

# Regularized Model of Post-Touchdown Configurations in Electrostatic MEMS: Bistability Analysis.

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**Abstract** This paper considers the problem of stiction in electrostatic-elastic deflections whereby elastic surfaces adhere to one another after coming into physical contact under attracting Coulomb interactions. This phenomenon is studied in a family of recently derived models which account for forces which become important when the elastic surfaces are in close proximity. The presence of bistability in these models results in hysteresis, or non reversibility, which accounts for the difficulty in achieving separation after an initial contact event. We use singular perturbation techniques to derive explicit formula for the critical parameters over which bistability occurs and discuss new operational modes which arise when bistability is present.

**Keywords** Singular perturbation techniques · nano-technology · stiction · Van der Waals forces · Casimir forces · higher order partial differential equations.

## 1 Introduction

Micro electromechanical Systems (MEMS) combine moving elastic component with electrostatic forces on miniature scales to perform a variety of tasks in engineering applications. When the attracting electrostatic forces are large enough, the elastic components of the device may come into physical contact - an event known as *touchdown* or *snap-through*. This outcome may be undesirable or essential in normal operation, depending on the particular application. In either scenario, it is desirable that the device is able to revert to a base state after touchdown. However, after initial contact, the elastic surfaces may adhere to one another thus complicating the return to a separated state. This phenomenon, also known as *stiction*, is due to Casimir, capillary and Van der Waals forces which become prominent on very small separation scales and is a major problem in the fabrication and operation of MEMS (cf. [1–3]).

Canonical mathematical models (cf. [4–7]) of MEMS do not shed light on the problem of stiction as they capture contact events as finite time singularities of the governing equations, thus providing no information on subsequent configurations of the device. A recently introduced model (cf. [8]) is a first attempt to mathematically investigate these post-touchdown states by including a thin insulating layer which prevents physical contact between the deflecting surface and the substrate (cf. Fig. 1). These models are partial differential equations whose solutions represent the deflection of an elastic

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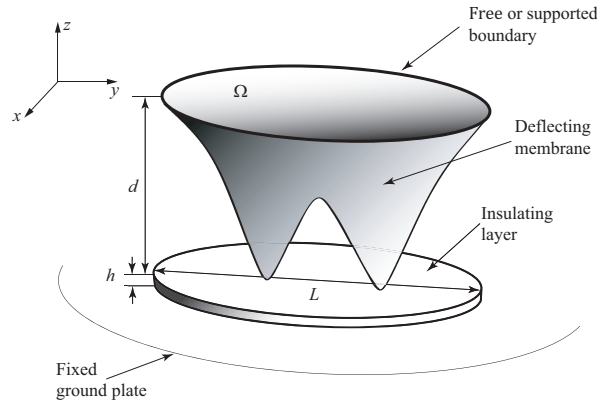
surface under Coulomb forcing. If the deflecting surface is represented as a one-dimensional flexible elastic beam on  $\Omega = [-1, 1]$ , then the non-dimensional deflection  $u(x, t)$  was shown (cf. [8]) to satisfy the fourth order partial differential equation

$$u_t = -u_{xxxx} - \frac{\lambda}{(1+u)^2} + \frac{\lambda\varepsilon^{m-2}}{(1+u)^m}, \quad x \in (-1, 1); \quad u(\pm 1) = u_x(\pm 1) = 0, \quad (1.1)$$

where  $\lambda \geq 0$  is a bifurcation parameter which depends on the voltage applied to the system. In terms of physical quantities, the two dimensionless parameters in (1.1) are given by (cf. [8])

$$\lambda = \frac{\varepsilon_0 L^4 V^2}{2dEI}, \quad \varepsilon = \frac{d\sigma_0}{h\sigma_1},$$

where  $L$ ,  $d$  and  $h$  are the characteristic length scales of the device, the gap spacing and the insulating layer (cf. Fig. 1). The parameter  $\varepsilon$  is determined in terms the geometrical ratio  $d/h$  and the ratio  $\sigma_0/\sigma_1$  of dielectric constants in the insulating layer and the gap. The parameter  $V$  is the potential difference between the deflecting surface and the substrate,  $\varepsilon_0$  is the permittivity of free space and  $EI$  is the flexural rigidity of the deflecting plate. The present work focuses on understanding the bifurcation structure, and in particular the bi-stable properties, of one dimensional equilibrium solutions to (1.1).



**Fig. 1** Schematic diagram of the regularized MEMS device. Reproduced from [8].

The regularizing term  $\varepsilon^{m-2}(1+u)^{-m}$  for  $m > 2$  can account for a variety of physical effects which come into play when  $u \approx -1$  and play a role in stiction. For example  $m = 4$  accounts for the Casimir force, a quantum effect which manifests itself on macroscopic scales [9, 10]. The case  $m = 3$  models Van der Waals forces [9, 11, 12]. The particular force that dominates when the spacing is small depends on the particular geometry of the device and application. Casimir forces scale as  $F_{Cas} \propto d^{-4}$  while Van der Waals forces scale like  $F_{VdW} \propto d^{-3}$  where  $d$  is the dimensional gap spacing (cf. Fig. 1). In certain scenarios, both forces may be of equal importance and the inclusion of two regularizing terms would be justified [3, 13]. Regularizing potentials of this form have also been extensively utilized in studies of the de-wetting process of thin films on solid substrates [14–17].

In canonical models of MEMS for which  $\varepsilon = 0$ , touchdown occurs when  $\lambda$  exceeds a threshold  $\lambda^*$  and  $u \rightarrow -1$  in a finite time  $T$ . Since this event is crucial to the operation of MEMS, many studies have focussed on analyzing the local structure of solutions to (1.1) in this regime and estimation of parameters  $T$  and  $\lambda^*$  (cf. [4, 6, 7, 18, 19]). However, the manifestation of touchdown as a singularity of (1.1) is a serious limitation of the canonical model as no information is provided regarding subsequent configurations of the system.

