



On flow separation under stable conditions: results from flow visualization in MATERHORN-X

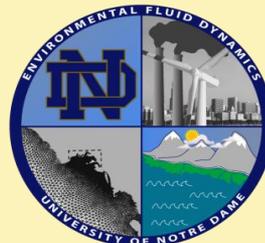
Michael Thompson

September 6th 2013 4:45pm

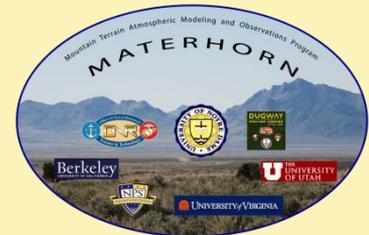
McKenna Hall, Notre Dame



University of
Notre Dame



Notre Dame
Environmental
Fluid Dynamics



MATERHORN

Overview



- [1] Quick Background: Dividing Streamline Concept
- [2] Site Location and Instrumentation
- [3] Goals and Procedure
- [4] Atmospheric Conditions during flow visualization
- [5] Smoke Visualization
- [6] Movie

Quick Background



Based on energy arguments:

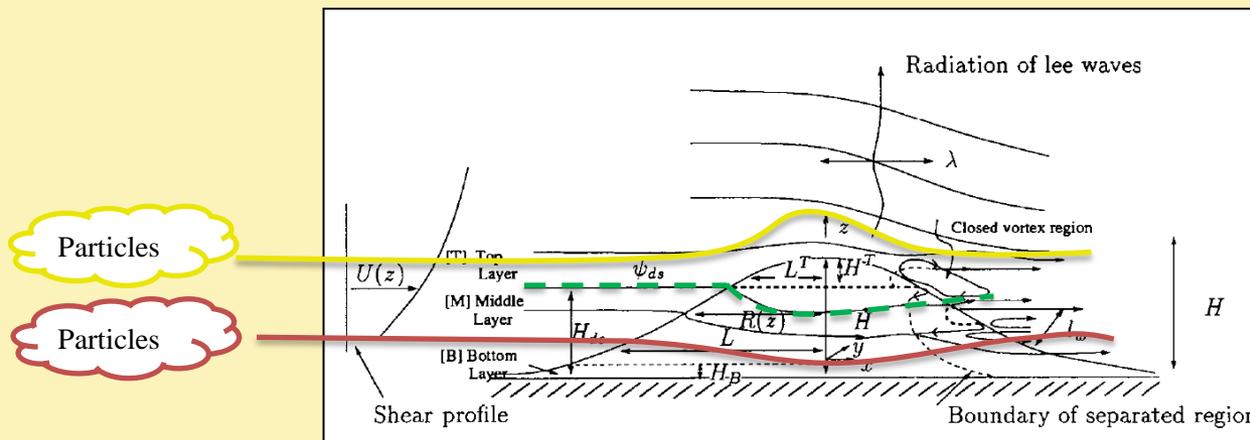
Sheppard (1956)

“Under what conditions will an airstream rise over a mountain range?”

Sheppard's Equation:
$$\underbrace{\frac{1}{2} \rho U_0^2(H_s)}_{\text{The kinetic energy of the parcel far upstream at elevation } H_s} = g \underbrace{\int_{H_s}^h (h - z) \left(-\frac{\partial \rho}{\partial z} \right) dz}_{\text{The potential energy gained by the parcel in being lifted from the dividing streamline } H, \text{ to the top of the hill } h \text{ through the density gradient } \partial \rho / \partial z} \quad \text{with} \quad Fr < 1$$

The kinetic energy of the parcel far upstream at elevation H_s

The potential energy gained by the parcel in being lifted from the dividing streamline H , to the top of the hill h through the density gradient $\partial \rho / \partial z$



Adopted from Hunt et al. (1997)

Dividing Streamline (ψ_{ds}): The streamline separating the top and middle regions of flow.

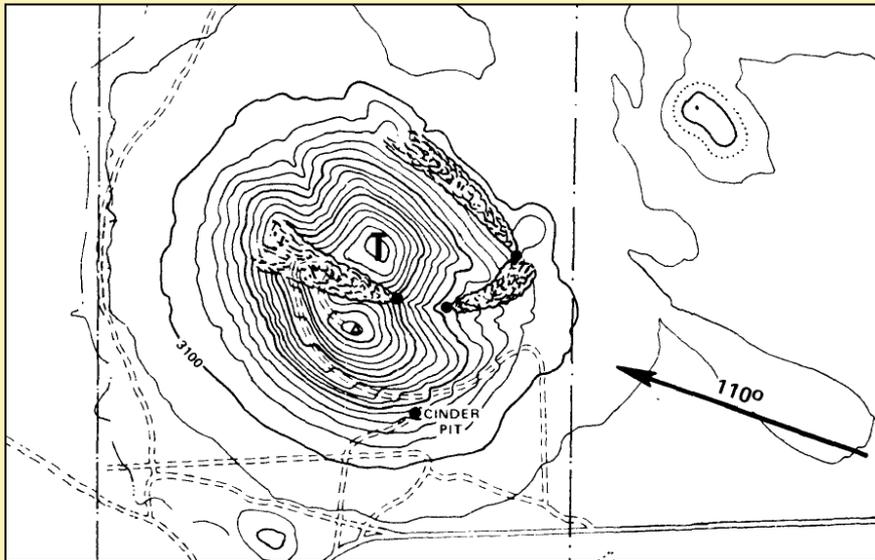
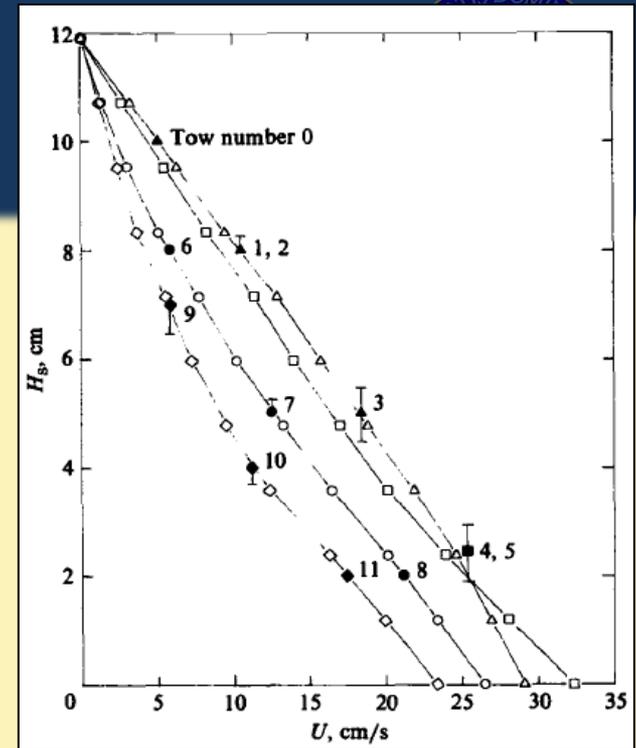
Dividing Streamline Height (H_{ds}): The height between the ground and ψ_{ds}

