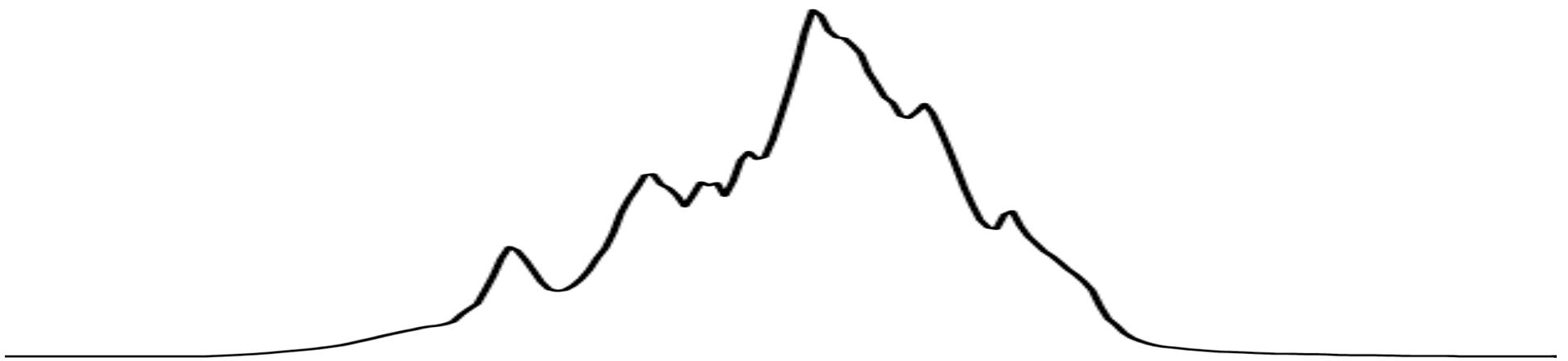


MATERHORN

The immersed boundary method for flow over complex terrain



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University of California, Berkeley

Overview

- Field work
- Owens Valley rotor simulations
- WRF-IBM for mesoscale to microscale
 - Terra incognita
- Log law implementation
 - Method development and testing
 - Comparisons with WRF
- Application to Granite Mountain
 - Preliminary results

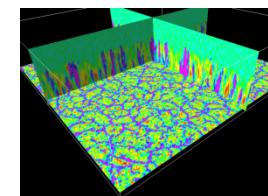
Terra incognita

- Push mesoscale models to higher resolution?
 - Or increase domain size for LES?
 - Is there a conflict?



Meso-scale

$L \sim 2\text{-}2000 \text{ km}$

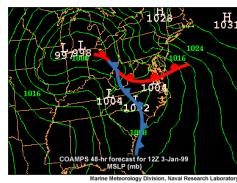


“Terra incognita”

Wyngaard (JAS 2004)

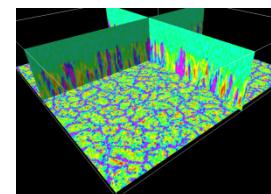
Challenges in the “Terra incognita”

- ❑ Steep topography
 - Terrain-following coordinate system
 - ❑ Turbulence modeling
 - ❑ Land-surface fluxes – similarity theory
 - ❑ Lateral boundary forcing
 - ❑ Other physics parameterizations



Meso-scale

$L \sim 2\text{-}2000 \text{ km}$

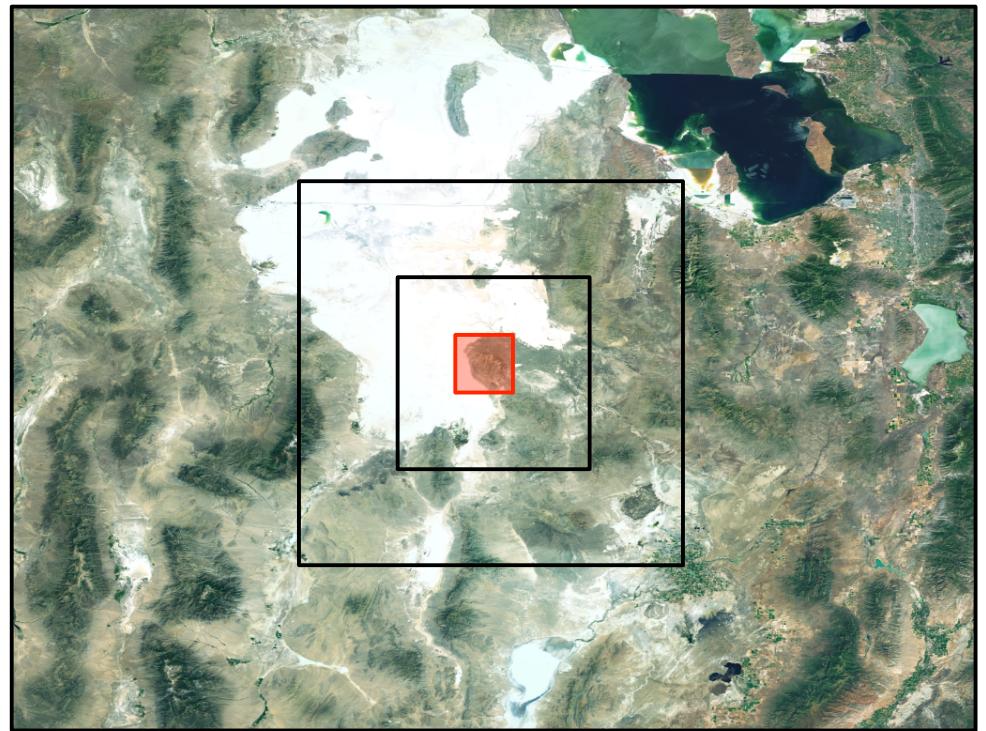


“Terra incognita”

Wyngaard (JAS 2004)

What we are doing

- Weather and Research Forecasting (WRF) model
 - Mesoscale to microscale
- One tool for all scales
 - Improved turbulence models for LES
 - Immersed boundary method (IBM) for steep terrain

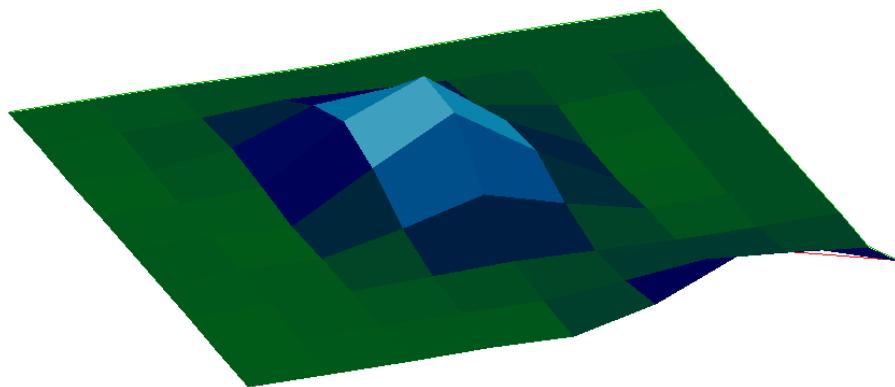


WRF-IBM Framework

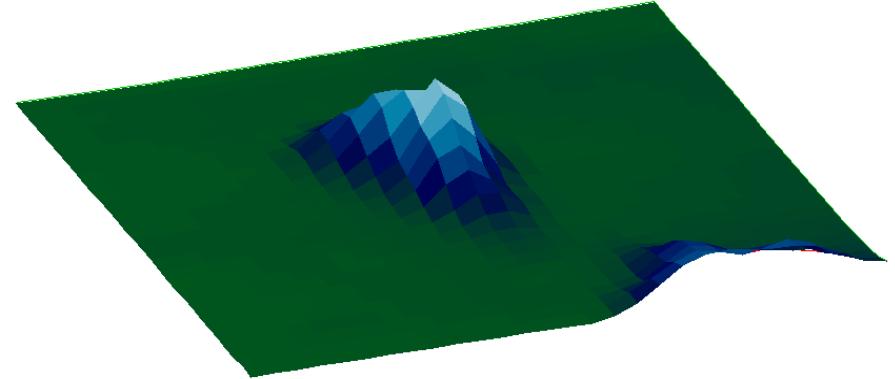
- Capable as mesoscale or LES code
- WRF fails with steep terrain slopes
- WRF-IBM (Lundquist et al. 2010, 2012)
 - WRF + immersed boundary method (IBM)
 - Same model; just a switch
 - Nesting possible