The regularized model (1.1) with suitable initial data is globally well posed for  $\varepsilon > 0$  [8]. This key property follows because (1.1) arises from the  $L^2$  gradient flow of the energy functional

$$\mathcal{E}(u) = \int_0^1 \left( \frac{1}{2} |u_{xx}|^2 - \frac{\lambda}{(1+u)} + \frac{\lambda\varepsilon^{m-2}}{(m-1)(1+u)^{m-1}} \right) dx.$$

which is dissipative ( $d\mathcal{E}/dt \leq 0$ ) and bounded from below. The possibilities for the limiting behavior of dynamic solutions to (1.1) as  $t \rightarrow \infty$  are therefore related to the multiplicity and stability of solutions to the steady state problem

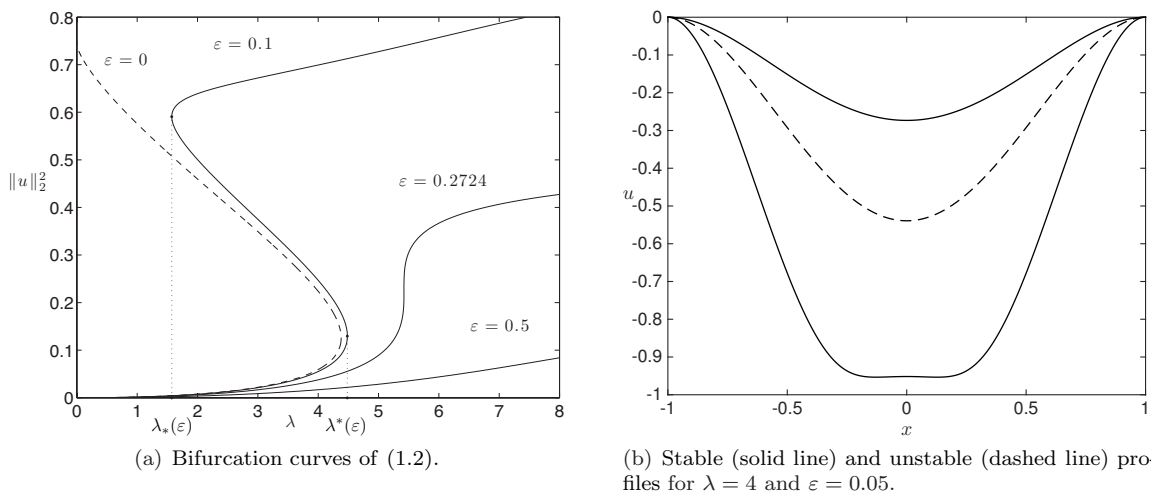
$$-u_{xxxx} = \frac{\lambda}{(1+u)^2} - \frac{\lambda\varepsilon^{m-2}}{(1+u)^m}, \quad x \in (-1, 1); \quad u(\pm 1) = u_x(\pm 1) = 0. \quad (1.2)$$

In the present work, the focus is on studying solution multiplicity of (1.2) as the parameters  $\varepsilon$  and  $m$  vary.

The numerically obtained bifurcation diagrams of (1.2), displayed in Fig. 2, show that there are two remarkable departures from the  $\varepsilon = 0$  case. First, there is a new maximal solution branch representing post-touchdown (contact) steady states. This branch of equilibria is characterized (cf. [8] for derivation and validation) by the following asymptotic parameterization in terms its squared  $L^2$  norm

$$\|u(x; \varepsilon)\|_2^2 = 2 \left[ 1 - \frac{22}{35} \left( \frac{18\varepsilon(m-1)}{\lambda(m-2)} \right)^{\frac{1}{4}} + \mathcal{O}(\varepsilon^{\frac{3}{4}}) \right], \quad (1.3)$$

in the limit as  $\varepsilon \rightarrow 0$ . Second, it is clear that the multiplicity of equilibrium solutions to (1.2) can be quite different depending on the value of the parameter  $\varepsilon$ . More precisely, the bifurcation diagrams suggest the existence of a critical value  $\varepsilon_c$  such that for  $\varepsilon \geq \varepsilon_c$ , equation (1.2) has a unique solution for each  $\lambda$ . In the case where  $0 < \varepsilon < \varepsilon_c$ , the bifurcation diagrams have two saddle node bifurcation points  $\lambda_*(\varepsilon)$  and  $\lambda^*(\varepsilon)$ . Correspondingly, for  $\lambda_* < \lambda < \lambda^*$ , equation (1.2) admits three solutions, while for  $\lambda > \lambda^*$  and  $\lambda < \lambda_*$ , there is a unique solution.



**Fig. 2** Left Panel: Bifurcation curves for equilibrium solutions of (1.2) for  $m = 4$ . The three solid curves plotted correspond to  $\varepsilon < \varepsilon_c$ ,  $\varepsilon \approx \varepsilon_c$  and  $\varepsilon > \varepsilon_c$  highlight the threshold of bistability. The dashed curve is the solution set associated with the  $\varepsilon = 0$  problem. Right Panel: Stable (solid lines) and unstable (dashed line) solution profiles of (1.2) for  $\lambda = 4$  and  $\varepsilon = 0.05$ . The upper profile represents a separated state, while the lower profile represents a contact state of the device. Multiple minima in the contacted state arise from a non-monotone boundary layer profile in the vicinity of the contact points (cf. [8]).

The potential for bistability over the range of values  $0 < \varepsilon < \varepsilon_c$  has several practical implications for the construction of MEMS (cf. [20–22]). Robust switching behavior can be generated from bistable systems, specifically the system can transition between stable large and small norm solutions over the parameter window  $\lambda \in (\lambda_*(\varepsilon), \lambda^*(\varepsilon))$ . Additionally, Fig. 2 also reveals the presence of hysteresis, or non-reversibility, in (1.1) for  $\varepsilon < \varepsilon_c$  and therefore captures the stiction phenomenon. For  $\lambda > \lambda^*$ , the

device is in a stable state with surfaces in contact. To unstick the device however,  $\lambda$  must be decreased below the second fold point  $\lambda_*$  where  $\lambda_* < \lambda^*$ . For a detailed study of the transient dynamics between stable states of (1.1), see [23].

The important practical problem addressed in this work is the quantification of the key thresholds  $\varepsilon_c$ ,  $\lambda^*(\varepsilon)$  and  $\lambda_*(\varepsilon)$  in (1.2) for  $m > 2$ . The approach undertaken is a detailed asymptotic analysis of equations (1.2) in the limit as  $\varepsilon \rightarrow 0^+$ , the result of which is explicit formulas for the fold points  $\lambda^*(\varepsilon)$  and  $\lambda_*(\varepsilon)$  for  $m > 2$ . A heuristic approximation of the critical parameter  $\varepsilon_c$  can then be obtained from the condition

$$\lambda^*(\varepsilon_c) = \lambda_*(\varepsilon_c). \quad (1.4)$$

In engineering studies of MEMS, mathematical models typically feature fourth order terms such as (1.2) as these descriptions give good quantitative agreement with experiments. On the other hand, mathematical studies of MEMS are largely focussed on second order equations which describe the deflecting surface as a tensioned membrane and rely on maximum principles for their analysis. The present work is focussed solely on the fourth order model for two main reasons. First, the explicit formulas developed in the present work are useful to MEMS practitioners who seek to exploit bistability in the operation of these devices. Second, while the Laplacian counterpart of (1.2) (with  $\partial_n u|_{\partial\Omega} = 0$  omitted) also exhibits the bistability structure observed in Fig. 2, its analysis is better suited to a phase plane approach (cf. Sec. 3.4 of [8]). A dynamical systems approach does not naturally extend to the fourth order problem and so we adopt a singular perturbation analysis of (1.2) as  $\varepsilon \rightarrow 0$ . For recent mathematical studies on the existence of solutions to the second order counterpart of (1.1) in the case  $m = 4$ , see [24, 25].