Quick Background

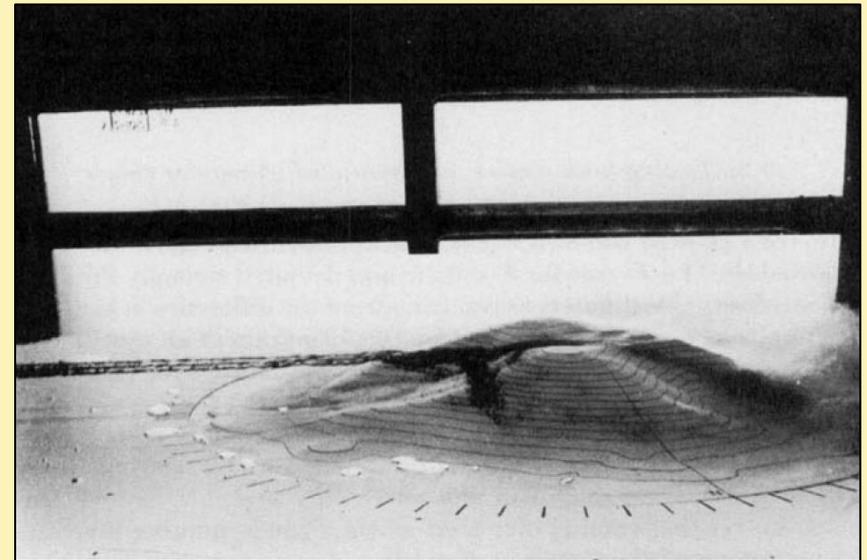
Cinder Cone Butte, ID

- Field experiment originally conducted by USEPA
- Modeled in stratified towing tank using salt gradients
 - Open symbols \Rightarrow Calculated values
 - Closed symbols \Rightarrow Observed values
- Sheppard's Equation can be simplified:

$$H_s = h(1 - Fr)$$

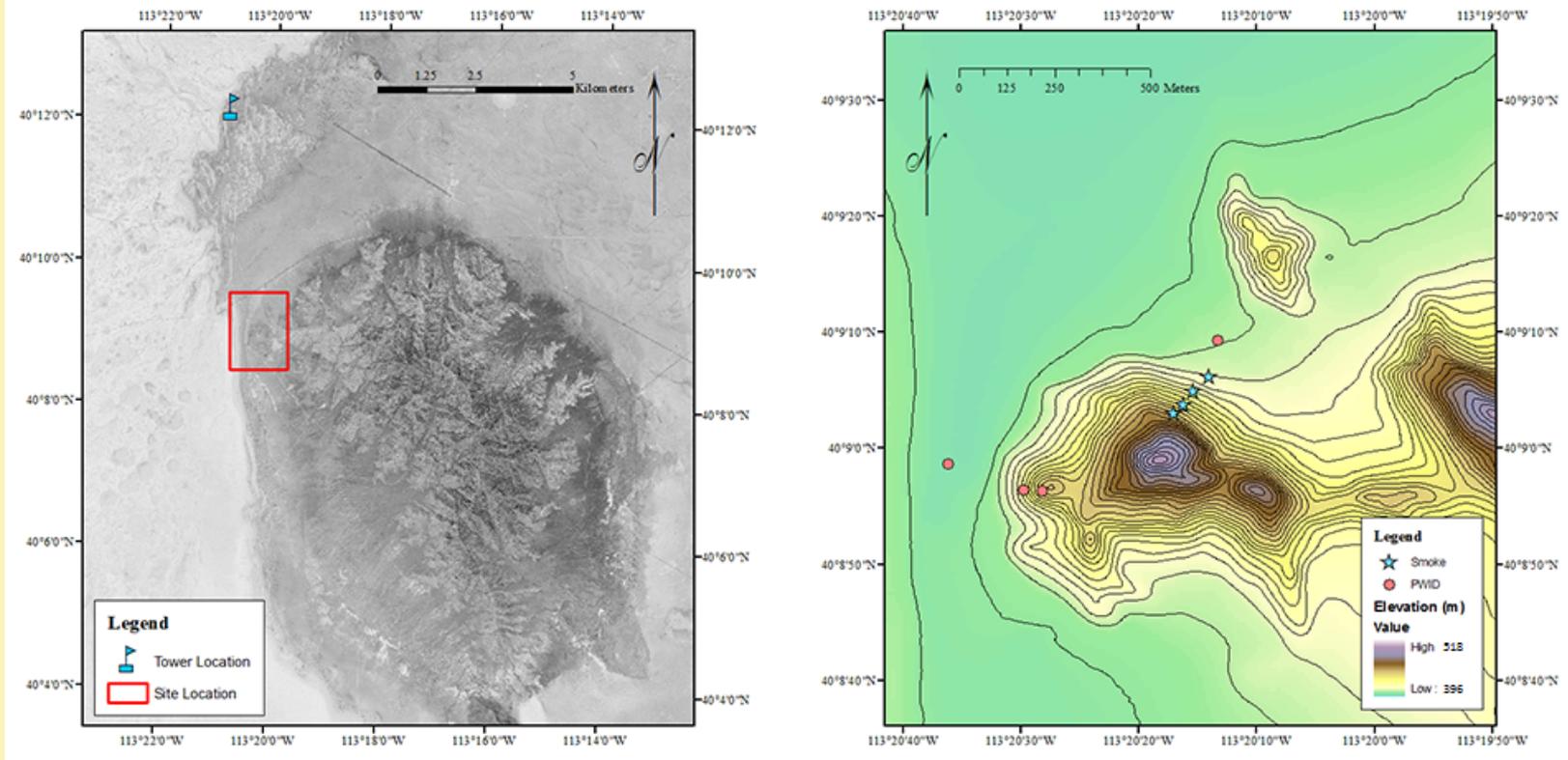


Adopted from Snyder et al. (1980)



