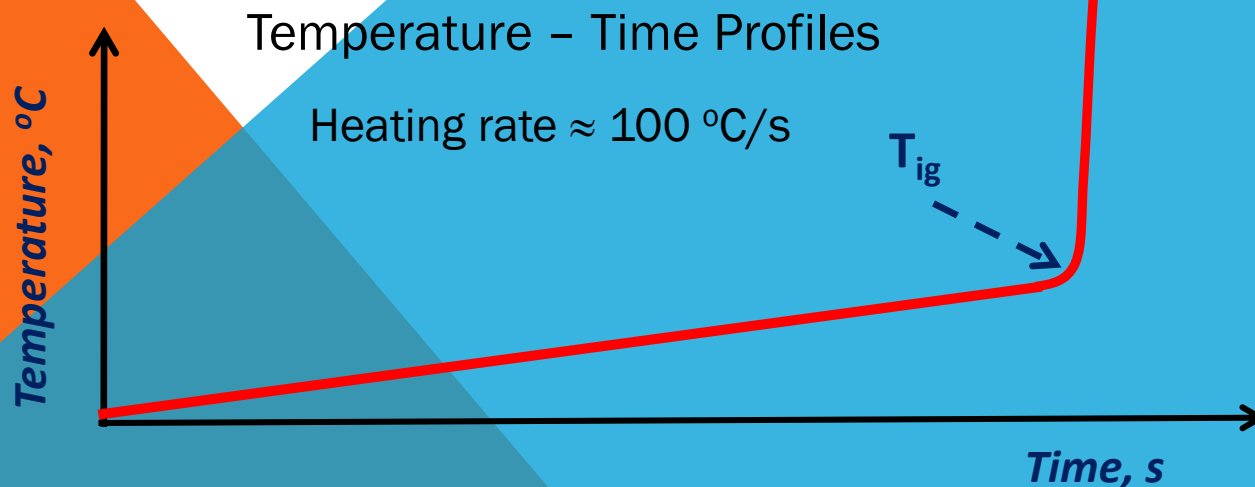


***Reactivity of Ni + Al  
mechanically treated mixtures***

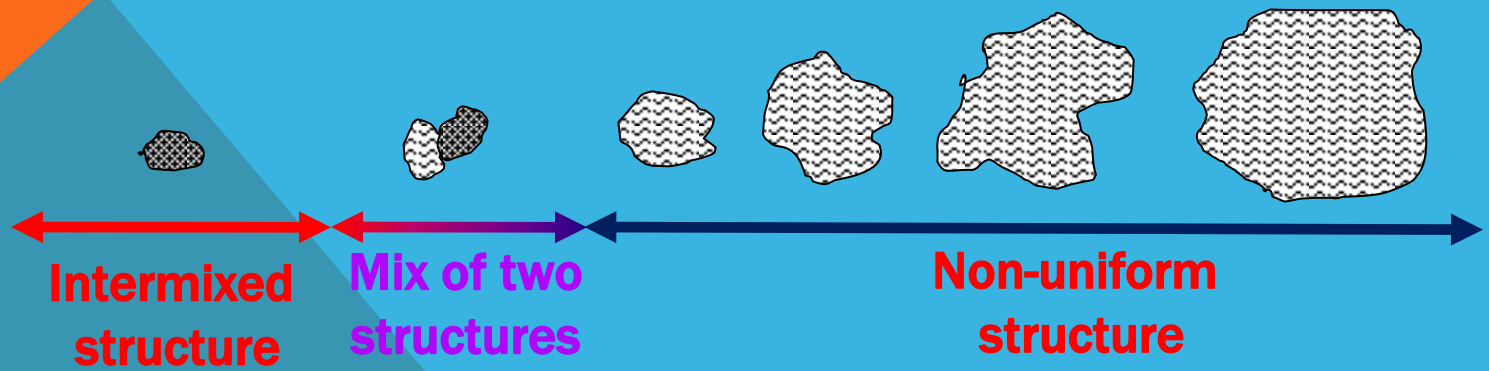
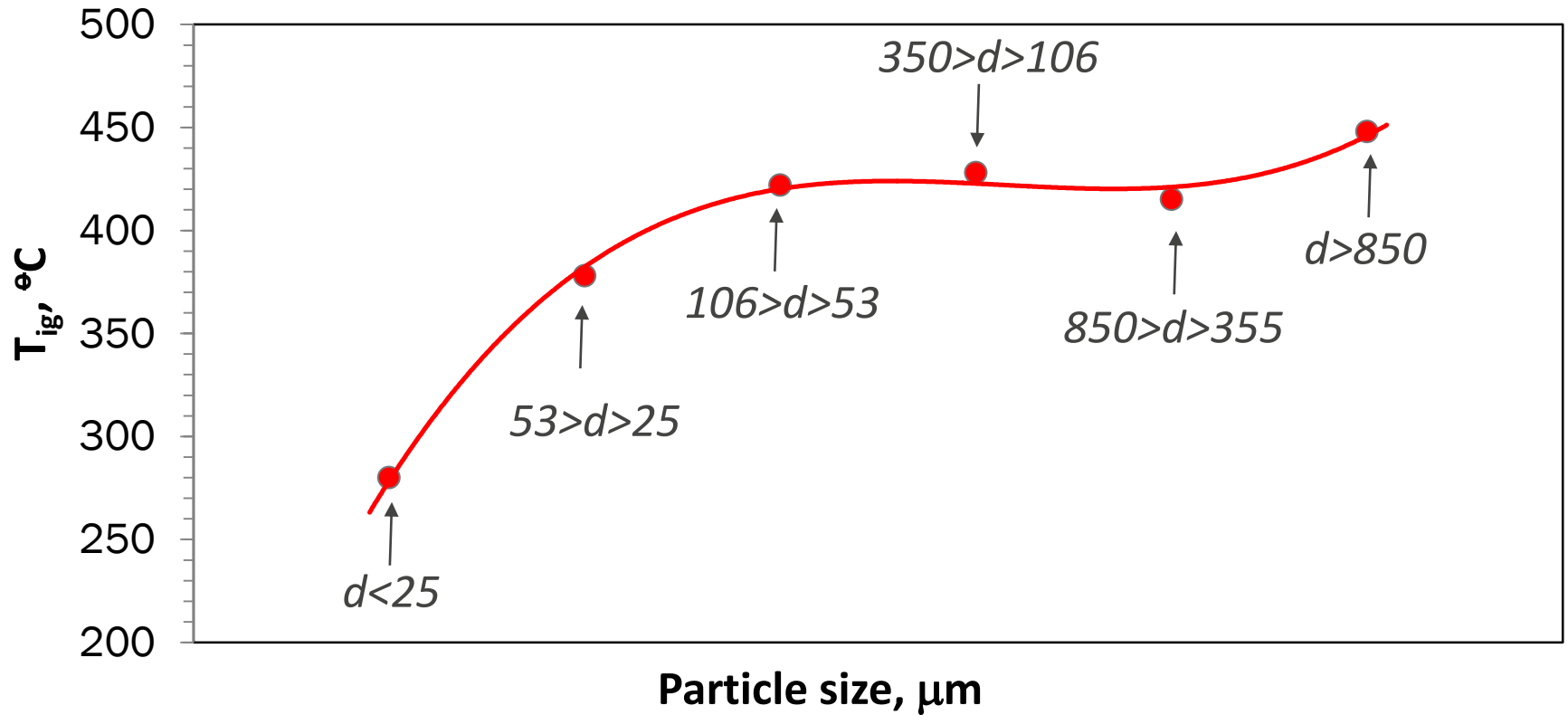
# Setup for measuring Ignition temperature of Ni+Al composite particles



Ignition temperature ( $T_{\text{ig}}$ ) - the lowest ambient temperature at which the self-propagating reaction initiates.