The structure of the paper is as follows. In Sec. 2, the dependence of the principal fold point  $\lambda^*$  of (1.2) on  $\varepsilon$  and  $m$  is analyzed in the limit as  $\varepsilon \rightarrow 0$ . Through a regular perturbation analysis, the formula

$$\lambda^*(\varepsilon) = \lambda_0 + \varepsilon^{2(m-2)}\lambda_1 + \mathcal{O}(\varepsilon^{4(m-2)}),$$

is established in Principal Result 1 and values of  $\lambda_0$  and  $\lambda_1$  calculated for a range of  $m$ .

In Sec. 3, we calculate the secondary saddle node bifurcation point  $\lambda_*(\varepsilon)$  in the limit  $\lambda_*(\varepsilon) \rightarrow 0$  as  $\varepsilon \rightarrow 0$ . This fold point is not present in the case  $\varepsilon = 0$  and its location requires a detailed singular perturbation calculation with systematic use of logarithmic switchback terms. These terms are well known in the asymptotic analysis of high Reynold's number flow problems [26–29] and in other singular perturbation problems related to MEMS [19, 30]. In Principal Result 2, we obtain the expansion

$$\lambda_*(\varepsilon) \sim \varepsilon^{\frac{3}{2}}\lambda_0 + \varepsilon^2\lambda_1 + \dots$$

where  $\lambda_0$  and  $\lambda_1$  are determined in terms of  $m$ . Combining Principal Results 1 and 2 gives an asymptotic prediction (cf. (3.29)) for the bistable parameter range  $\lambda_* < \lambda < \lambda^*$  of equation (1.2). For example, in the case  $m = 4$ , we find that range to be

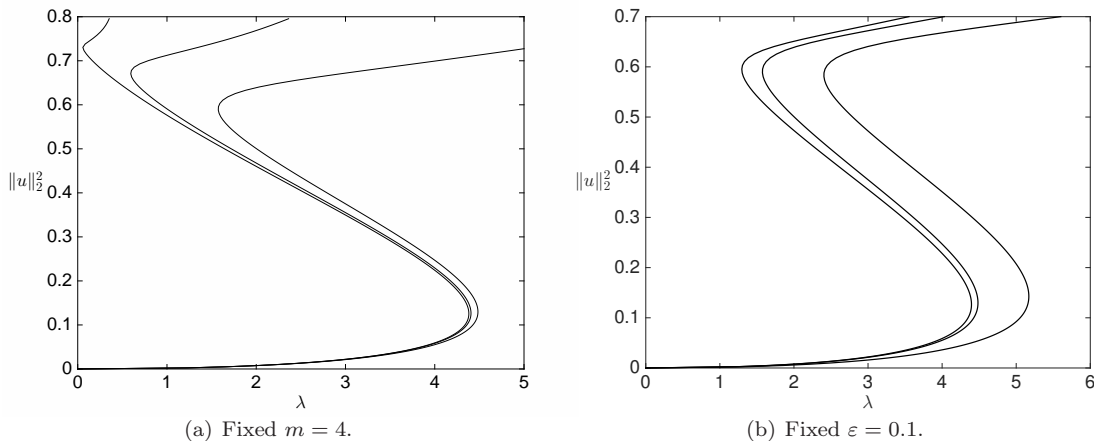
$$61.4586 \varepsilon^{\frac{3}{2}} - 41.8124 \varepsilon^2 < \lambda < 4.3809 + 9.9713 \varepsilon^2. \quad (1.5)$$

By numerically solving for the value of  $\varepsilon$  at which this bistable range shrinks to a point, an estimate can be formulated for the critical  $\varepsilon_c$  (cf. Sec. 3.1 and Principal Result 3). In the case  $m = 4$  for example, we obtain an asymptotic estimate of  $\varepsilon_c \approx 0.2468$  which compares well ( $\approx 10\%$ ) with the numerical estimate  $\varepsilon_c \approx 0.2724$ . In Sec. 4 we discuss avenues for future investigation.

## 2 Asymptotics of the fold point of the minimal branch

In this section, we calculate the effect of the perturbed potential on the location of the fold point  $\lambda^*(\varepsilon)$ , located at the end of the minimal solution branch of the equilibrium problem (1.2). The solution set  $(\lambda(\varepsilon), u(x; \varepsilon))$  of (1.2) can be computed numerically by first specifying the squared  $L^2$  norm of

solutions, then formulating the MATLAB boundary value problem solver `bvp4c` to obtain  $\lambda$  as a constant parameter.



**Fig. 3** Bifurcation diagrams of equilibrium solutions of (1.2). Left panel,  $m = 4$  and  $\varepsilon = 0.1, 0.05, 0.01$ . Right panel:  $\varepsilon = 0.1$  and  $m = 3, 4, 5$ .

The fold point  $\lambda^*(\varepsilon)$  is calculated by means of a regular expansion of (1.2), developed in the limit as  $\varepsilon \rightarrow 0$ . See also [31–33] for more background on this approach. This approach will not work for the secondary saddle-node bifurcation  $\lambda_*(\varepsilon)$  which is not present in the  $\varepsilon = 0$  case. This second threshold indicates the onset of the large norm solution branch and is located at the end of the unstable branch of equilibria emanating from the first saddle-node.

Let us assume a parameterization of the minimal solution branch in terms of the squared  $L^2$  norm  $\alpha = \|u(x; \varepsilon)\|_2^2$ , of equilibrium solutions. A two term expansion of the solution, valid for  $u$  away from  $-1$ , is given by

$$u = u_0(x; \alpha) + \varepsilon^{m-2}u_1(x; \alpha) + \mathcal{O}(\varepsilon^{2(m-2)}), \quad \lambda = \lambda_0(\alpha) + \varepsilon^{m-2}\lambda_1(\alpha) + \mathcal{O}(\varepsilon^{2(m-2)}). \quad (2.1)$$

The location of the principal fold point is expanded in a regular fashion as

$$\alpha^*(\varepsilon) = \alpha_0^* + \varepsilon^{m-2}\alpha_1^* + \dots$$

where the  $\alpha_j$  are determined by the condition that  $d\lambda/d\alpha = 0$  independent of  $\varepsilon$ . The principal fold  $(\lambda^*, \alpha^*)$ , then admits the two term expansion

$$\lambda^*(\varepsilon) = \lambda(\alpha^*) = \lambda_0(\alpha_0^*) + \varepsilon^{m-2}\lambda_1(\alpha_0^*) + \mathcal{O}(\varepsilon^{2(m-2)}). \quad (2.2)$$

To complete the two term expansion (2.2), the quantity  $\lambda_1(\alpha_0^*)$  is now determined by applying the expansion (2.1) to equation (1.2) and arriving at the problems

$$-u_{0xxxx} = \frac{\lambda_0}{(1+u_0)^2}, \quad -1 < x < 1; \quad u_0(\pm 1) = u_{0x}(\pm 1) = 0. \quad (2.3a)$$

$$\mathcal{L}u_1 = \frac{\lambda_1}{(1+u_0)^2} - \frac{\lambda_0}{(1+u_0)^m}, \quad -1 < x < 1; \quad u_1(\pm 1) = u_{1x}(\pm 1) = 0. \quad (2.3b)$$

where  $\mathcal{L}$  is the linearized operator

$$\mathcal{L}\phi = -\phi_{xxxx} + \frac{2\lambda_0}{(1+u_0)^3}\phi.$$

$m$	3	4	5	6	7	8
$\lambda_1(\alpha_0^*)$	6.5715	9.9690	15.2703	23.5847	36.6840	57.4034

**Table 1** Numerical values of correction term  $\lambda_1(\alpha_0^*)$  in the asymptotic expansion of the saddle-node fold point  $(\lambda^*, \alpha^*)$  for  $m = 3, 4, \dots, 8$ .