Increasing resolution → steeper slopes

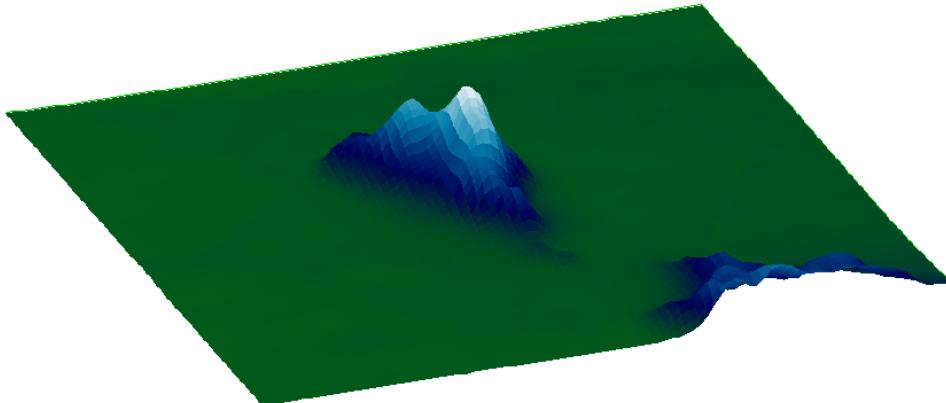
3 km, max slope $\sim 4^\circ$



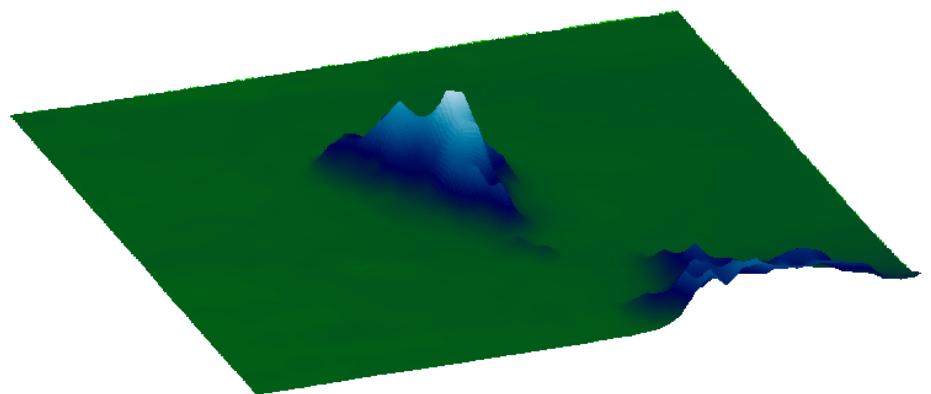
1 km, max slope $\sim 14^\circ$



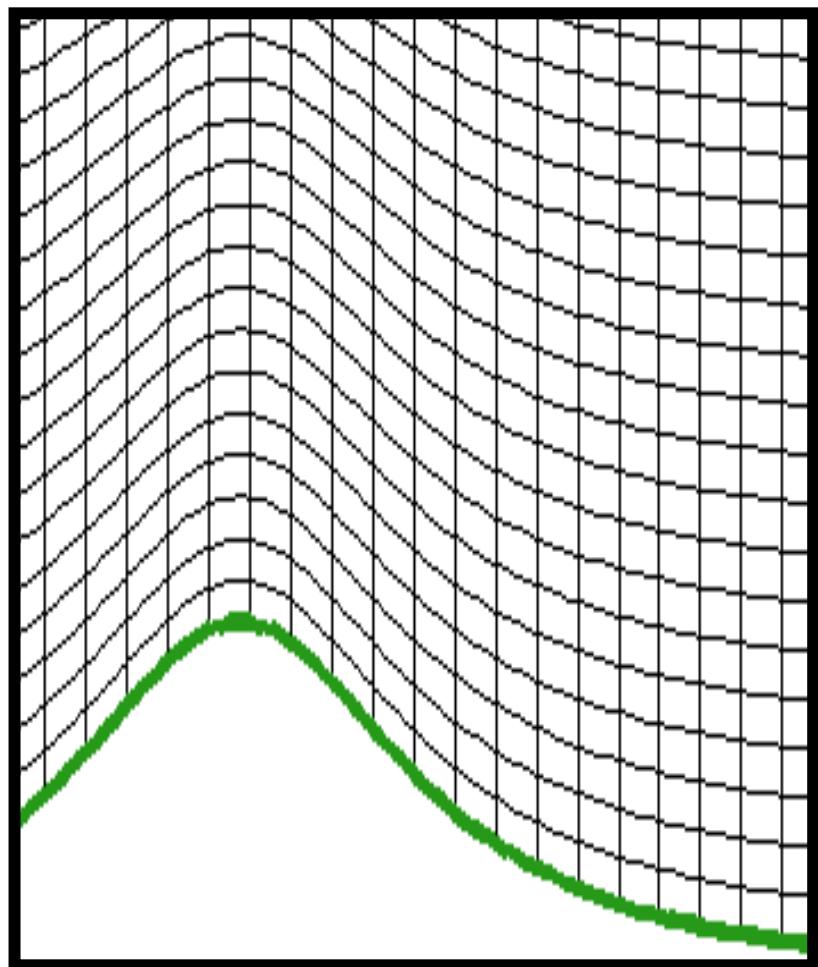
300 m, max slope $\sim 28^\circ$



100 m, max slope $\sim 32^\circ$



Terrain slope limit

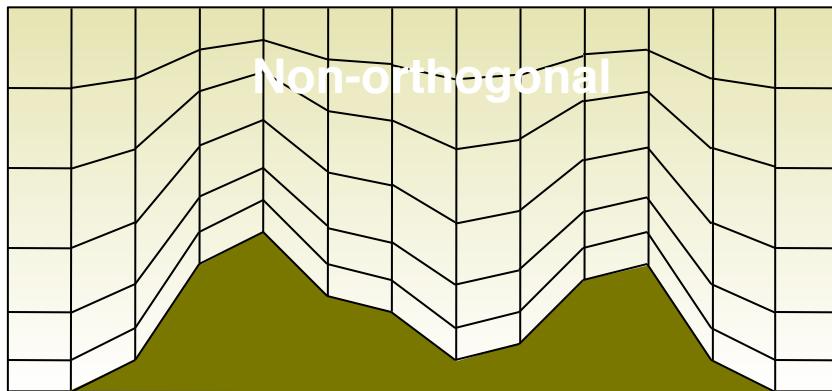


Terrain-following coordinates

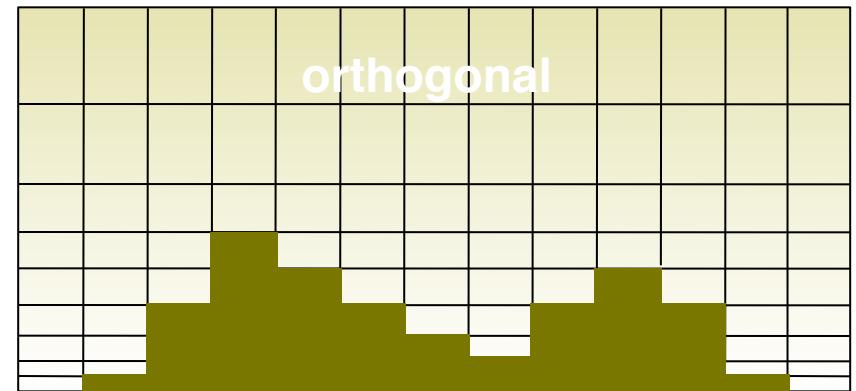
- Horizontal pressure gradient errors
 - 45° limit, usually ~30° starts causing problems (e.g. Mahrer 1984)
- Grid aspect ratio limitations
- Numerical stability

Vertical coordinate systems

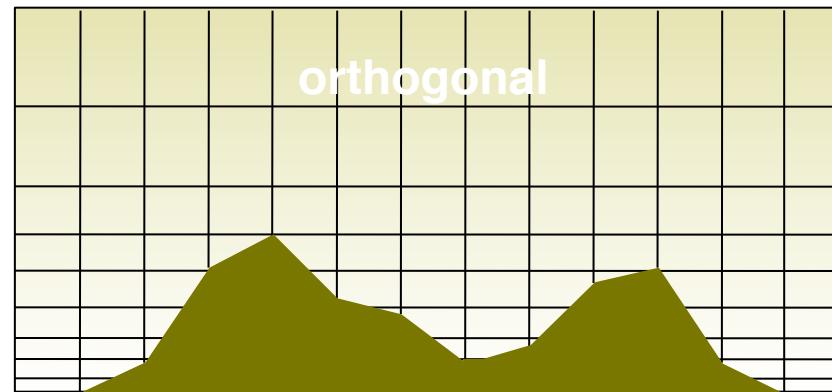
sigma, or terrain-following



eta, or “step mountain”