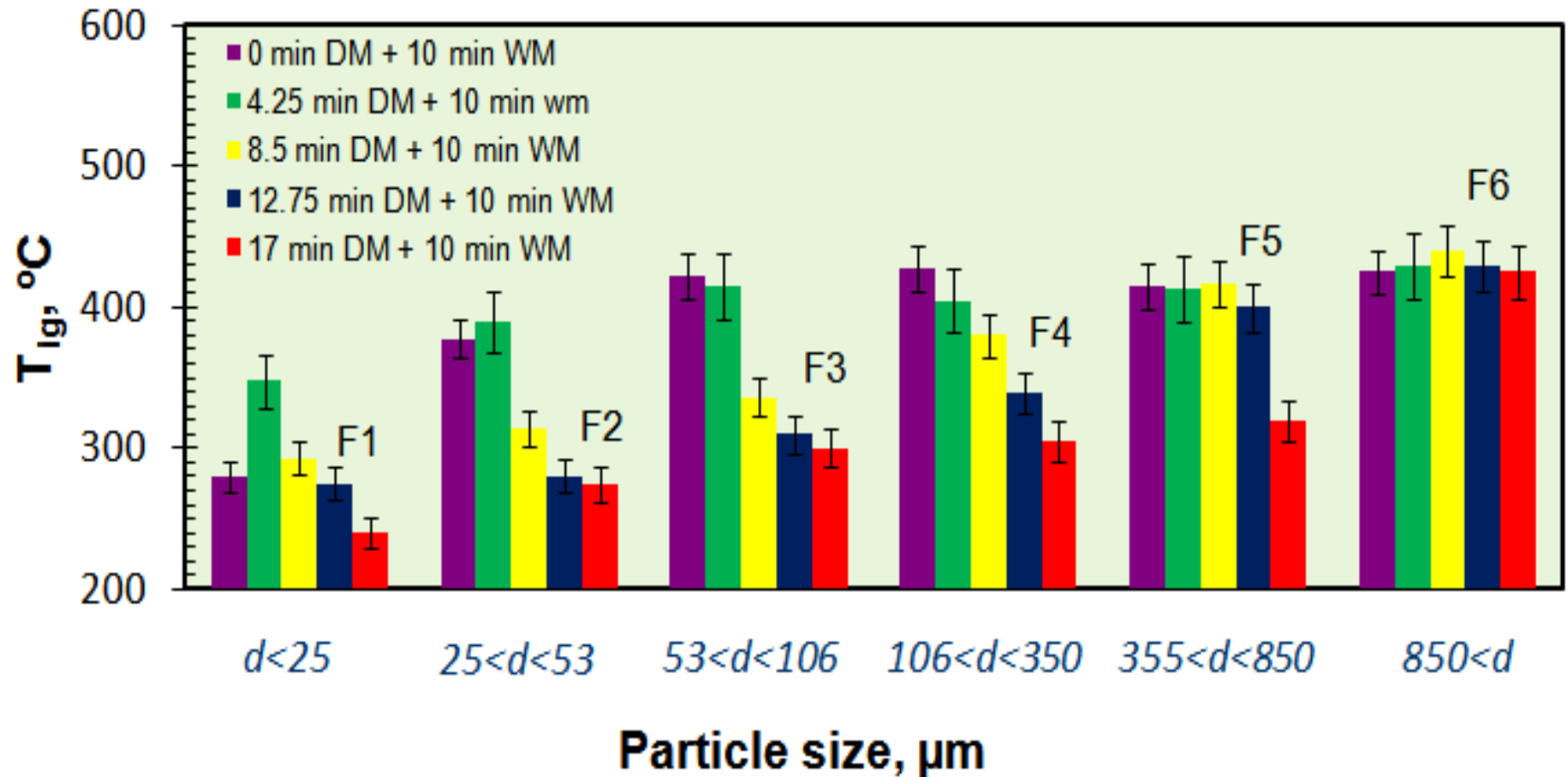


# $T_{IG}$ VS. PARTICLE SIZES OF NI-AL MIXTURE AFTER 0 MIN DM + 10 MIN WM

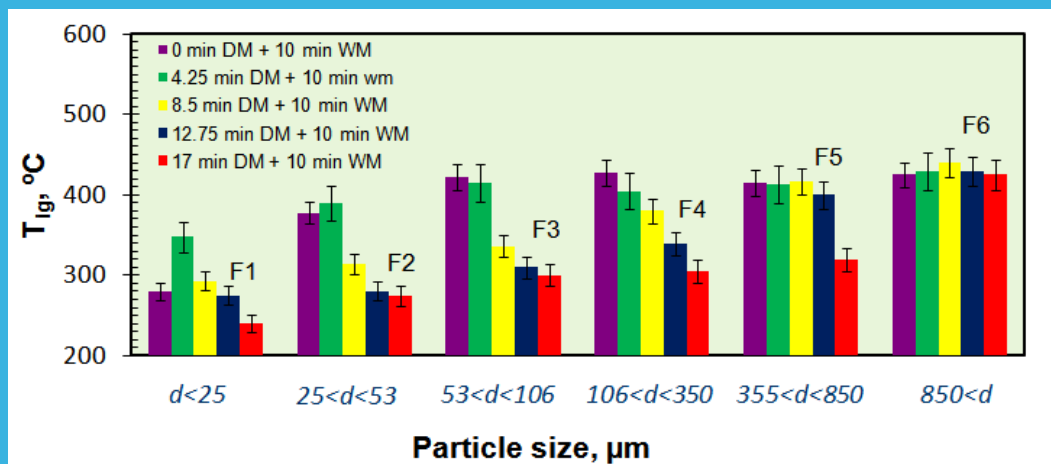
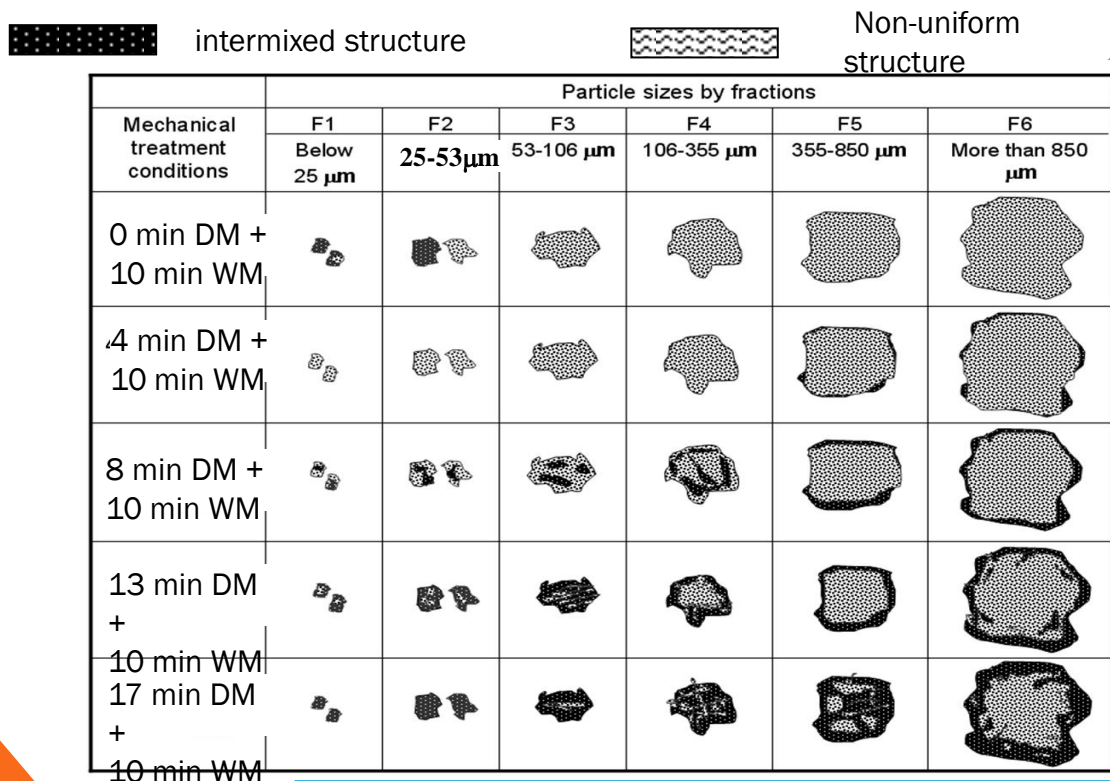