The location of the principal fold point of (2.3a) is  $(\alpha_0^*, \lambda_0(\alpha_0^*))$  and satisfies  $\lambda_{0\alpha}(\alpha_0^*) = 0$ . The coordinates of this principal fold point can be accurately located by Newton-Raphson iterations and has the numerical value

$$(\alpha_0^*, \lambda_0(\alpha_0^*)) = (0.1256, 4.3809). \quad (2.4)$$

To calculate the quantity  $\lambda_1(\alpha_0^*)$ , equation (2.3b) is differentiated with respect to  $\alpha$  to reveal that at  $\alpha = \alpha_0^*$ ,  $\lambda_{0\alpha} = 0$  and consequently there is a nontrivial solution satisfying  $\mathcal{L}u_{0\alpha} = 0$ . This provides a solvability condition of (2.3b) at  $\alpha = \alpha_0^*$  which fixes the correction term

$$\lambda_1(\alpha_0^*) = \lambda_0(\alpha_0^*) \frac{\int_{-1}^1 \frac{u_{0\alpha}}{(1+u_0)^m} dx \Big|_{\alpha=\alpha_0^*}}{\int_{-1}^1 \frac{u_{0\alpha}}{(1+u_0)^2} dx \Big|_{\alpha=\alpha_0^*}} = \lambda_0(\alpha_0^*) \frac{I_1}{I_2} \quad (2.5)$$

in terms of the two integrals  $I_1$  and  $I_2$  give rise to the two term expansion. These integrals are easily evaluated numerical by first noticing that

$$I_1 = -\frac{\partial}{\partial \alpha} \left[ \int_{-1}^1 \frac{dx}{(m-1)(1+u_0)^{m-1}} \right]_{\alpha=\alpha_0^*}, \quad I_2 = -\frac{\partial}{\partial \alpha} \left[ \int_{-1}^1 \frac{dx}{(1+u_0)} \right]_{\alpha=\alpha_0^*}.$$

The values of the correction  $\lambda_1(\alpha_0^*)$  are given in Table. 1 for several  $m$ .

**Principal Result 1** *In the limit as  $\varepsilon \rightarrow 0$ , the principal fold points  $\lambda^*$  of the equilibrium problems (1.2) admits the two term expansion*

$$\lambda^*(\varepsilon) = \lambda_0(\alpha_0^*) + \varepsilon^{m-2} \lambda_1(\alpha_0^*) + \mathcal{O}(\varepsilon^{2(m-2)}), \quad (2.6)$$

where  $(\lambda_0(\alpha_0^*), \alpha_0^*)$  and  $\lambda_1(\alpha_0^*)$  represent the principal fold point of the unperturbed problem and its correction respectively. The numerical value of  $(\lambda_0(\alpha_0^*), \alpha_0^*)$  is given in (2.4) while  $\lambda_1(\alpha_0^*)$  is given by (2.5).

As an example of Principal Result 1 in the case  $m = 4$ , the fold point  $\lambda^*$  has the expansion

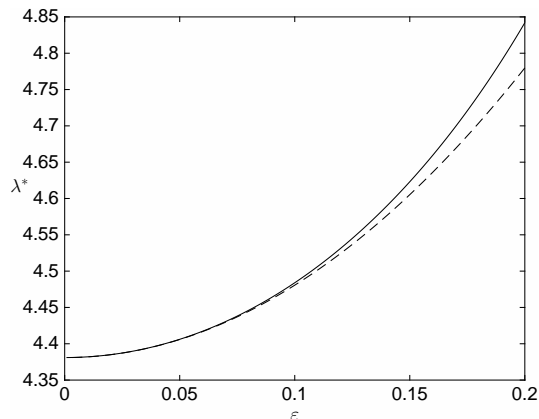
$$\begin{aligned} \lambda^* &= \lambda_0(\alpha_0^*) + \lambda_1(\alpha_0^*) \varepsilon^2 + \mathcal{O}(\varepsilon^4) \\ &= 4.3809 + 9.9690 \varepsilon^2 + \mathcal{O}(\varepsilon^4). \end{aligned} \quad (2.7)$$

In Fig. 4, the agreement between the expansion (2.7) and the full numerical calculation of the fold point is plotted.

### 3 Asymptotics of the secondary fold point

In this section, we construct the solutions to the steady state deflection problem (1.2) in the vicinity of the second saddle node bifurcation point  $\lambda_*$ . This second fold point is located at the end of the unstable branch emanating from the principal fold point. In contrast to the regular expansions developed in section Sec. 2, a singular perturbation will be required as the fold point  $(\lambda_*, \alpha_*)$  is not present in the  $\varepsilon = 0$  case. The calculation of this secondary bifurcation point allows us to estimate that equations (1.2) are bistable on the range

$$\lambda_*(\varepsilon) < \lambda < \lambda^*(\varepsilon). \quad (3.1)$$



**Fig. 4** A comparison of the asymptotic (dashed) and numerical (solid) predictions for the principal fold point of (2.7) in the case  $m = 4$ .

In addition, the system is predicted to lose bi-stability for  $\varepsilon > \varepsilon_c$  where  $\varepsilon_c$  is defined implicitly by  $\lambda_*(\varepsilon_c) = \lambda^*(\varepsilon_c)$ . The calculation of  $\lambda_*(\varepsilon)$  requires systematic use of switchback terms to obtain a well ordered expansion in the limit as  $\varepsilon \rightarrow 0^+$ .