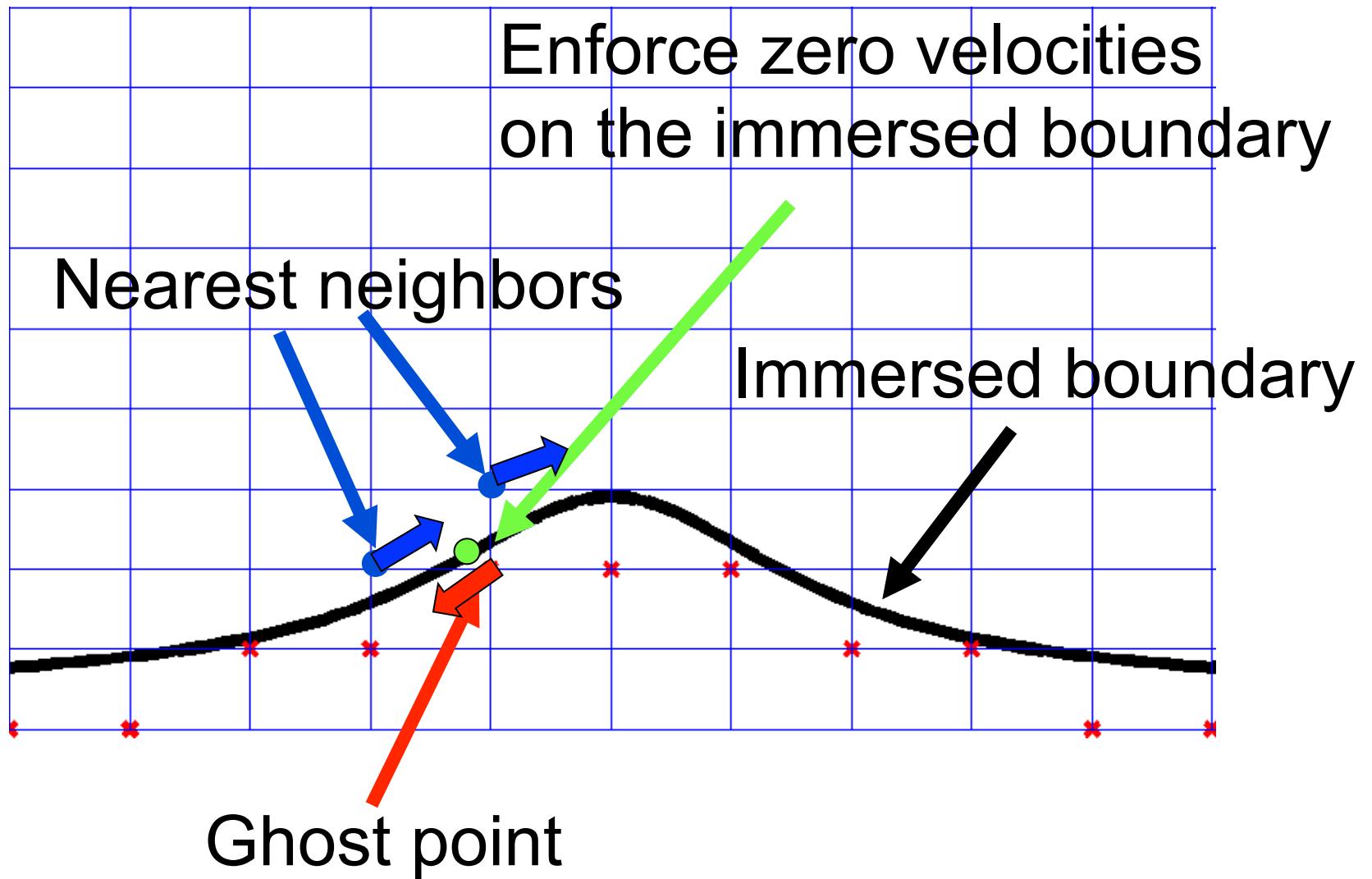


immersed boundary



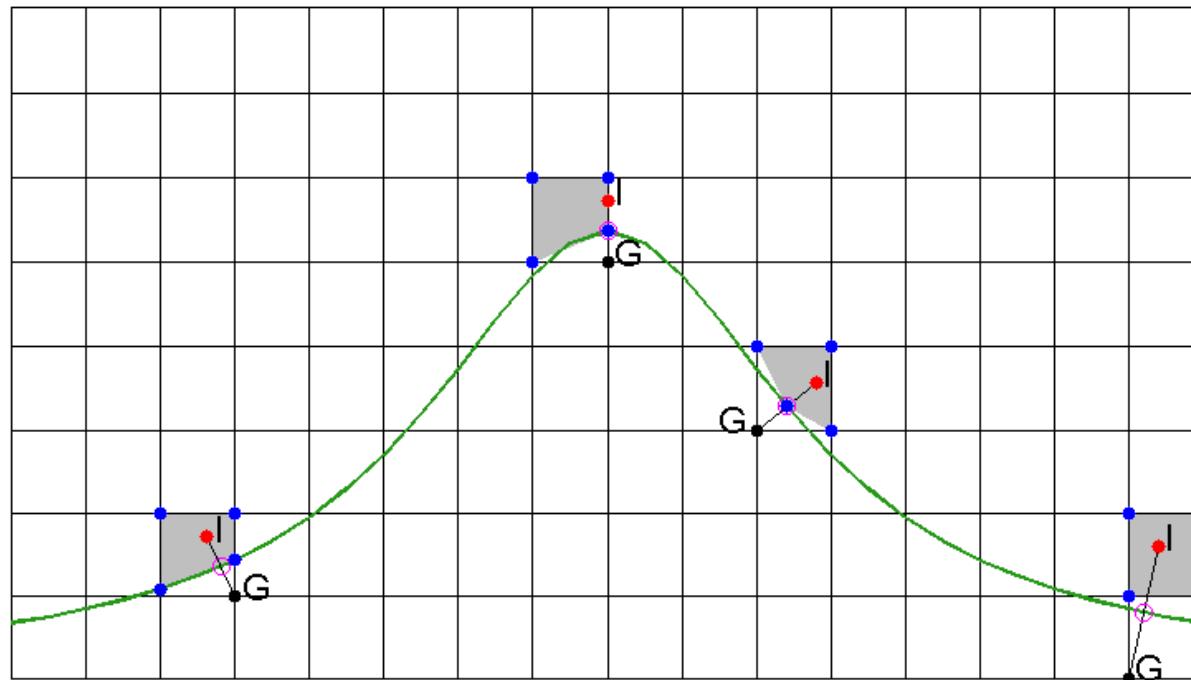
others include sigma-pressure, isentropic, and hybrids

Ghost-cell immersed boundary method



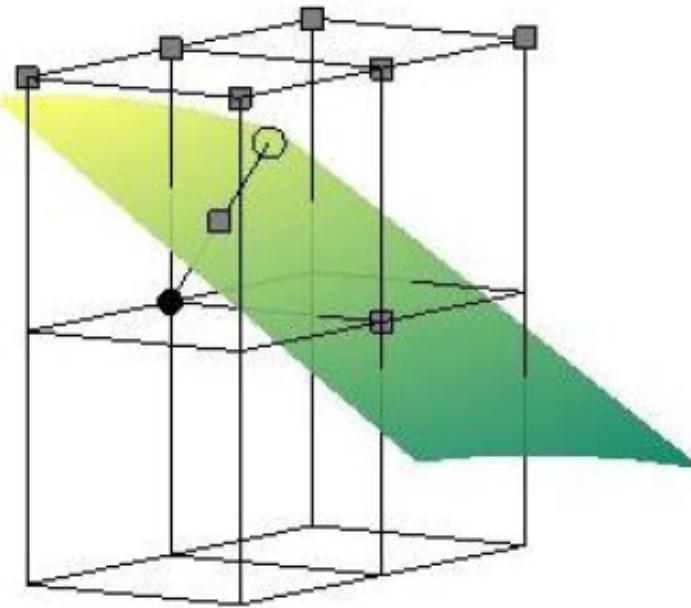
IBM - Boundary reconstruction

- ❑ IBM implemented in WRF
- ❑ 2 different interpolation algorithms
- ❑ Handles highly complex topography