Adopted from Snyder et al. (1985)

Site Location and Instrumentation



(Left) High resolution 1m orthoimagery of Granite Mountain, portraying the location of the instrumentation tower and smoke visualization site.
(Right) Ten times magnification of the smoke visualization site; the contours are presented at 5m intervals.

32m NW tower:

- 5 81000 R.M. Young ultrasonic sonic anemometers (20Hz sampling rate)

PWIDs:

- 05103 R.M. Young mechanical wind sensors
- Temperature and relative humidity probes

Goals and Procedure



Goals:

- Multiple smoke releases in time of stratified flow
- Capture with high quality photos and movies
- Be able to quantify observations using DSL concept

Procedure:

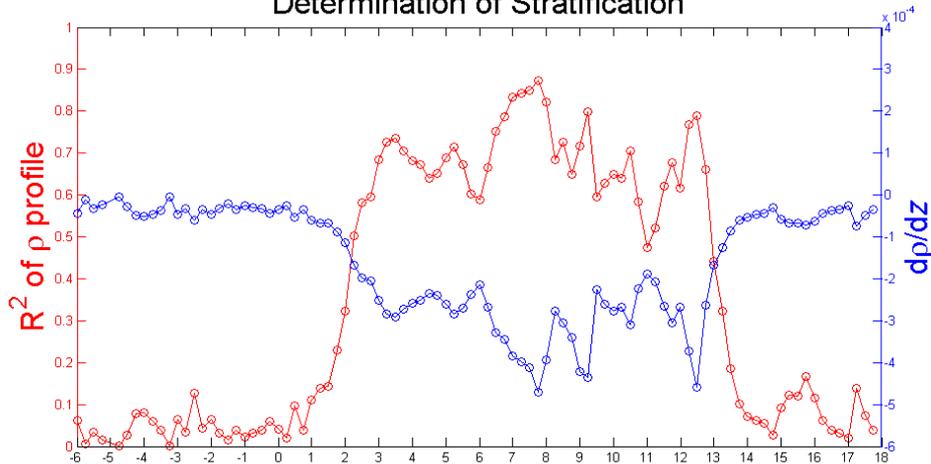
1. Wait for appropriate conditions
2. First smoke release
 - Red smoke canisters; (~1.5 min release)
 - 4 simultaneous ground releases (0.0h, 0.08h, 0.45h, 0.88h)
3. Second smoke release
 - Use crane for elevated release; observation of approaching streamline
 - White smoke canisters (~5 min release)
 - 3 simultaneous ground releases; 1 elevated release (~0.33h)



Atmospheric Conditions



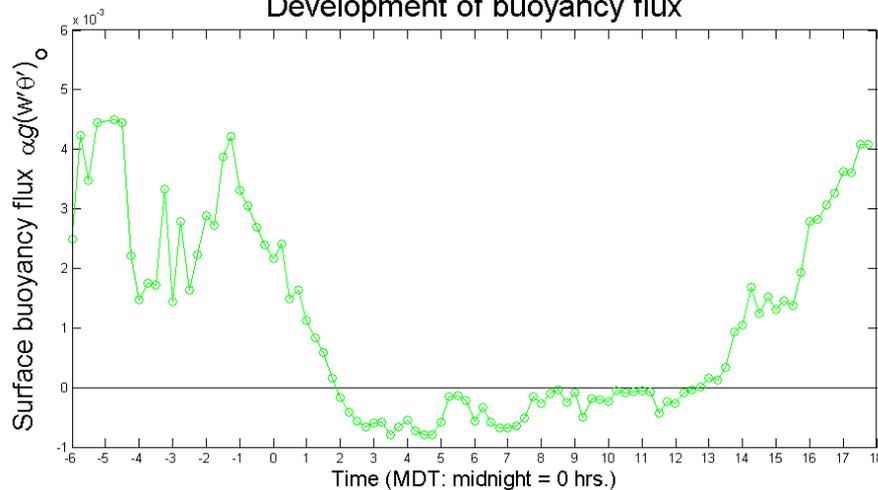
Determination of Stratification



Density profiles:

- Development of strong linear correlation by 3AM
- R^2 values reaching ~ 0.7 in the early morning
- Breakdown of linearity around noon

Development of buoyancy flux



Surface buoyancy flux:

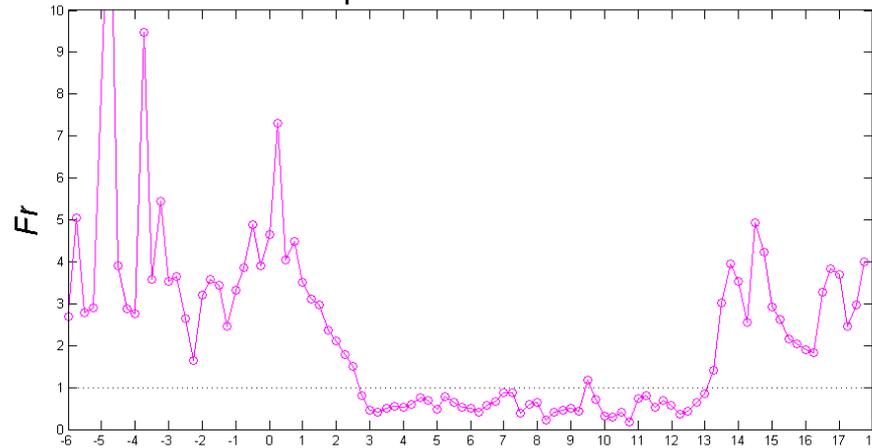
- **Positive** when surface is heated – convective overturning
- **Negative** when boundary layer tends to be stably stratified (reduce turbulent energy)

(Top) Linear regression coefficient of the density profile, calculated from the 32m sonic anemometers; corresponding density gradient strength.
(Bottom) Development of the buoyancy flux, as calculated from the tower sonic anemometer positioned 2m above the ground.