In the vicinity of  $\lambda_*$  we stipulate that  $u(0) = -1 + \varepsilon\alpha$  where  $\alpha = \mathcal{O}(1)$  and obtain the parameterized bifurcation curve  $(\lambda(\alpha; \varepsilon), \|u(\alpha; \varepsilon)\|_2)$  in the limit where  $\varepsilon \rightarrow 0^+$ . We assume that  $\lambda(\varepsilon) \rightarrow 0$  as  $\varepsilon \rightarrow 0^+$ , so that in terms of some  $\nu(\varepsilon) \ll 1$ ,

$$\lambda(\varepsilon) \sim \nu(\varepsilon)\lambda_0 + \dots \quad (3.2)$$

Since  $u_\varepsilon$  is even in  $x$ , we restrict (1.2) to  $0 < x < 1$  and impose the symmetry conditions  $u_x(0) = u_{xxx}(0) = 0$ . In the outer region for  $0 < x < 1$ , we expand the solution as

$$u(x; \varepsilon) \sim u_0(x) + \nu(\varepsilon)u_1(x) + \dots \quad (3.3)$$

From (3.3) and (1.2), we obtain on  $0 < x < 1$  that

$$u_{0xxxx} = 0, \quad 0 < x < 1; \quad u_0(1) = u_{0x}(1) = 0, \quad (3.4a)$$

$$u_{1xxxx} = -\frac{\lambda_0}{(1+u_0)^2}, \quad 0 < x < 1; \quad u_1(1) = u_{1x}(1) = 0. \quad (3.4b)$$

For (3.4a), we impose the point constraints  $u_0(0) = -1$  and  $u_{0x}(0) = 0$  in order to match to an inner solution below. This determines  $u_0(x)$  as

$$u_0(x) = -1 + 3x^2 - 2x^3. \quad (3.5)$$

Since  $u_{0xxx}(0) \neq 0$ ,  $u_0$  does not satisfy the symmetry condition  $u_{xxx}(0) = 0$ . Thus, we need an inner layer near  $x = 0$ .

Upon substituting (3.5) into (3.4b), we obtain for  $x \ll 1$  that

$$u_{1xxxx} = -\frac{\lambda_0}{(3x^2 - 2x^3)^2} = -\frac{\lambda_0}{9x^4} \left(1 - \frac{2x}{3}\right)^{-2} = -\frac{\lambda_0}{9x^4} \left(1 + \frac{4x}{3} + \frac{12x^2}{9} + \dots\right).$$

Then, by integrating this limiting relation, we obtain the local behavior

$$u_1 \sim \frac{\lambda_0}{54} \log x - \frac{2\lambda_0}{27} x \log x + c_1 + b_1 x + \mathcal{O}(x^2 \log x), \quad \text{as } x \rightarrow 0, \quad (3.6)$$

in terms of constants  $c_1$  and  $b_1$  to be fixed. The determination of these constants then specifies the homogeneous component of the solution to  $u_1$ . From (3.3), (3.5), and (3.6), we obtain that

$$u(x; \varepsilon) \sim -1 + 3x^2 - 2x^3 + \nu \left( \frac{\lambda_0}{54} \log x - \frac{2\lambda_0}{27} x \log x + c_1 + b_1 x + \mathcal{O}(x^2 \log x) \right) + \dots, \quad \text{as } x \rightarrow 0. \quad (3.7)$$

By introducing the inner variable  $y = x/\gamma$ , we have to leading order from (3.7) that  $u \sim -1 + 3\gamma^2 y^2 + \dots$  as  $x \rightarrow 0$ . Since  $u = -1 + \mathcal{O}(\varepsilon)$  in the inner region, this motivates the scaling  $\gamma = \varepsilon^{\frac{1}{2}}$  and the definition of local variables  $y$  and  $w(y)$  where

$$y = \frac{x}{\varepsilon^{\frac{1}{2}}}, \quad u = -1 + \varepsilon w(y). \quad (3.8)$$

Next, we balance the cubic term  $-2x^3$  in (3.7) with the  $\mathcal{O}(\nu)$  term in (3.7) to get  $\nu = \varepsilon^{\frac{3}{2}}$ . Then, we substitute (3.8) and  $\lambda(\varepsilon) \sim \varepsilon^{\frac{3}{2}}\lambda_0$  into (1.2), to obtain that  $w(y)$  satisfies

$$-w_{yyyy} = \lambda_0 \varepsilon^{\frac{1}{2}} \left[ \frac{1}{w^2} - \frac{1}{w^m} \right], \quad y > 0; \quad w(0) = \alpha, \quad w_y(0) = w_{yyy}(0) = 0. \quad (3.9)$$

To determine the correct expansions for the inner and outer solutions, we write the local behavior of the outer expansion in (3.7) in terms of the inner variable  $x = \varepsilon^{\frac{1}{2}}y$ , with  $\nu = \varepsilon^{\frac{3}{2}}$ , to get

$$\begin{aligned} u(x; \varepsilon) = & -1 + 3\varepsilon y^2 + \left( \varepsilon^{\frac{3}{2}} \log \varepsilon \right) \frac{\lambda_0}{108} + \varepsilon^{\frac{3}{2}} \left( -2y^3 + \frac{\lambda_0}{54} \log y + c_1 \right) + (-\varepsilon^2 \log \varepsilon) \frac{\lambda_0}{27} y \\ & + \varepsilon^2 \left[ -\frac{2\lambda_0}{27} y \log y + b_1 y \right] + \mathcal{O}(\varepsilon^{\frac{5}{2}} \log \varepsilon). \end{aligned} \quad (3.10)$$

The terms of order  $\mathcal{O}(\varepsilon^{\frac{3}{2}} \log \varepsilon)$  and order  $\mathcal{O}(\varepsilon^2 \log \varepsilon)$  must be accounted for with *switchback terms* in the outer expansion. In addition, the  $\mathcal{O}(\varepsilon)$  term in (3.10), enables us to conclude that (3.9) should admit the expansion  $w \sim w_0 + o(1)$ , where  $w_0$  satisfies

$$w_{0yyyy} = 0, \quad y > 0; \quad w_0(0) = \alpha, \quad w_{0y}(0) = w_{0yyy}(0) = 0; \quad w_0 \sim 3y^2 \quad \text{as } y \rightarrow \infty. \quad (3.11a)$$

This problem has the exact solution

$$w_0 = 3y^2 + \alpha. \quad (3.11b)$$

The constant term in (3.11b) then generates the unmatched term  $\varepsilon$  in the outer region, which can only be removed by introducing a second switchback term into the outer expansion. This suggests that  $\lambda(\varepsilon)$ , and the outer expansion for  $u(x; \varepsilon)$ , must have the form

$$u(x; \varepsilon) = u_0 + \varepsilon u_{\frac{1}{2}} + \left( \varepsilon^{\frac{3}{2}} \log \varepsilon \right) u_{\frac{3}{2}} + \varepsilon^{\frac{3}{2}} u_1 + \dots, \quad \lambda(\varepsilon) = \varepsilon^{\frac{3}{2}} \lambda_0 + \varepsilon^2 \lambda_1 + \dots. \quad (3.12)$$