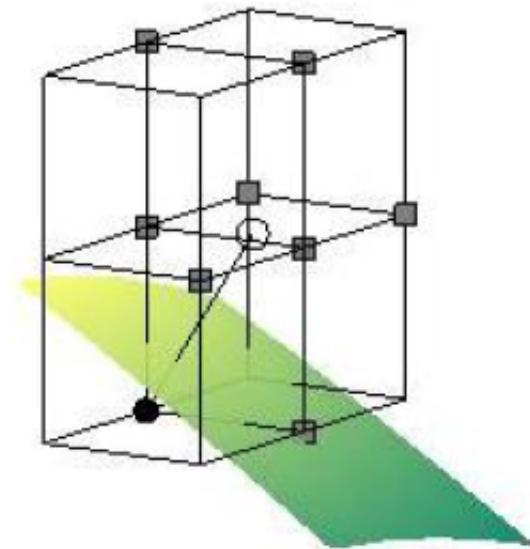


Lundquist et al. MWR 2010

Inverse distance weighting



(a) Dirichlet



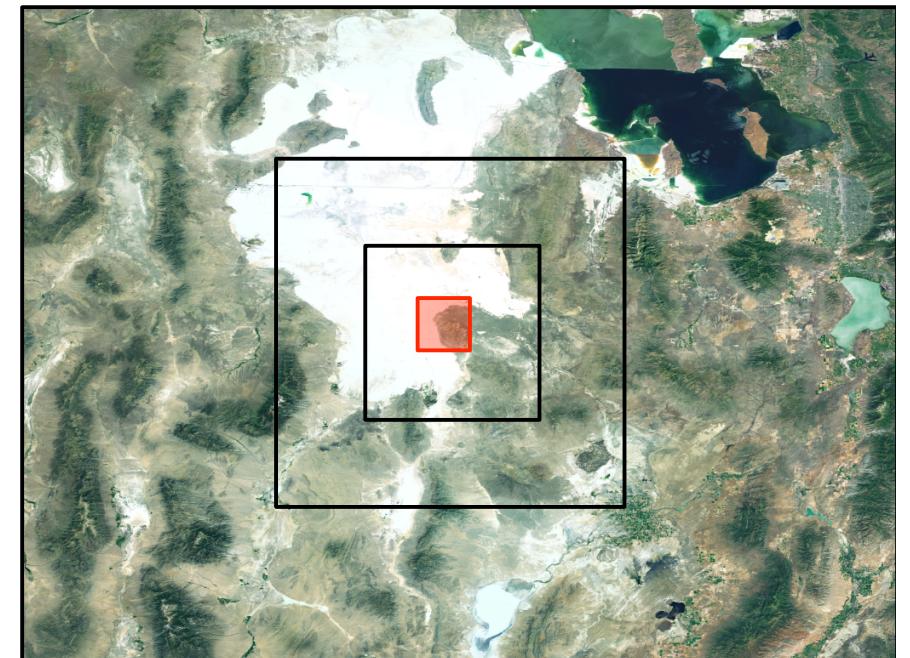
(b) Neumann

For complex urban geometries

Lundquist et al. 2010, 2012

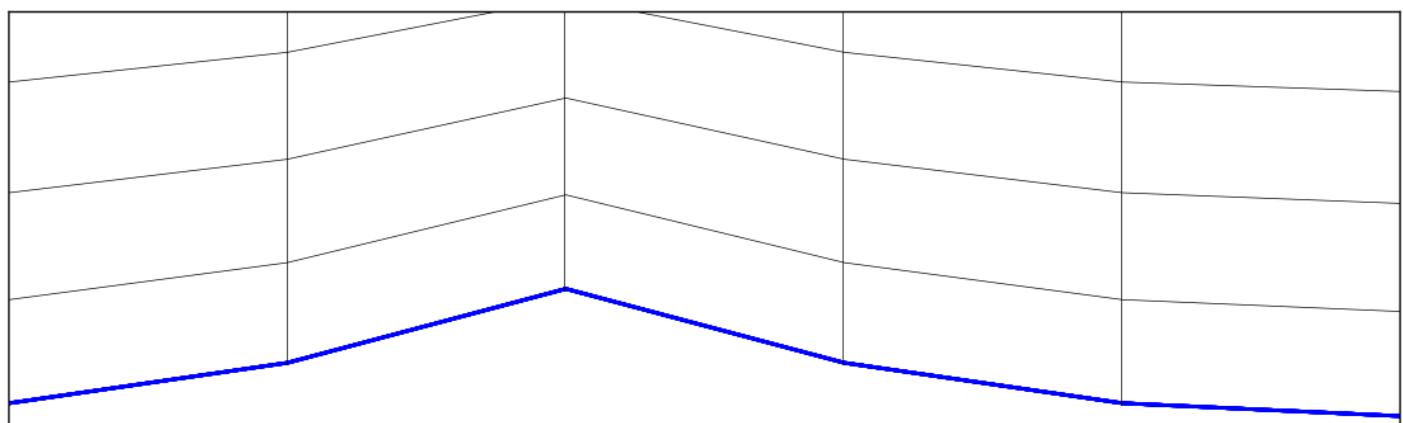
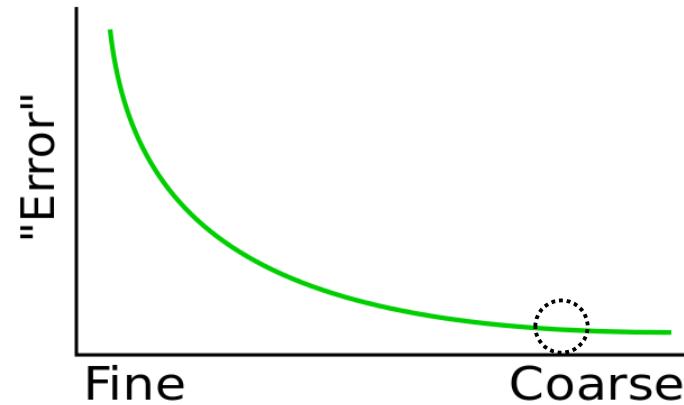
Seamless grid nesting

- Mesoscale to microscale
- Must switch from WRF to IBM-WRF
- When to switch?
 - Resolution, steepness, aspect ratio, turbulence closure



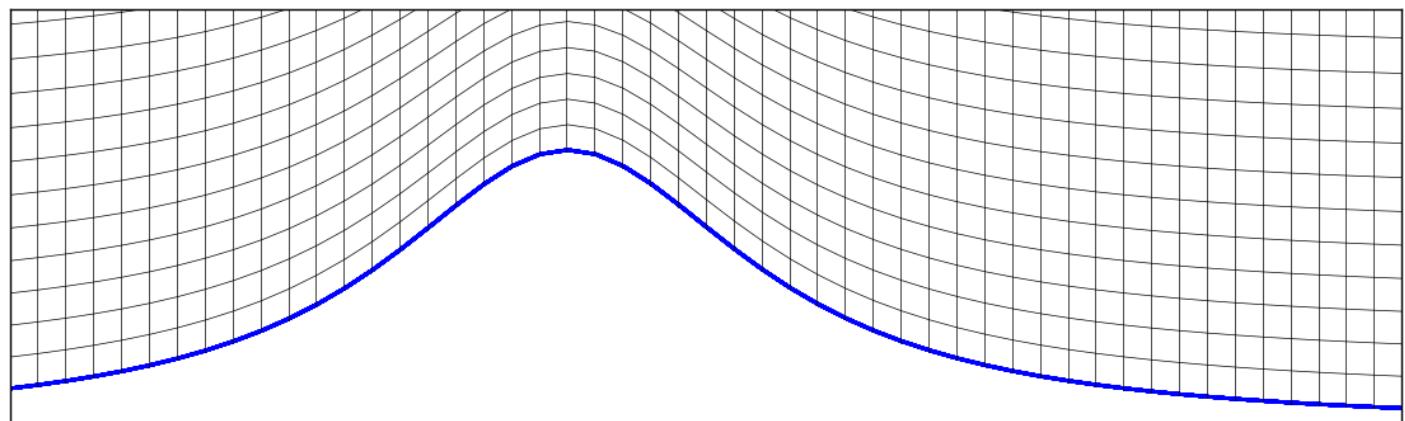
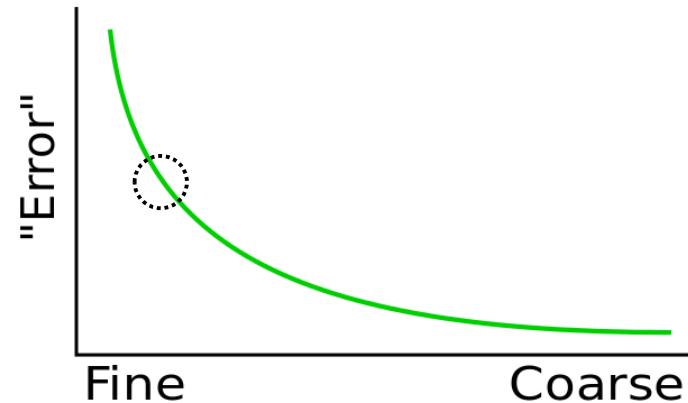
WRF Alone

- Coarse resolution
 - smooth terrain
 - low error
- Fine resolution
 - steep terrain
 - high error



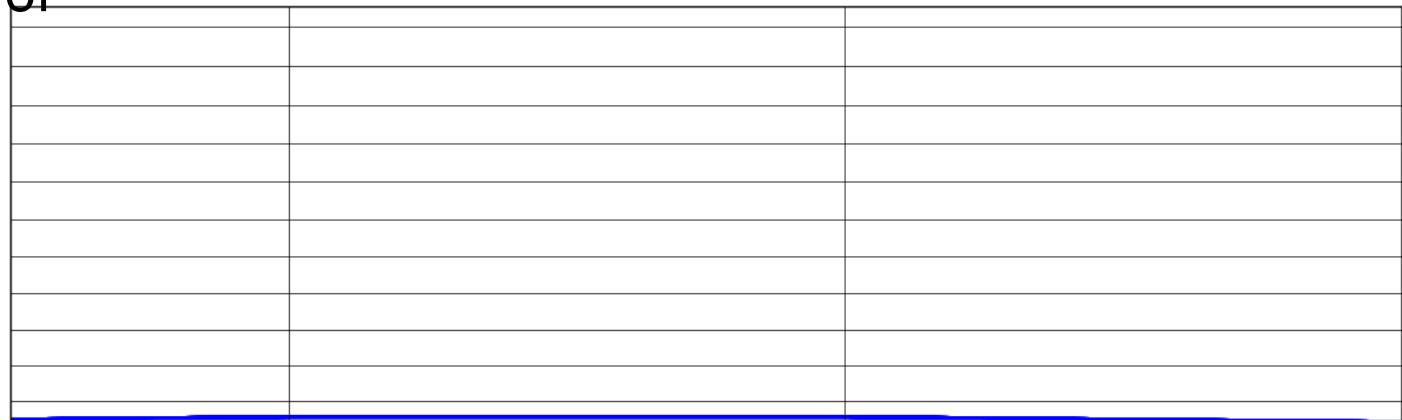
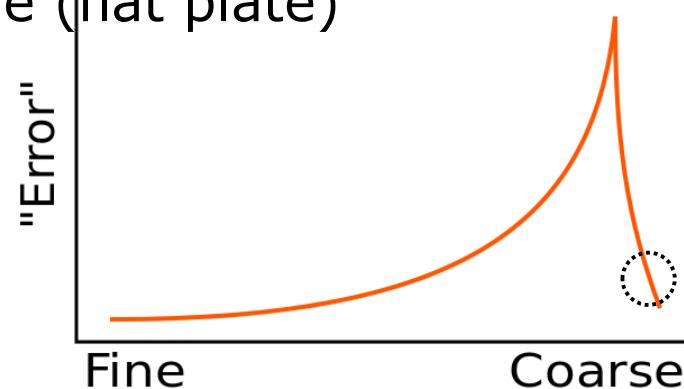
WRF Alone