Atmospheric Conditions



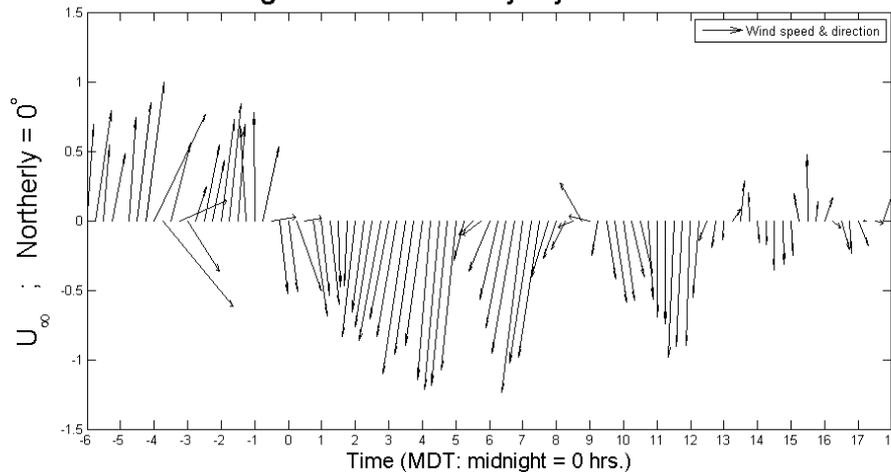
Development of Froude number



Froude number:

- During period of stratification, Fr drops within applicable range

Averaged 32m boundary layer wind direction

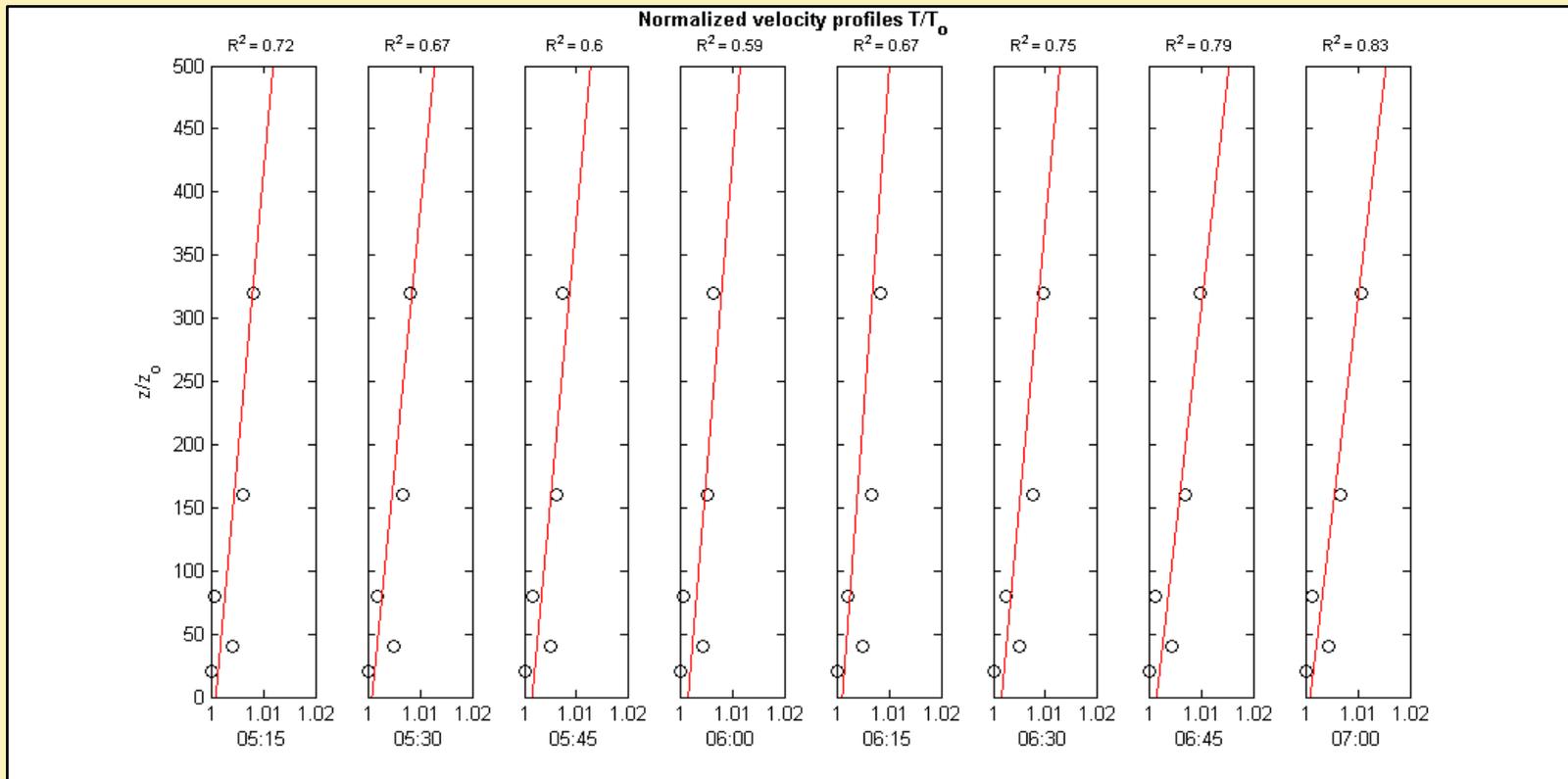


Wind Direction:

- During time of experiment, wind originating from the northeast $\sim 30^\circ$ at about 1 m/s

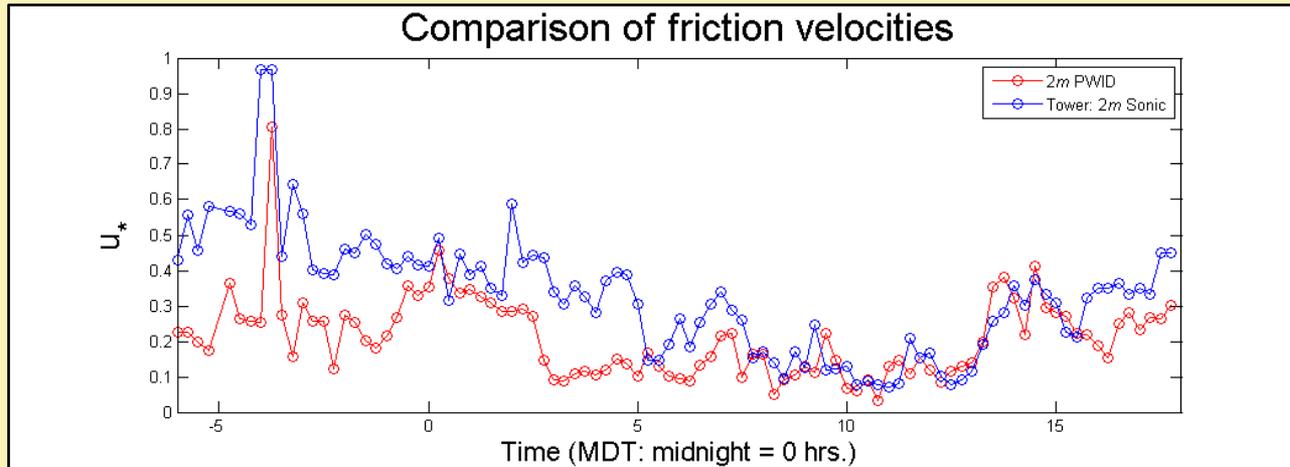
(Top) Linear regression coefficient of the density profile, calculated from the 32m sonic anemometers; corresponding density gradient strength.
(Bottom) Development of the buoyancy flux, as calculated from the tower sonic anemometer positioned 2m above the ground.

Temperature Profiles



- Temperature profiles normalized by T_0
- Show good stratification, with $0.67 < R^2 < 0.75$ around the time of flow visualizations

Velocity Profiles



Monin-Obukhov Similarity Theory (**MOST**):

$$\bar{u}(z) = \frac{u_*}{k} \ln\left(\frac{z}{z_o}\right) \quad \text{where} \quad u_* = ((\overline{u'w'^2}) + (\overline{v'w'^2}))^{\frac{1}{4}}$$

$$L_* = -\frac{u_*^3}{kq_o} \quad \text{where} \quad q_o = \alpha g \overline{(w'\theta')}_o \quad \text{and} \quad \alpha \approx \bar{\theta}^{-1}$$

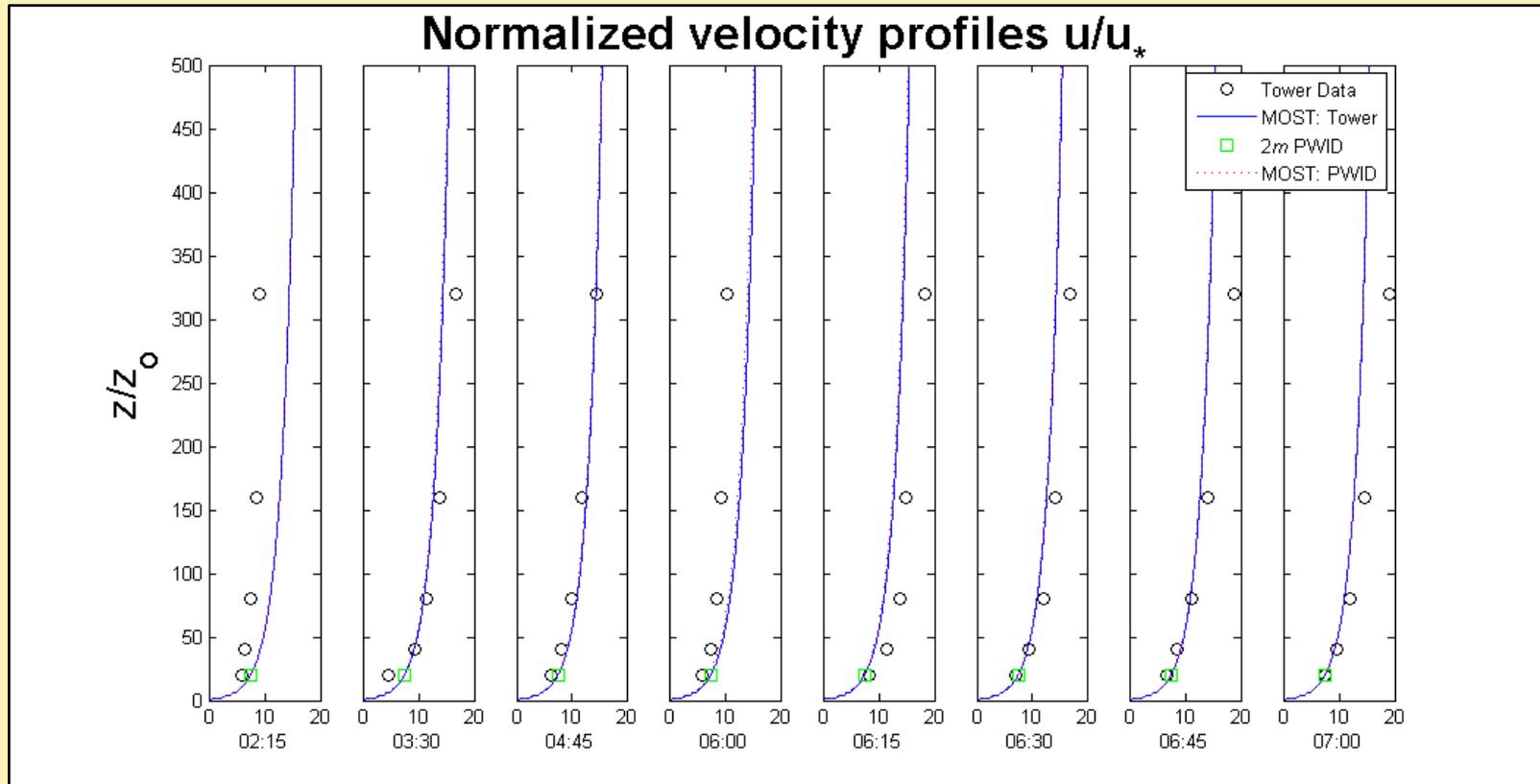
$$\xi = z/L_* \quad \text{and} \quad \xi_o = z_o/L_*$$