Upon substituting (3.12) into (1.2), and collecting similar terms in  $\varepsilon$ , we obtain that  $u_{\frac{1}{2}}$  satisfies

$$u_{\frac{1}{2}xxxx} = 0, \quad 0 < x < 1; \quad u_{\frac{1}{2}}(0) = \alpha, \quad u_{\frac{1}{2}x}(0) = b_{\frac{1}{2}}, \quad u_{\frac{1}{2}}(1) = u_{\frac{1}{2}x}(1) = 0, \quad (3.13a)$$

where  $b_{\frac{1}{2}}$  is a constant to be found. The condition  $u_{\frac{1}{2}}(0) = \alpha$  accounts for the constant term in  $w_0$ . The solution is

$$u_{\frac{1}{2}}(x) = \alpha + b_{\frac{1}{2}} x + \left( -3 - 2b_{\frac{1}{2}} \right) x^2 + \left( b_{\frac{1}{2}} + 2 \right) x^3. \quad (3.13b)$$

Similarly,  $u_{\frac{3}{2}}(x)$  satisfies  $u_{\frac{3}{2}xxxx} = 0$ . To eliminate the  $\mathcal{O}(\varepsilon^{\frac{3}{2}} \log \varepsilon)$  and  $\mathcal{O}(\varepsilon^2 \log \varepsilon)$  terms in (3.10), we let  $u_{\frac{3}{2}}$  satisfy

$$u_{\frac{3}{2}xxxx} = 0, \quad 0 < x < 1; \quad u_{\frac{3}{2}}(0) = -\frac{\lambda_0}{108}, \quad u_{\frac{3}{2}x}(0) = \frac{\lambda_0}{27}, \quad u_{\frac{3}{2}}(1) = u_{\frac{3}{2}x}(1) = 0. \quad (3.14a)$$

The solution for  $u_{\frac{3}{2}}$  is

$$u_{\frac{3}{2}} = \lambda_0 \left( -\frac{1}{108} + \frac{x}{27} - \frac{5x^2}{108} + \frac{x^3}{54} \right). \quad (3.14b)$$



We then substitute (3.5), (3.6), (3.13b), (3.14b), for  $u_0$ ,  $u_1$ ,  $u_{\frac{1}{2}}$ , and  $u_{\frac{3}{2}}$  respectively, into the outer expansion (3.12), and write the resulting expression in terms of the inner variable  $x = \varepsilon^{\frac{1}{2}}y$ . This yields the following behavior for  $u(x; \varepsilon)$  as  $y \rightarrow \infty$ :

$$\begin{aligned} u(x; \varepsilon) \sim & -1 + \varepsilon (3y^2 + \alpha) + \varepsilon^{\frac{3}{2}} \left( -2y^3 + \frac{\lambda_0}{54} \log y + b_{\frac{1}{2}}y + c_1 \right) \\ & + \varepsilon^2 \left( -(3 + 2b_{\frac{1}{2}})y^2 - \frac{2\lambda_0}{27}y \log y + b_1y + \dots \right). \end{aligned} \quad (3.15)$$

As  $u = -1 + \varepsilon w(y)$  in the inner region, behavior (3.15) suggests the inner solution be expanded as

$$w = w_0 + \varepsilon^{\frac{1}{2}}w_1 + \varepsilon w_2 + \dots. \quad (3.16)$$

Upon substituting (3.16) and (3.12) for  $\lambda(\varepsilon)$  into (3.9), we obtain that  $w_0$  satisfies (3.11), and that  $w_1, w_2$  solve

$$w_{1yyy} = -\frac{\lambda_0}{w_0^2} + \frac{\lambda_0}{w_0^m}, \quad y > 0; \quad w_1(0) = w_{1y}(0) = w_{1yyy}(0) = 0, \quad (3.17a)$$

$$w_1 \sim -2y^3 + \frac{\lambda_0}{54} \log y + b_{\frac{1}{2}}y + c_1 + \dots, \quad \text{as } y \rightarrow \infty, \quad (3.17b)$$

$$w_{2yyy} = \left[ \frac{2\lambda_0}{w_0^3} - \frac{m\lambda_0}{w_0^{m+1}} \right] w_1 - \frac{\lambda_1}{w_0^2} + \frac{\lambda_1}{w_0^m}, \quad y > 0; \quad w_2(0) = w_{2y}(0) = w_{2yyy}(0) = 0, \quad (3.18a)$$

$$w_2 \sim -(3 + 2b_{\frac{1}{2}})y^2 - \frac{2\lambda_0}{27}y \log y + b_1y + \dots, \quad \text{as } y \rightarrow \infty. \quad (3.18b)$$

The solution to these problems determine  $\lambda_0$ ,  $\lambda_1$ ,  $b_{\frac{1}{2}}$  and  $c_1$  as is now shown. The value of  $\lambda_0$  is first calculated by integrating (3.17a) over  $(0, \infty)$  to give

$$\begin{aligned} 12 &= \lambda_0 \left[ \int_0^\infty \frac{dy}{(\alpha + 3y^2)^2} - \int_0^\infty \frac{dy}{(\alpha + 3y^2)^m} \right] = \lambda_0 \sqrt{\frac{\alpha}{3}} \left[ \frac{\pi}{4\alpha^2} + \frac{1}{\alpha^m} \int_0^{\frac{\pi}{2}} [\cos u]^{2(m-1)} du \right] \\ &= \frac{\lambda_0}{\sqrt{3}} \left[ \frac{\pi}{4\alpha^{\frac{3}{2}}} - \frac{\sqrt{\pi}}{2\alpha^{m-\frac{1}{2}}} \frac{\Gamma(m-\frac{1}{2})}{\Gamma(m)} \right] \quad [y = \sqrt{\alpha/3} \tan u]. \end{aligned}$$

which leads to the expression for  $\lambda_0$

$$\lambda_0 = 12\sqrt{3} \left[ \frac{\pi}{4\alpha^{\frac{3}{2}}} - \frac{\sqrt{\pi}}{2\alpha^{m-\frac{1}{2}}} \frac{\Gamma(m-\frac{1}{2})}{\Gamma(m)} \right]^{-1}, \quad m > 2. \quad (3.19)$$

Here  $\Gamma(z) = \int_0^\infty x^{z-1} e^{-x} dx$ . The correction term  $\lambda_1$  is calculated from (3.18) by integrating (3.18a) over  $0 < y < \infty$ , and then applying  $w_{2yyy} \rightarrow 0$  as  $y \rightarrow \infty$ , with  $w_0 = \alpha + 3y^2$ . This yields that

$$\lambda_1 = \frac{\lambda_0^2}{12} \int_0^\infty \left[ \frac{2}{(\alpha + 3y^2)^3} - \frac{m}{(\alpha + 3y^2)^{m+1}} \right] w_1 dy. \quad (3.20)$$