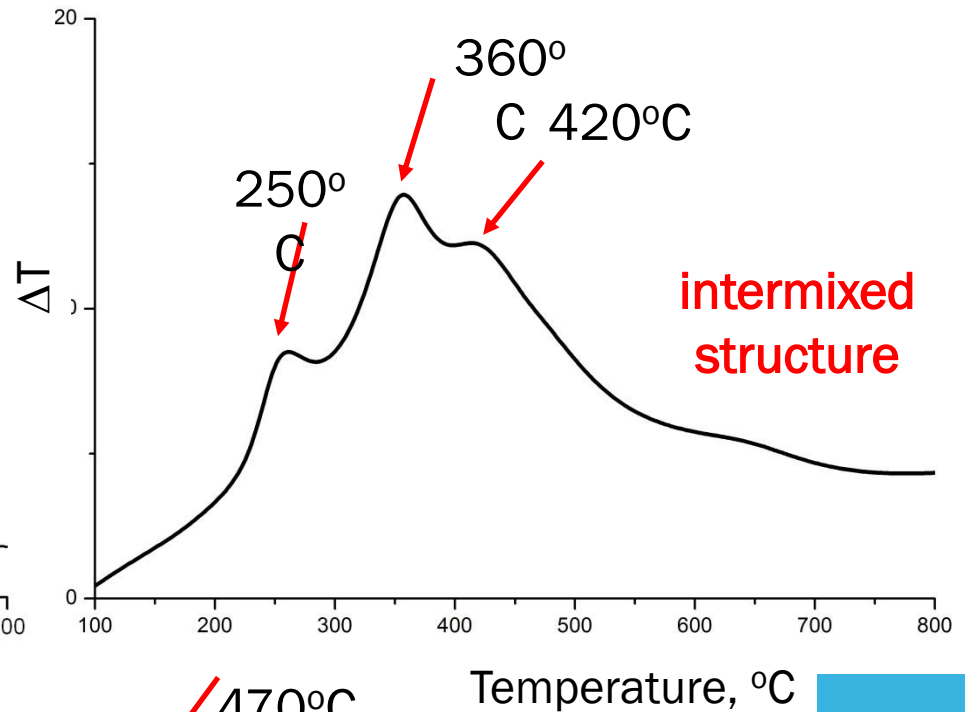
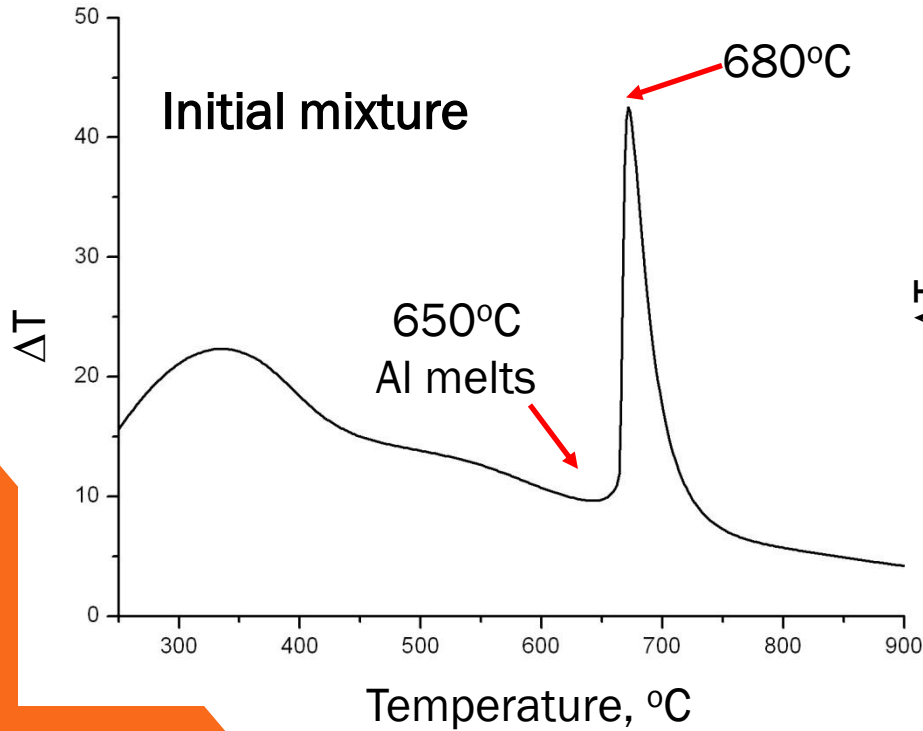
# *$T_{IG}$ OF NI+AL MECHANICALLY TREATED MATERIALS*



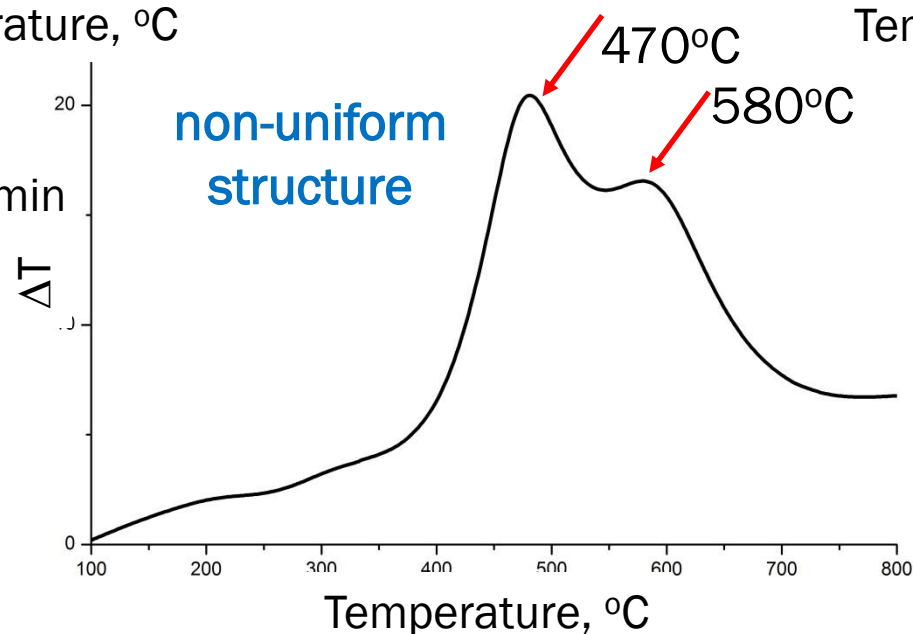