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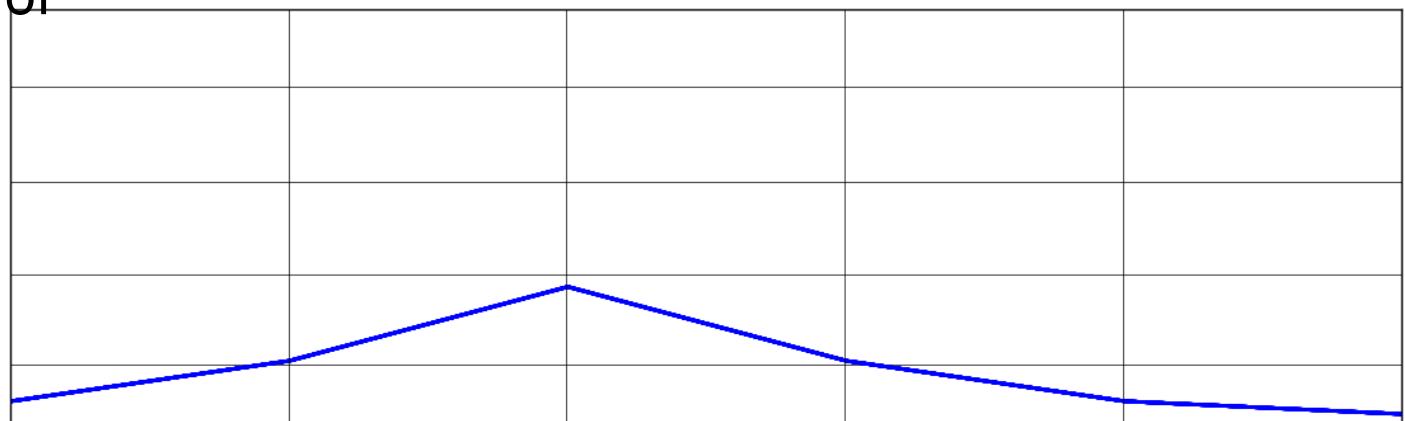
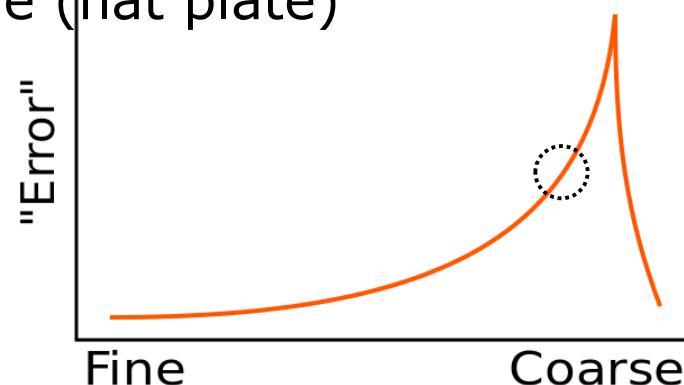
IBM-WRF Alone

- Very coarse resolution
 - grid-scale > mountain-scale (flat plate)
 - low error
- Coarse resolution
 - large spacing
 - high error (interpolation)
- Fine resolution
 - small spacing
 - low error



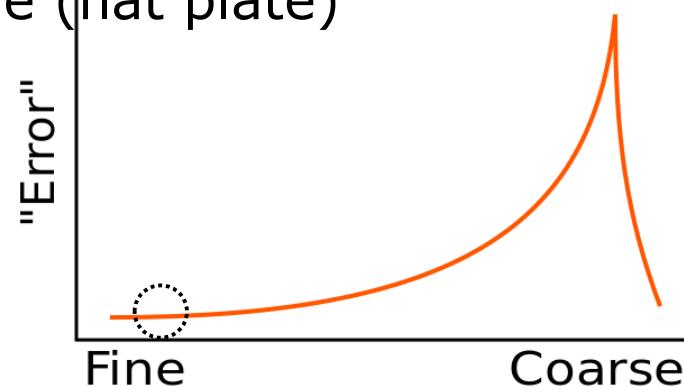
IBM-WRF Alone

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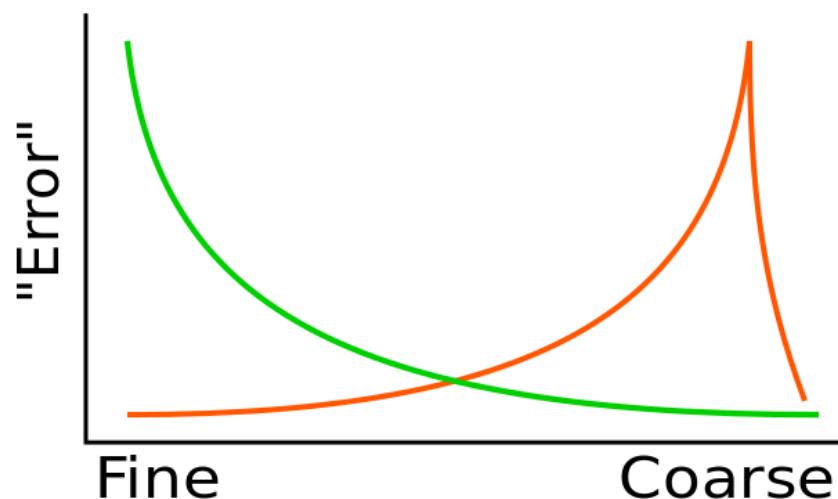
IBM-WRF Alone

- Very coarse resolution
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 - small spacing
 - low error



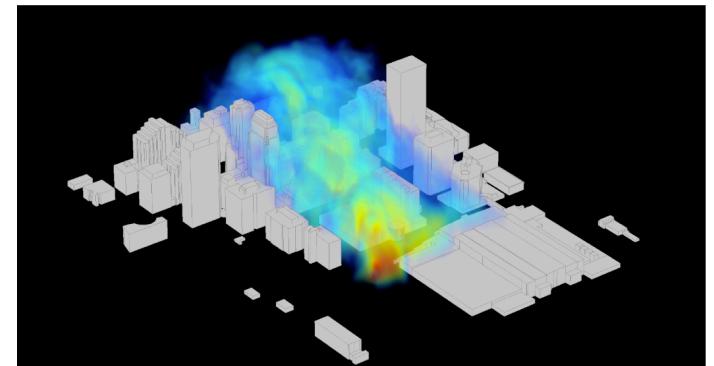
WRF to IBM-WRF

- Switch at intersection for best results
- Want to develop general guidelines for this curve
 - WRF starts blowing up near 300m resolution on 2D GMAST



Complex terrain applications

- Current implementation for no-slip
 - Good for urban environments at ~ 1 m resolution
- Need log law wall stress for complex terrain



IBM-WRF for Oklahoma City

$$U = \frac{u_*}{\kappa} \ln \left(\frac{z + z_0}{z_0} \right) \quad C_D = \left[\frac{1}{\kappa} \ln \left(\frac{z_1 + z_0}{z_0} \right) \right]^{-2}$$