$$\phi_m = \begin{cases} (1 + 16|\xi|)^{-\frac{1}{4}}, & \text{for } -2 \leq \xi \leq 0 \\ (1 + 5\xi), & \text{for } 0 \leq \xi \leq 1 \end{cases}$$

$$\bar{u}(z) = \frac{u_*}{k} \ln\left(\frac{z}{z_o} - \Psi_m\right) \quad \text{where} \quad \Psi_m = \int_{\xi_o}^{\xi} \frac{(1 - \phi_m)}{\xi} d\xi$$

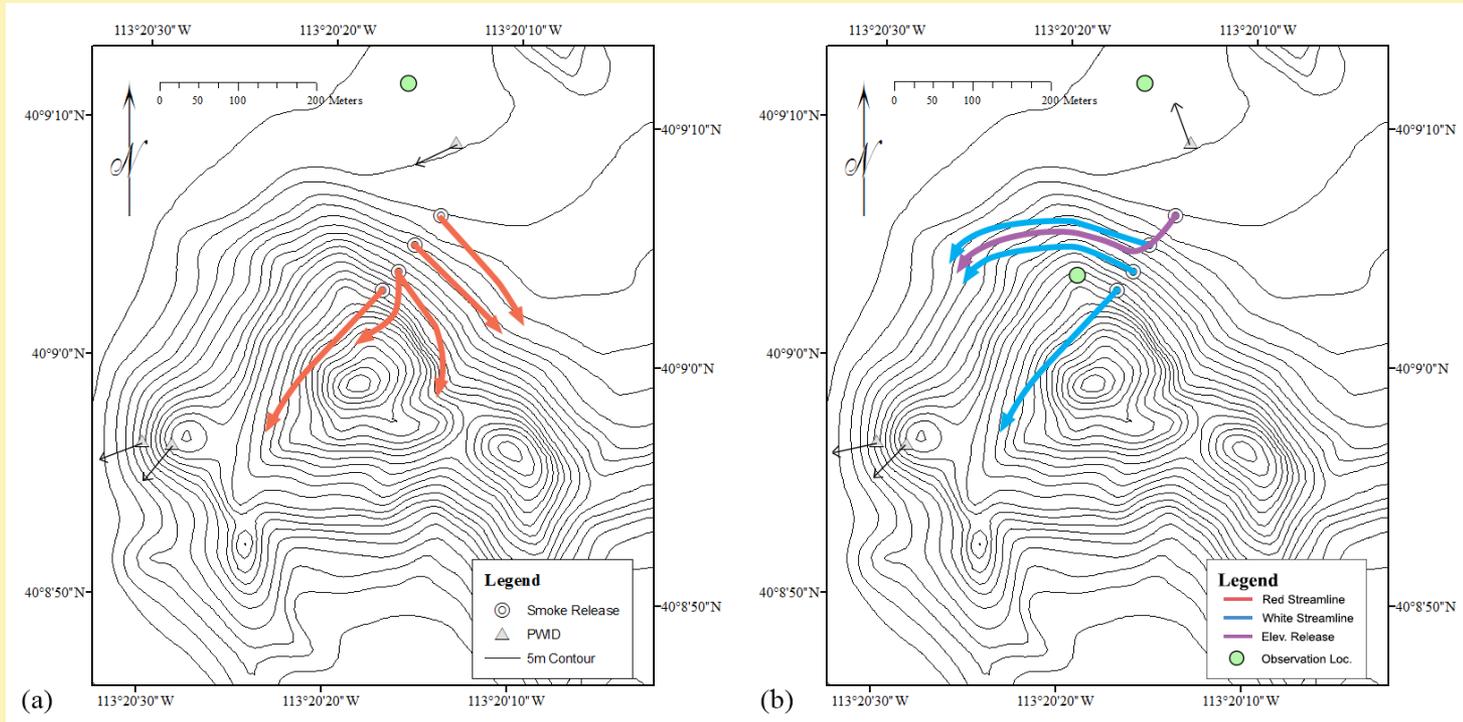
u_*	Friction velocity
z_o	Roughness height (0.10m)
k	Von Kármán constant (0.40)
$\overline{u'w'} \overline{v'w'}$	Surface kinematic momentum fluxes to represent the surface stress
L_*	Monin-Obukhov length scale
q_o	Surface buoyancy flux
α	Thermal expansion coefficient
θ	Potential temperature
$\overline{(w'\theta')}_o$	Mean temperature flux at the surface
ϕ_m	Stability function for wind shear
Ψ_m	Correction term

Velocity and Temp Profiles



- Tower data is normalized by the friction velocity computed from the Sonic Anemometer positioned at 2m on the 32m Tower.
- PWID data is normalized by the u_* needed for the MOST profile to pass through the recorded 2m velocity.
- Normalized profiles show good agreement