This integral can be explicitly evaluated by solving for the exact solution  $w_1(y)$  of (3.17). The first step is to calculate  $w_{1yy}(0)$  and then formulate (3.17) as an initial value ODE problem for  $w_1$ . To do so, we multiply (3.17a) by  $w_{0y}$ , integrate over  $0 < y < R$ , then pass to the limit as  $R \rightarrow \infty$ , to obtain

$$\lim_{R \rightarrow \infty} \int_0^R w_{0y} w_{1yyy} dy = \lim_{R \rightarrow \infty} (w_{0y} w_{1yyy} - w_{0yy} w_{1yy}) \Big|_0^R + \lim_{R \rightarrow \infty} \int_0^R w_{1yy} w_{0yyy} dy = 6w_{1yy}(0).$$

On the other hand,

$$-\lambda_0 \lim_{R \rightarrow \infty} \int_0^R \frac{w_{0y}}{w_0^2} - \frac{w_{0y}}{w_0^m} dy = \lambda_0 \left( \frac{1}{w_0} - \frac{1}{(m-1)w_0^{m-1}} \right) \Big|_{y=0}^\infty = 6w_{1yy}(0). \quad (3.21)$$

Since  $w_0(0) = \alpha$ , this yields that

$$w_{1yy}(0) = \frac{\lambda_0[1 - (m-1)\alpha^{m-2}]}{6(m-1)\alpha^{m-1}},$$

which together with the initial values  $w_1(0) = w_{1y}(0) = w_{1yyy}(0) = 0$ , allows the initial value problem (3.17) to be solved for  $w_1$ . A closed form of  $w_1$  is available in terms of hypergeometric functions, though for general  $m > 2$  it is quite cumbersome. For the particular value  $m = 4$  for example, the solution is

$$w_1 = \frac{-\lambda_0}{864\alpha^{\frac{7}{2}}} \left[ 3\sqrt{3}y \tan^{-1} \left( \sqrt{\frac{3}{\alpha}}y \right) \left[ 8\alpha^3 - \alpha + y^2(8\alpha^2 - 5) \right] \right. \\ \left. + y^2(24\alpha^{\frac{5}{2}} - 15\alpha^{\frac{1}{2}}) - 8\alpha^{\frac{7}{2}} \log \left( 1 + \frac{3y^2}{\alpha} \right) \right] \quad (3.22)$$

The constants  $b_{\frac{1}{2}}$  and  $c_1$  are determined by applying the large argument expansion  $\tan^{-1}(y) \sim \pi/2 - y^{-1} + (3y^3)^{-1}$  for  $y \rightarrow \infty$  to (3.22) and comparing to (3.17b) to obtain for  $m = 4$  that

$$c_1 = \frac{2\lambda_0}{81} - \frac{\lambda_0}{648\alpha^2} + \frac{\lambda_0 \log \frac{3}{\alpha}}{108}, \quad b_{\frac{1}{2}} = \frac{2\alpha(1 - 8\alpha^2)}{8\alpha^2 - 5}. \quad (3.23)$$

The exact expression for  $w_1$  in (3.22) allows  $\lambda_1$  to be calculated by directly evaluating the integral (3.20). In this way, the formula for the case  $m = 4$

$$\lambda_1 = 2\lambda_0^2 \left[ \frac{-595 + 32\alpha^2[235 - 210 \log 2 + 48\alpha^2(3 \log 2 - 4)]}{41472\alpha^3(8\alpha^2 - 5)} \right], \quad (3.24)$$

is found. For completeness, we remark that  $b_1$  from (3.18b) is uniquely determined by first multiplying (3.18a) by  $w_0$  followed by integrating over  $(0, R)$  and evaluation of the limit  $R \rightarrow \infty$ . The details are omitted as the value of  $b_1$  does not contribute to the location of the saddle node  $\lambda_*$  at this order.

Briefly summarizing the calculation so far, we have that in the vicinity of the saddle node bifurcation, the solution branch has parameterization

$$u(0) = -1 + \varepsilon\alpha, \quad \lambda \sim \varepsilon^{\frac{3}{2}}\lambda_0(\alpha) + \varepsilon^2\lambda_1(\alpha) + \dots,$$

The saddle-node bifurcation point  $(\alpha_*, \lambda_*)$  is located by the condition  $\lambda_\alpha(\alpha_*) = 0$  to be

$$\lambda_* = \lambda(\alpha_*) = \varepsilon^{\frac{3}{2}}\lambda_0(\alpha_{*0}) + \varepsilon^2\lambda_1(\alpha_{*0}) + \dots$$

where the fold point is fixed by the condition  $\lambda_\alpha(\alpha_*) = 0$  and  $\alpha_{*0}$  is determined by

$$\lambda_{0\alpha}(\alpha_{*0}) = 0. \quad (3.25)$$

The values of  $\alpha_{*0}$  and  $\lambda_0(\alpha_{*0})$  are

$$\alpha_{*0} = \left[ \frac{4(m - \frac{1}{2}) \Gamma(m - \frac{1}{2})}{3\sqrt{\pi} \Gamma(m)} \right]^{\frac{1}{m-2}}, \quad \lambda_0(\alpha_{*0}) = \frac{48\sqrt{3}}{\pi} \frac{(m - \frac{1}{2})}{(m - 2)} \alpha_{*0}^{\frac{3}{2}}. \quad (3.26)$$

The correction term  $\lambda_1(\alpha_{*0})$  is more difficult to express in a closed form expression for general  $m$  as this requires solution of (3.17) followed by integration of (3.20). We therefore provide in Table 2, closed form expressions for these higher order corrections for selected values of  $m$ .

The preceding calculations are now summarized:

$m$	$\alpha_{*0}$	$\lambda_0(\alpha_{*0})$	$\lambda_1(\alpha_{*0})$
3	$\frac{5}{4}$	$\frac{75\sqrt{15}}{\pi}$	$-\frac{5625}{8\pi^2}$
4	$\left(\frac{35}{24}\right)^{\frac{1}{2}}$	$\frac{7}{\pi} \left(\frac{105^3}{2}\right)^{\frac{1}{4}}$	$-\frac{26411}{64\pi^2}$
5	$\left(\frac{105}{64}\right)^{\frac{1}{3}}$	$\frac{27\sqrt{35}}{\pi}$	$-\frac{1143}{16\pi^2} \left(\frac{21^2}{5}\right)^{\frac{1}{3}}$

**Table 2** Explicit expressions for terms of the asymptotic expansion of the saddle-node fold point  $(\lambda_*, \alpha_*)$  for  $m = 3, 4, 5$ .