$$\tau_{wall} = -u_*^2 = -C_D |U_1| U_1$$

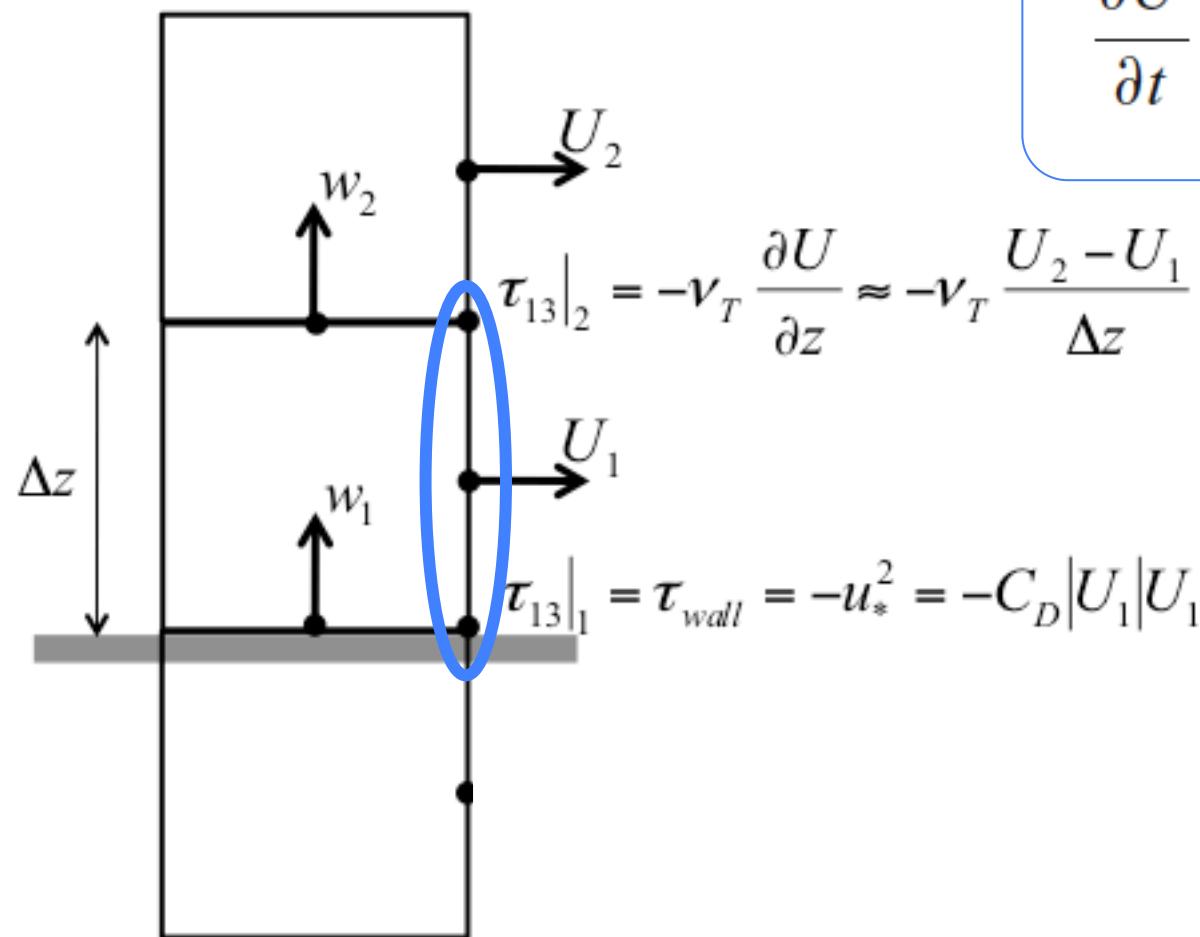
WRF implementation of log law

- Momentum equation in U direction

$$\frac{\partial U}{\partial t} + U \frac{\partial U}{\partial x} + V \frac{\partial U}{\partial y} + W \frac{\partial U}{\partial z} = -\frac{1}{\rho} \frac{\partial P}{\partial x} - \left(\frac{\partial \tau_{11}}{\partial x} + \frac{\partial \tau_{12}}{\partial y} + \frac{\partial \tau_{13}}{\partial z} \right)$$

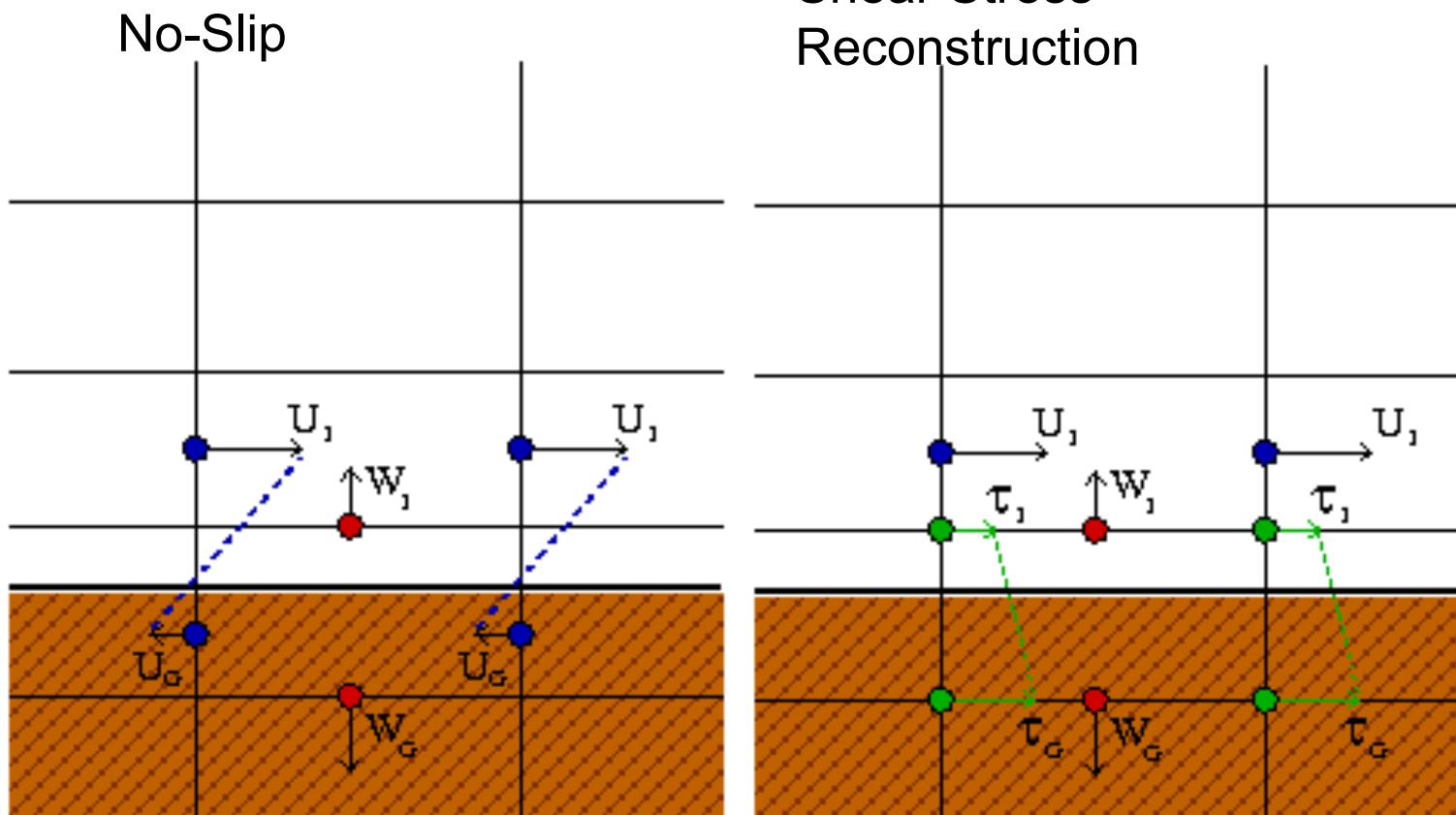
- Requires gradient in τ_{13}

WRF implementation of log law



$$\frac{\partial U}{\partial t} = - \frac{\partial \tau_{13}}{\partial z} \dots$$

IBM – log law implementation



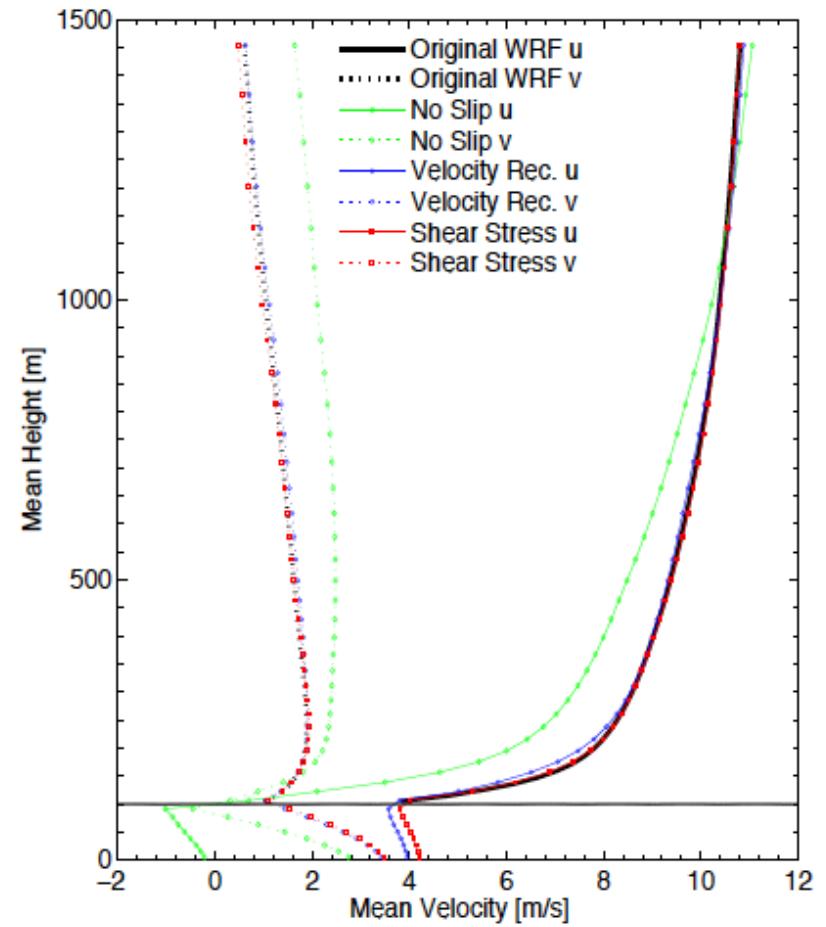
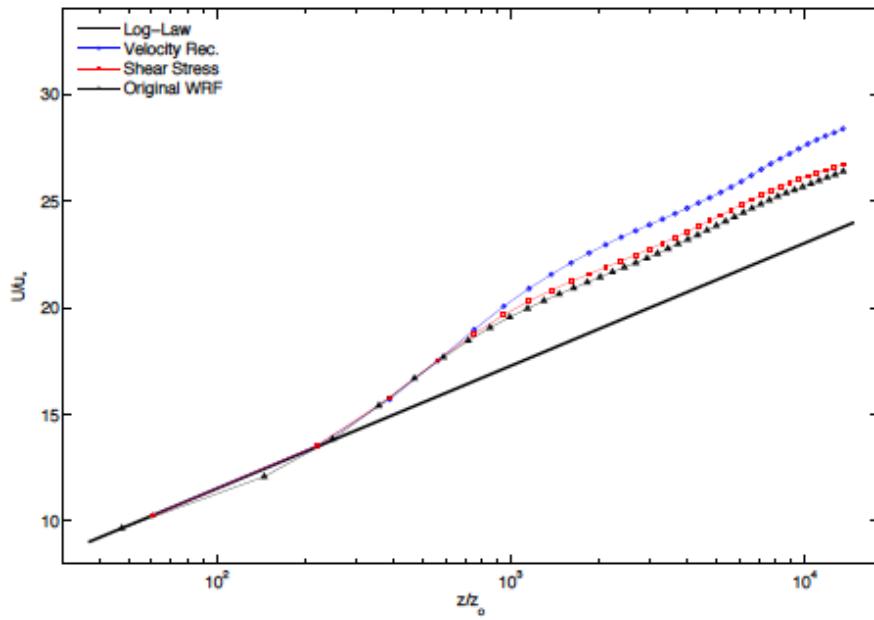
$$u_{surface} = v_{surface} = w_{surface} = 0$$