Smoke Visualization



~6:15AM : Red Smoke

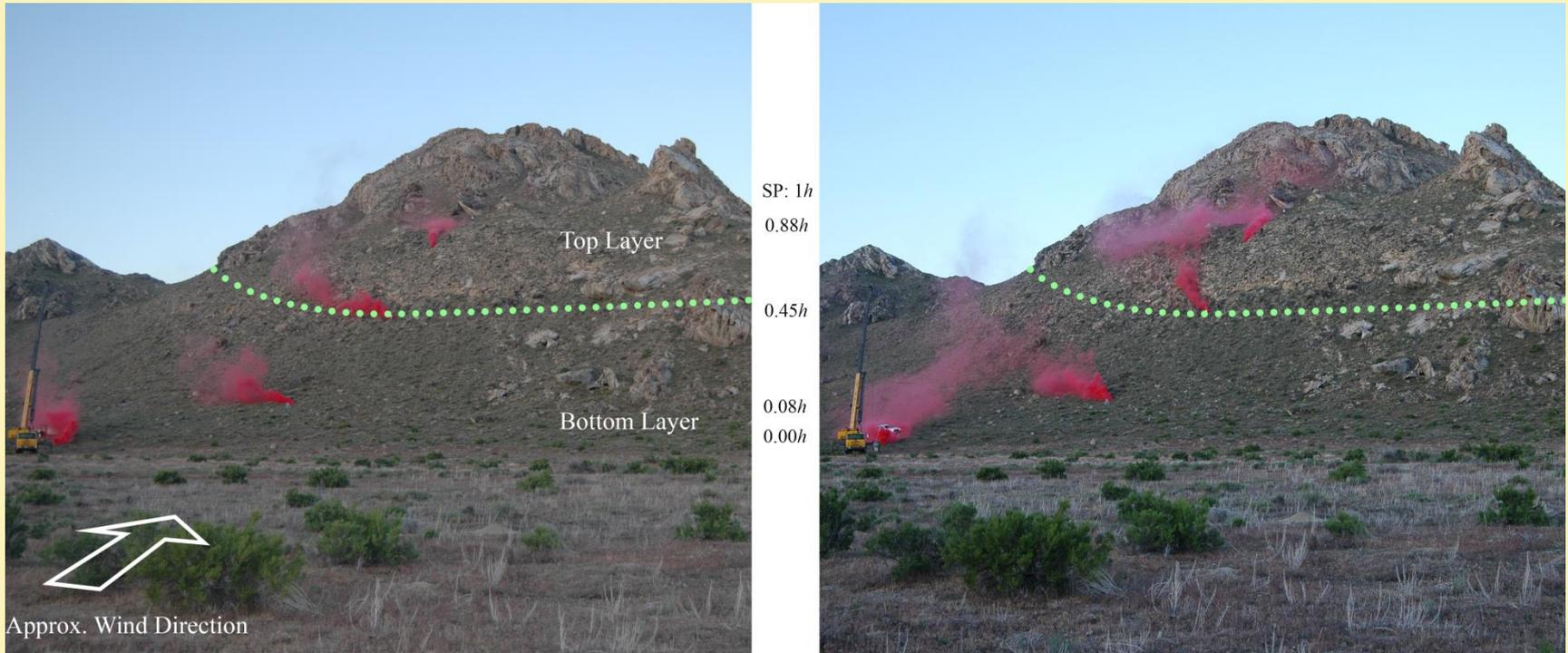
~6:30AM : White Smoke

Smoke release plume paths, as determine by observation:

(Left) Smoke release plume paths, as determine by observation.

(Right) Development of the buoyancy flux, as calculated from the tower sonic anemometer positioned 2m above the ground.