**Principal Result 2** *In the vicinity of the secondary fold point  $\lambda_*$ , solutions of (1.2) admit the parameterization*

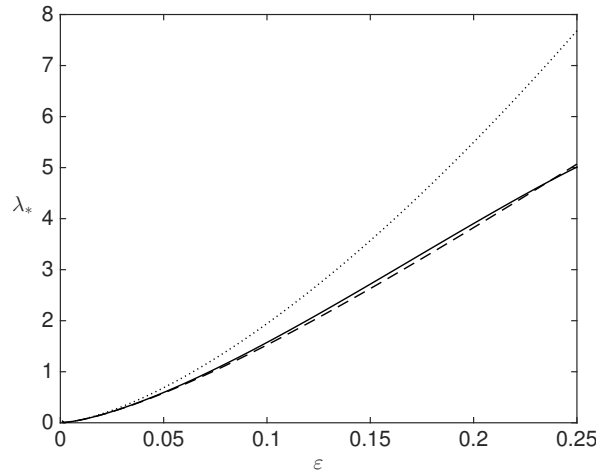
$$u(0) = -1 + \varepsilon \alpha, \quad \lambda(\varepsilon) \sim \lambda_0(\alpha) \varepsilon^{\frac{3}{2}} + \lambda_1(\alpha) \varepsilon^2 + \dots \quad (3.27a)$$

where  $\lambda_0$  and  $\lambda_1$  are given in (3.19) and (3.20) respectively. In the limit as  $\varepsilon \rightarrow 0$ , a two term expansion for  $\lambda_*$  is given by

$$\lambda_* \sim \lambda_0(\alpha_{*0}) \varepsilon^{\frac{3}{2}} + \lambda_1(\alpha_{*0}) \varepsilon^2 + \dots \quad (3.27b)$$

where values of  $\alpha_{*0}$ ,  $\lambda_0(\alpha_{*0})$ ,  $\lambda_1(\alpha_{*0})$  are given by (3.26) and (3.20). For selected values of  $m$ , explicit expressions for these thresholds are given in Table 2. For example, in the case  $m = 4$ , we have that

$$\begin{aligned} \lambda_* &\sim \frac{7}{\pi} \left(\frac{105^3}{2}\right)^{\frac{1}{4}} \varepsilon^{\frac{3}{2}} - \frac{26411}{64\pi^2} \varepsilon^2 + \dots \\ &\sim 61.4586 \varepsilon^{\frac{3}{2}} - 41.8124 \varepsilon^2 + \dots \end{aligned} \quad (3.27c)$$



**Fig. 5** Numerical validation of Principal Result 2. Comparison of  $\lambda_*$  from one term asymptotic (dotted), two term asymptotic (dashed) and numerical (solid) approximations.

### 3.1 Prediction of the bistable region.

The analysis of the previous sections has focussed on accurately determining two saddle-node bifurcation points,  $\lambda^*(\varepsilon)$  and  $\lambda_*(\varepsilon)$ . When combined, these two values predict that equations (1.2) are bistable on the range

$$\lambda_*(\varepsilon) < \lambda < \lambda^*(\varepsilon). \quad (3.28)$$

In terms of the expressions derived in Principal Results 1 and 2 for  $\lambda^*(\varepsilon)$  and  $\lambda_*(\varepsilon)$  respectively, the bistable region for the case  $m = 4$  is predicted to be

$$61.4586 \varepsilon^{\frac{3}{2}} - 41.8124 \varepsilon^2 < \lambda < 4.3809 + 9.9713 \varepsilon^2. \quad (3.29)$$

A heuristic prediction of  $\varepsilon_c$ , the threshold for bi-stability can be obtained by solving the equation  $\lambda_*(\varepsilon_c) = \lambda^*(\varepsilon_c)$  for each of the above cases. These predictions are encapsulated in the following Principal Result

**Principal Result 3** *The asymptotic formulation (3.29) for the fold points  $\lambda^*(\varepsilon)$  and  $\lambda_*(\varepsilon)$  associated with the equilibrium problems (1.2) coalesce at  $\varepsilon_c$  where asymptotic and numerical estimates of  $\varepsilon_c$  are given by*

$$\begin{aligned} m = 3: & \quad \varepsilon_c \sim 0.2102 \quad (\text{Asymptotic}), & \quad \varepsilon_c \sim 0.2319 \quad (\text{Numerical}); \\ m = 4: & \quad \varepsilon_c \sim 0.2468 \quad (\text{Asymptotic}), & \quad \varepsilon_c \sim 0.2727 \quad (\text{Numerical}); \\ m = 5: & \quad \varepsilon_c \sim 0.2646 \quad (\text{Asymptotic}), & \quad \varepsilon_c \sim 0.3039 \quad (\text{Numerical}). \end{aligned}$$

Consequently, equation (1.2) is predicted to be bistable on the range  $0 < \varepsilon < \varepsilon_c$  and to admit a unique solution for each  $\lambda \geq 0$  whenever  $\varepsilon \geq \varepsilon_c$ .

In Principal Result 3, the cubic fold point  $(\alpha_c, \lambda_c)$ , corresponding to the threshold of bistability in (1.2), is located by numerical solution of the system

$$\begin{bmatrix} \lambda_\alpha(\alpha_c, \varepsilon_c) \\ \lambda_{\alpha\alpha}(\alpha_c, \varepsilon_c) \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}. \quad (3.30)$$

We remark that in Principal Result 3, agreement between the asymptotic and numerical results is quite close ( $\approx 10\%$ ), especially given that is is derived from the heuristic condition that the bistable range (3.29) shrinks to a point.

## 4 Conclusion

In this paper we have studied equilibrium states of the regularized model (1.1) which accounts for repulsive forces which become important when the gap spacing is very small. The problem of stiction is explained in this setting by the presence of bistability in this system when  $\varepsilon < \varepsilon_c$ . The main practical contribution of this work is a framework for accurately estimating the conditions for bistability in the system. Namely, for  $\varepsilon < \varepsilon_c$  the system is bistable on the parameter range  $\lambda_* < \lambda < \lambda^*$  and we have established accurate estimates of the three key thresholds  $\varepsilon_c$ ,  $\lambda_*$  and  $\lambda^*$  for  $m > 2$ .

There are many avenues of future investigation that arise from this work. It is highly desirable to rigorously verify the bistable nature of (1.1) and establish the existence of solutions for all  $m > 2$  and in higher dimensional settings. A study of stiction in the more practically relevant two-dimensional setting would reveal additional factors that contribute to stiction such as contact line energies and dependence on device geometry.

There are significant challenges which can be anticipated to arise in such an extension. First, the methods used (Sec. 3) to calculate  $\lambda_*$  require exact expressions for the singular limiting solution, which is essentially the Green's function for the bi-Laplacian. Such expressions are not available in higher dimensional settings except in the most simple situations. Progress can be made by employing a combination of exact knowledge of the singularity structure with numerical calculation of quantities associated with the associated regular part (cf. [30]). Second, in spatial dimension  $d = 2$  the singularity structure associated with the Green's function is  $r^2 \log r$ . This can be expected to generate a more complex asymptotic expansion for the fold point  $\lambda_*$ , featuring an infinite logarithmic series as  $\varepsilon \rightarrow 0$ . Such series are common in singular perturbation problems in two dimensions and unfortunately converge very slowly. An interesting problem would be to formulate a hybrid asymptotic numerical method (cf. [34, 35]) to accelerate this convergence and obtain accurate estimates of the bistability range of MEMS devices with a wide variety of geometries.

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