$$\vec{U} \cdot \hat{n} = 0$$

$$\tau_w = -\mu \left(\frac{\kappa}{\ln \frac{z_1-h}{z_o}} \right)^2 |\vec{U}| u$$

How to validate?

- Small changes can make big difference

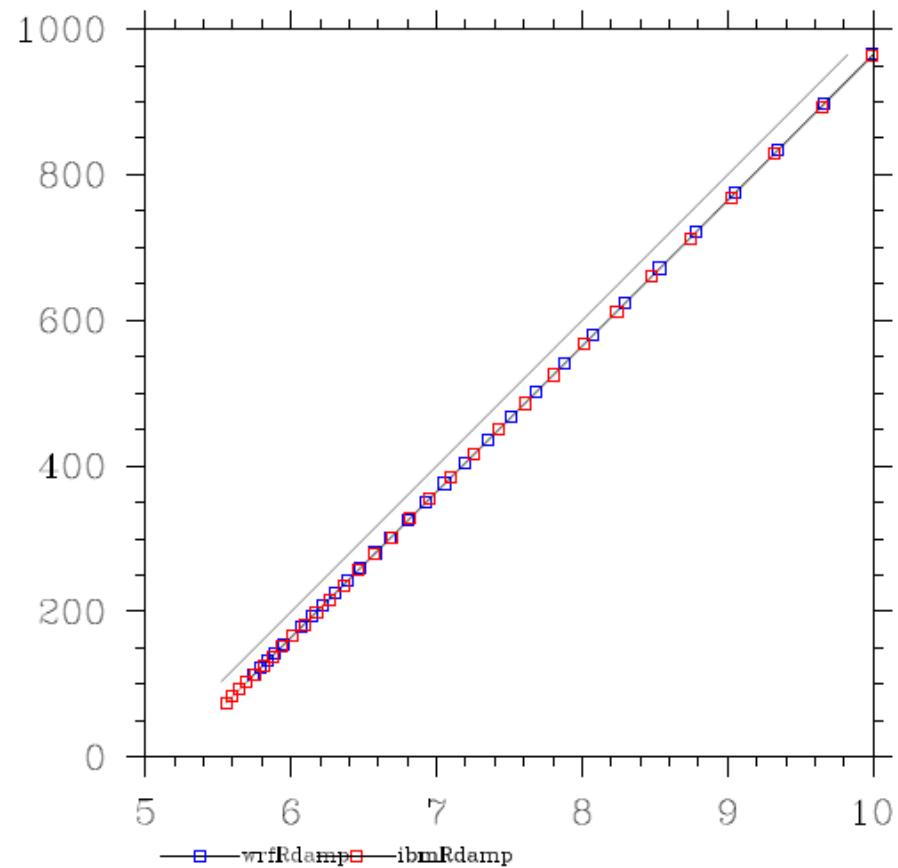


Test Case 1

- Flat plate
- Constant eddy viscosity
- Top Rayleigh damping layer
- Constant shear stress at wall
- Analytical solution

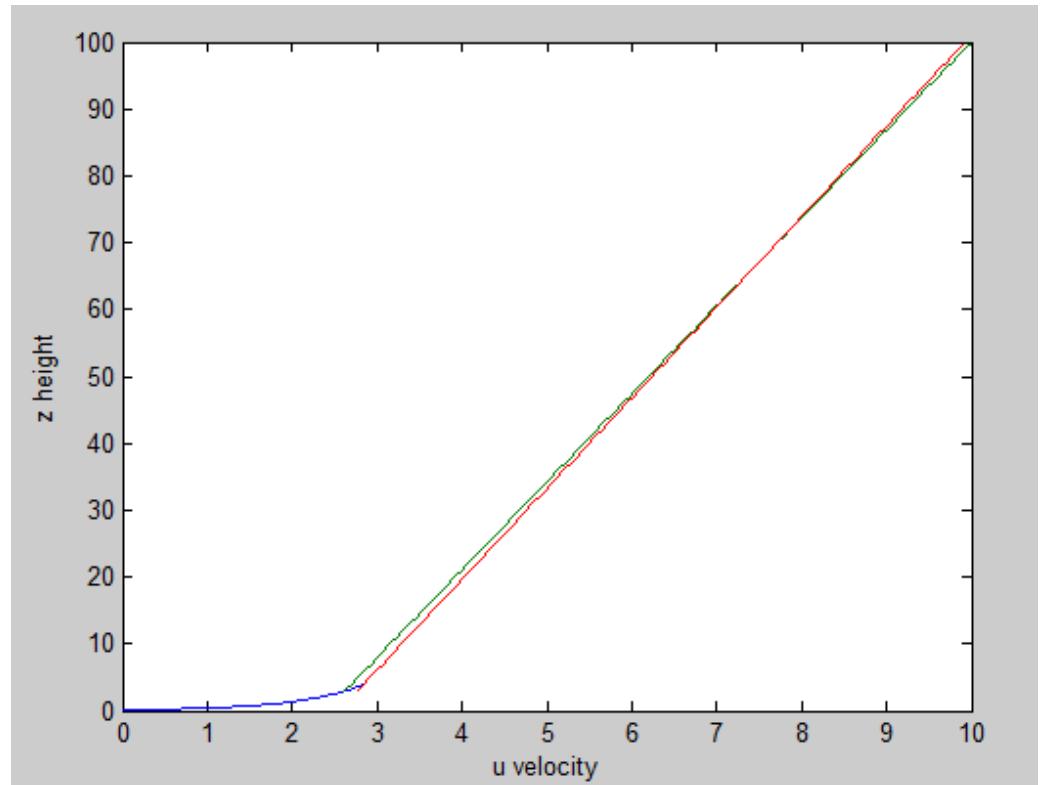
$$u = \frac{\tau_w}{v_t} z + 5.25$$

$$\tau_w = 0.1 \quad v_t = 20$$



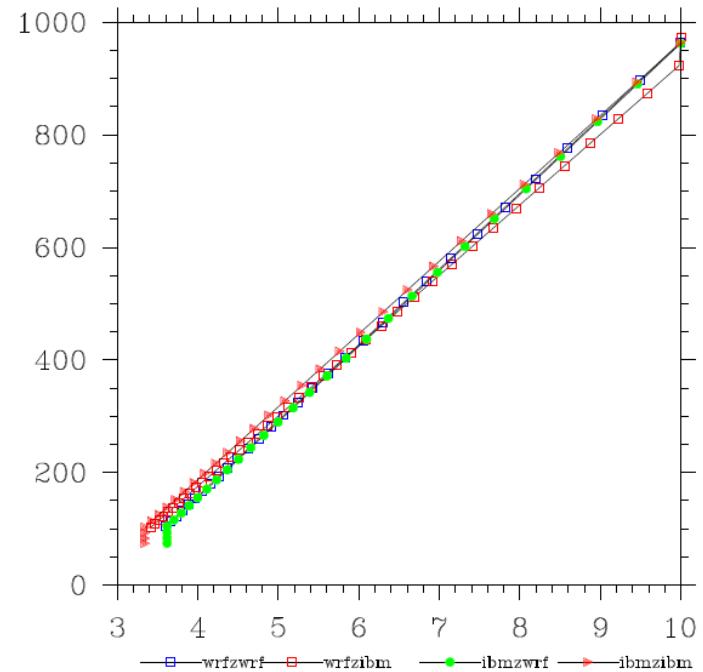
Test Case 2

- Flat plate
- Constant eddy viscosity
- Top Rayleigh damping layer
- Log law at wall
- Analytical solution
 - Below z_1 , velocity assumed logarithmic, above linear
 - Location of z_1 determines slope