Smoke Visualization: Red Smoke



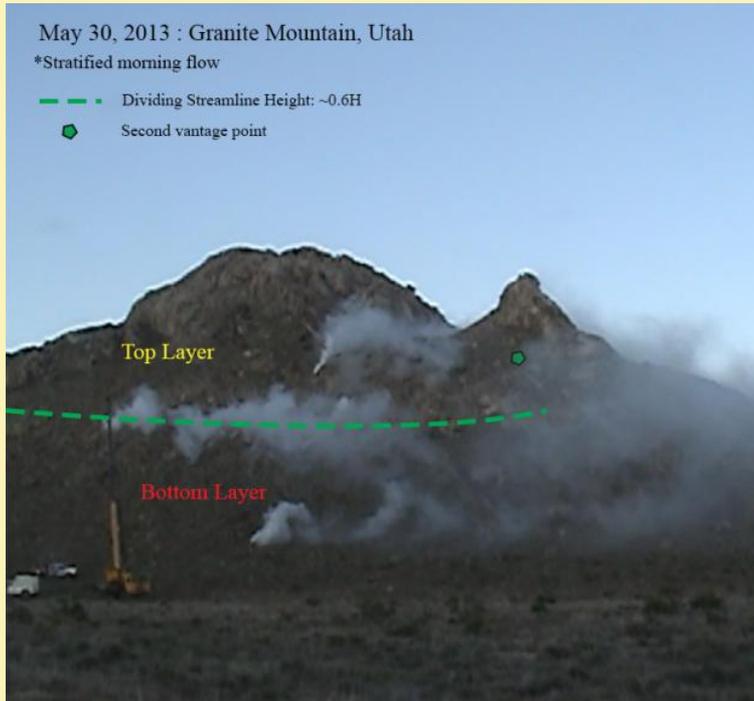
~6:15AM : Red Smoke

~30s after release

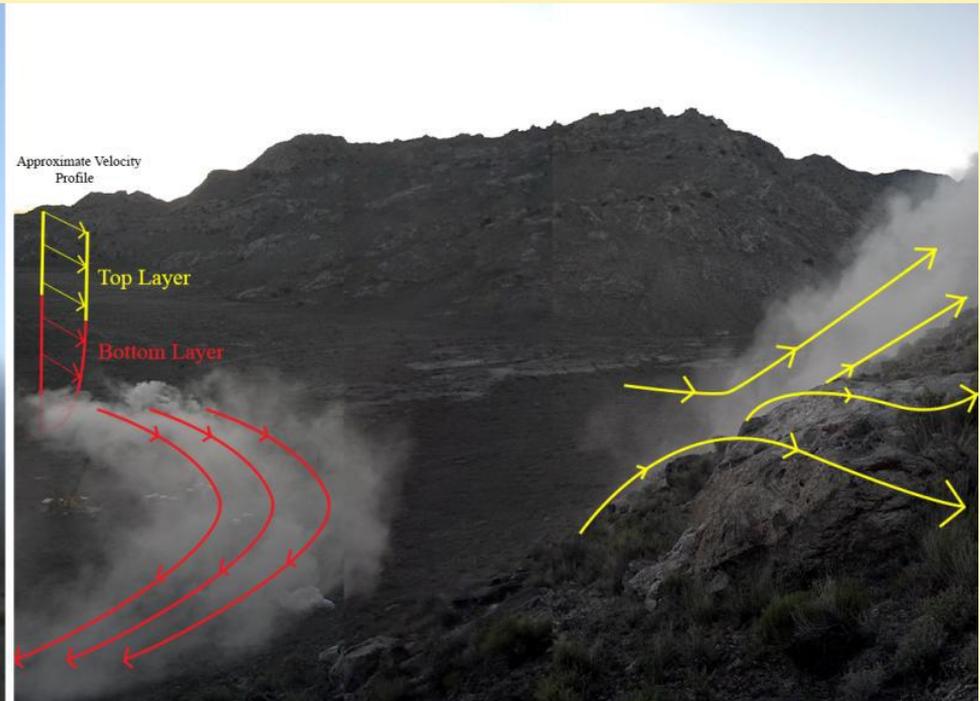
Things to note:

- Clear presence of dividing streamline
- Shift in middle release, perpendicular to parallel
- Release within the top layer is carried over the mountain

Smoke Visualization: Red Smoke



$\sim 6:30\text{AM}$: White Smoke / Elevated Release

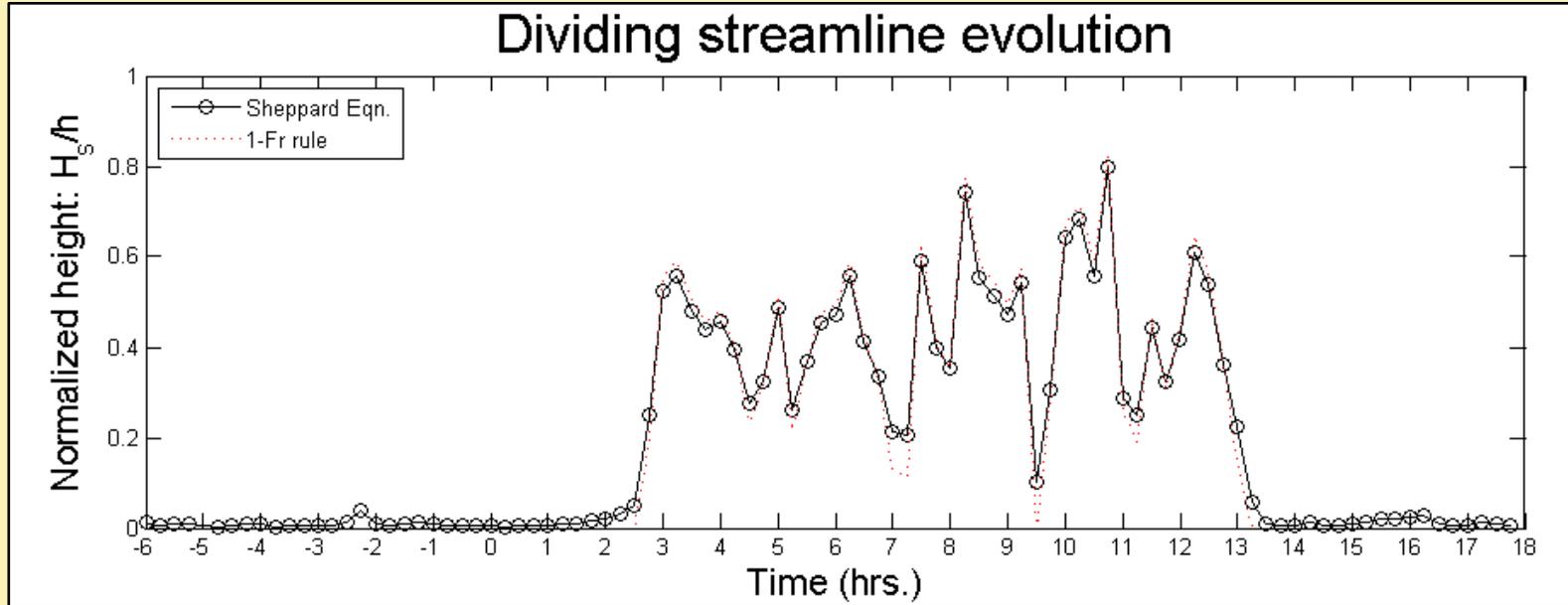


$\sim 180\text{s}$ after release

Things to note:

- Clear presence of dividing streamline
- Approaching streamline in bottom layer is deflected around the mountain
- Release within the top layer is carried over the mountain

Smoke Visualization: DSLH



Solve Sheppard's equation using velocity and temperature profiles previously established.

Things to note:

- As stratification forms, a dividing streamline becomes present
- During the time of the experiment, DSLH $\sim 0.5h$
- Calculations are consistent with field observations

Smoke Visualization: Movie



FlowVisualizationFinal.mov

Granite Mountain Overview



REFERENCES

- Hunt, et al. (1997) Low-Froude-number stable flows past mountains. *Il Nuovo Cimento*, **20**, 261-272.
- Kaimal, J.C. and J.J. Finnigan. 1994. *Atmospheric Boundary Layer Flows: Their Structure and Measurement*. New York: Oxford University Press.
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- Snyder, et al. (1980). Observations of flow around Cinder Cone Butte, Idaho. United States Environmental Protection Agency (USEPA). Report 00017-80-150
- Snyder, et al. (1985). The structure of strongly stratified flow over hills: dividing-streamline concept. *J. Fluid Mech.* **152**, 249-288.

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Thank You