# MICROSTRUCTURE - REACTIVITY RELATIONSHIP



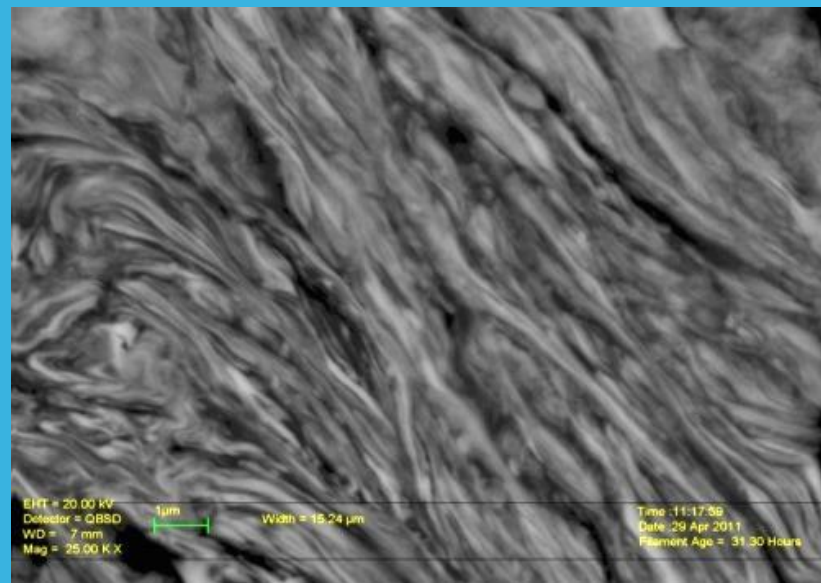
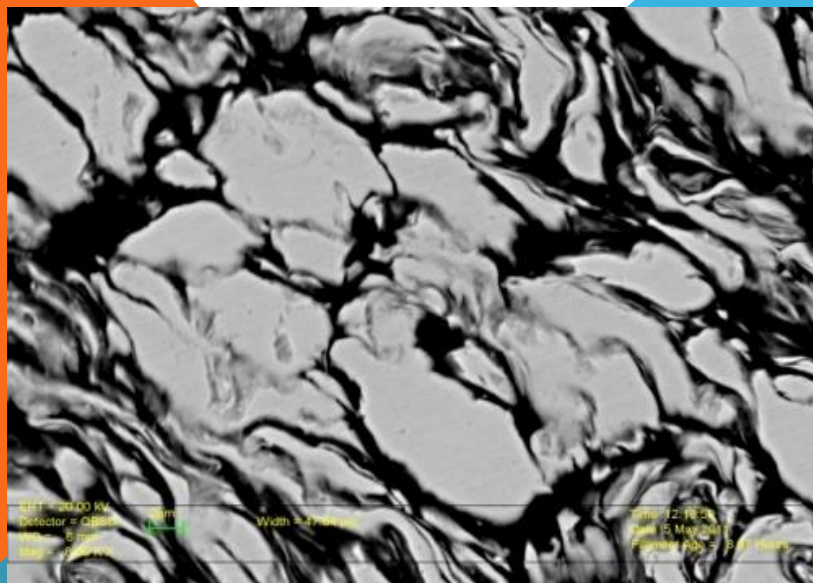
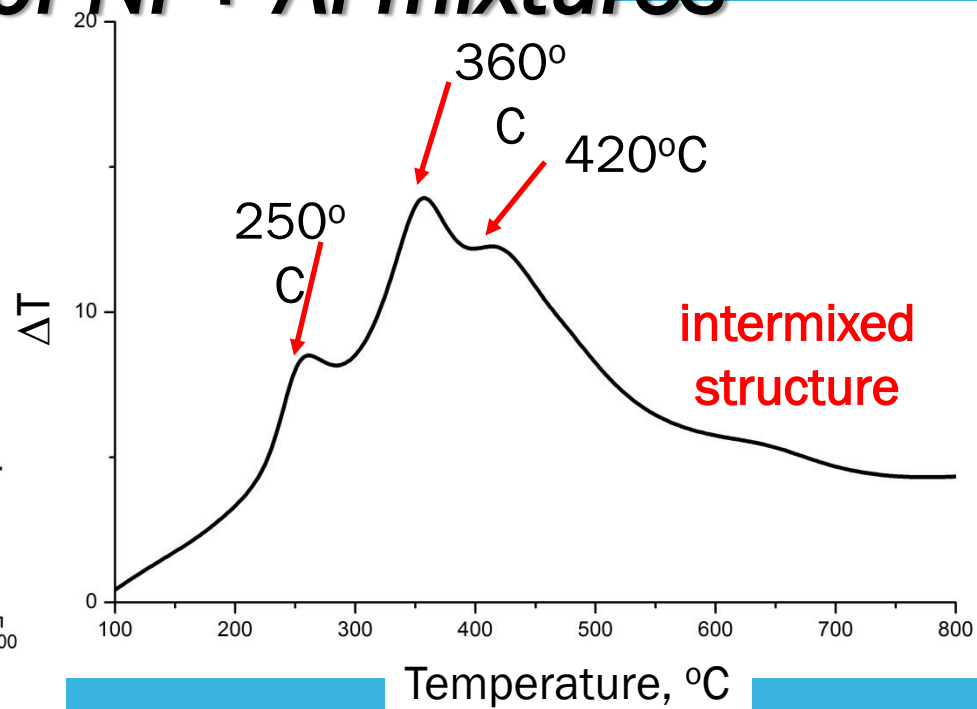
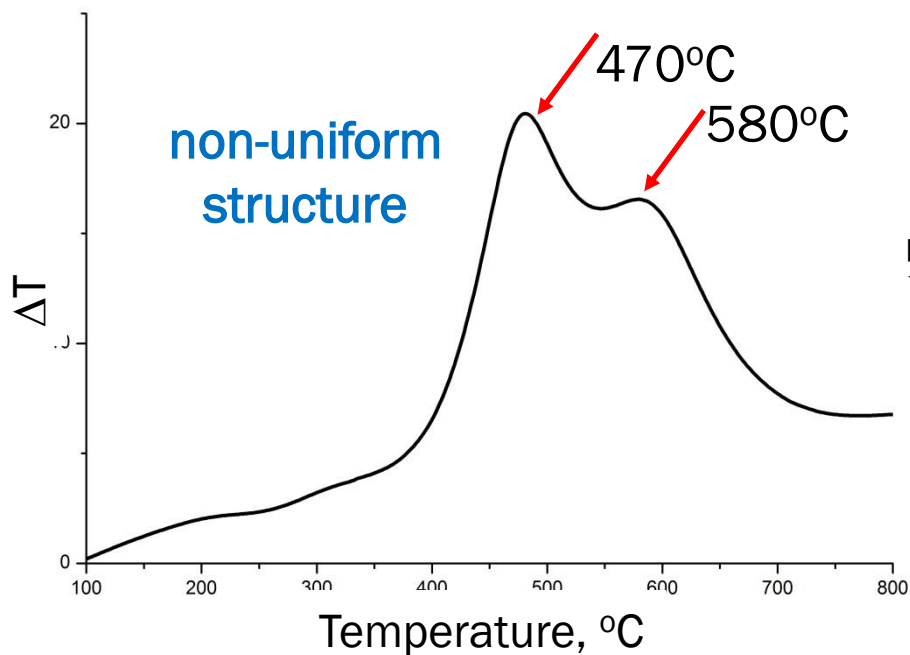
# DTA analysis of Ni + Al mixtures



Heating rate = 50 °C/min



# DTA analysis of Ni + Al mixtures



# Conclusions

- *Two types of microstructures (non-uniform and nano-intermixed) is observed in the Ni+Al composite particles produced by high energy ball milling*
- *The Ni-Al composite's microstructure can be tailored by adjusting the milling conditions*
- *Reactivity of Ni+Al composite particles is primarily depend on the microstructure, and intermixed nanostructure results in very low thermal ignition temperatures ( $\sim 250^{\circ}\text{C}$ ).*