Test Case 2

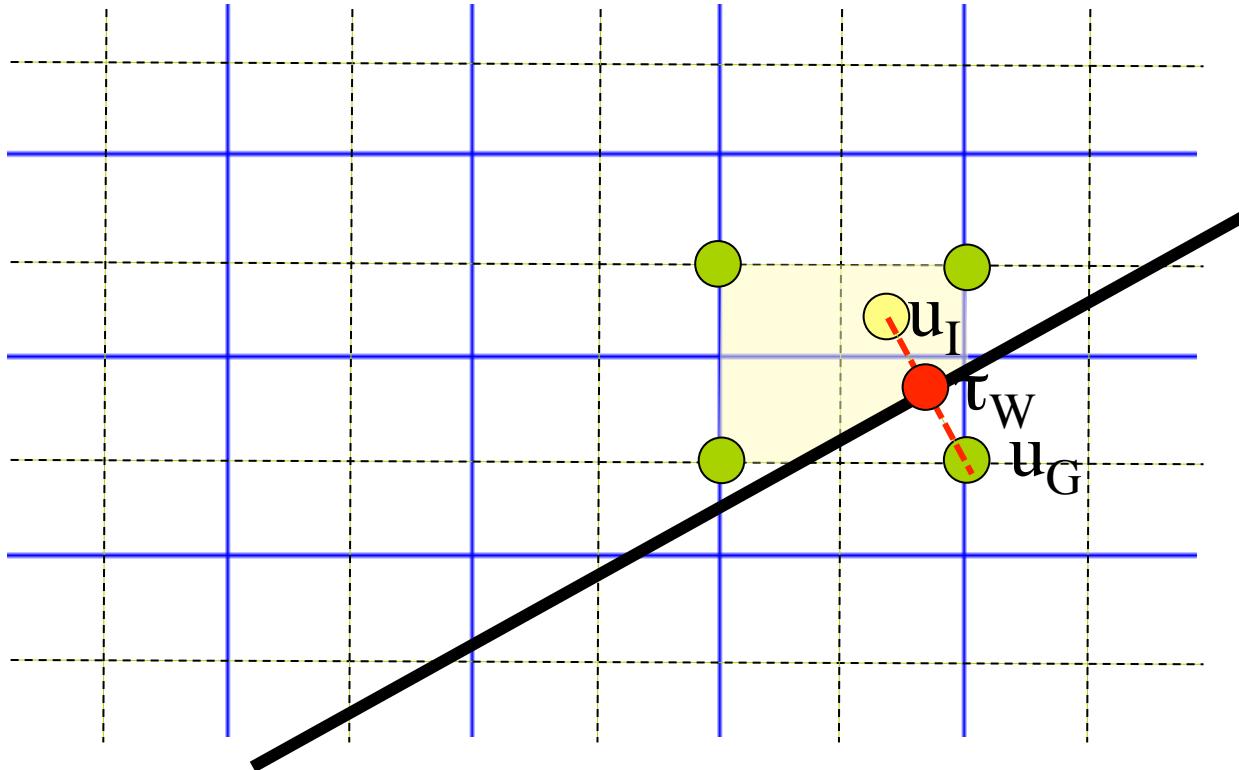
- Flat plate
- Constant eddy viscosity
- Top Rayleigh damping layer
- Log law at wall
- Analytical solution
 - Below z_1 , velocity assumed logarithmic, above linear
 - Location of z_1 determines slope



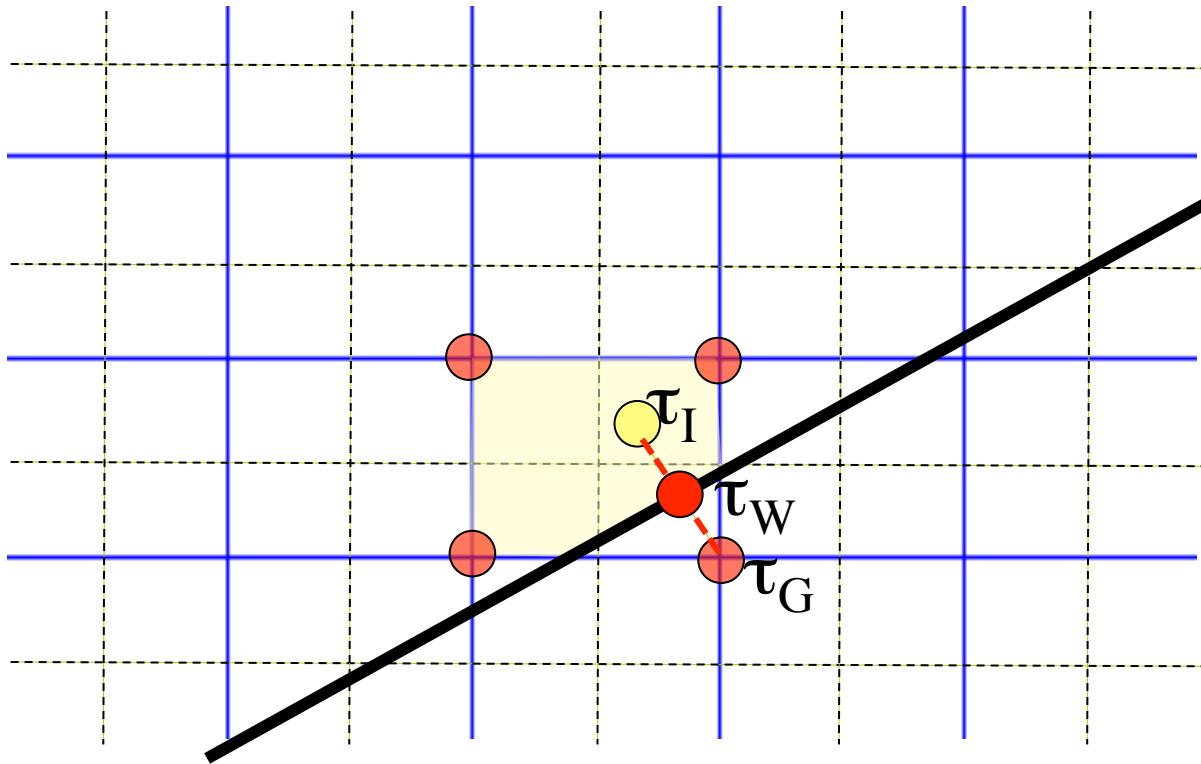
Test Case 3

- Flat plate
- Constant eddy viscosity
- Top Rayleigh damping layer
- Log law at wall
- Pressure gradient forcing

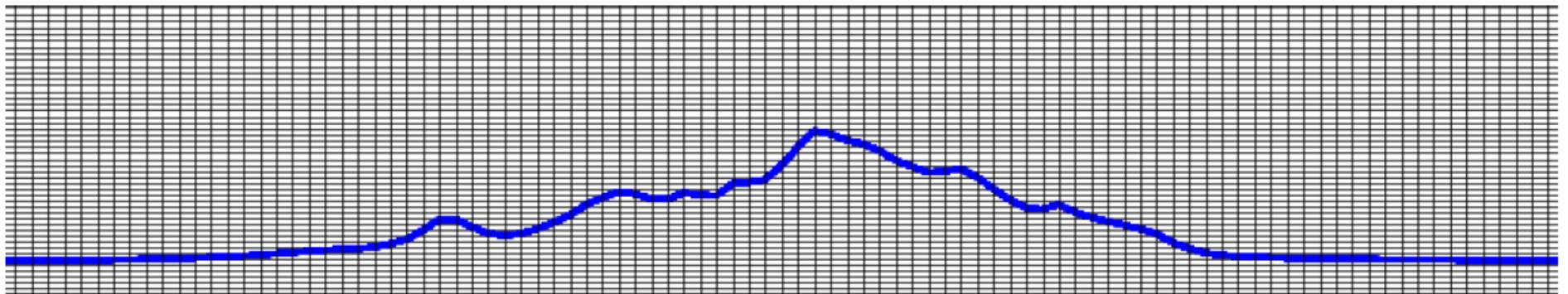
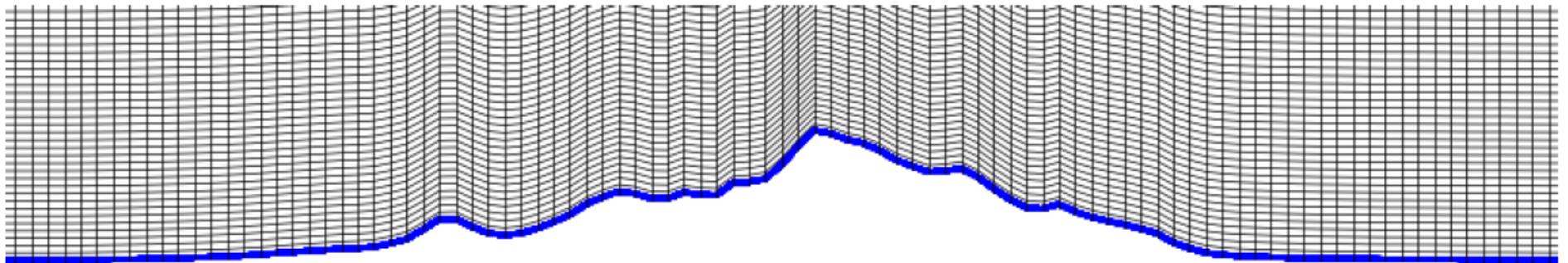
3D log law implementation



3D log law implementation



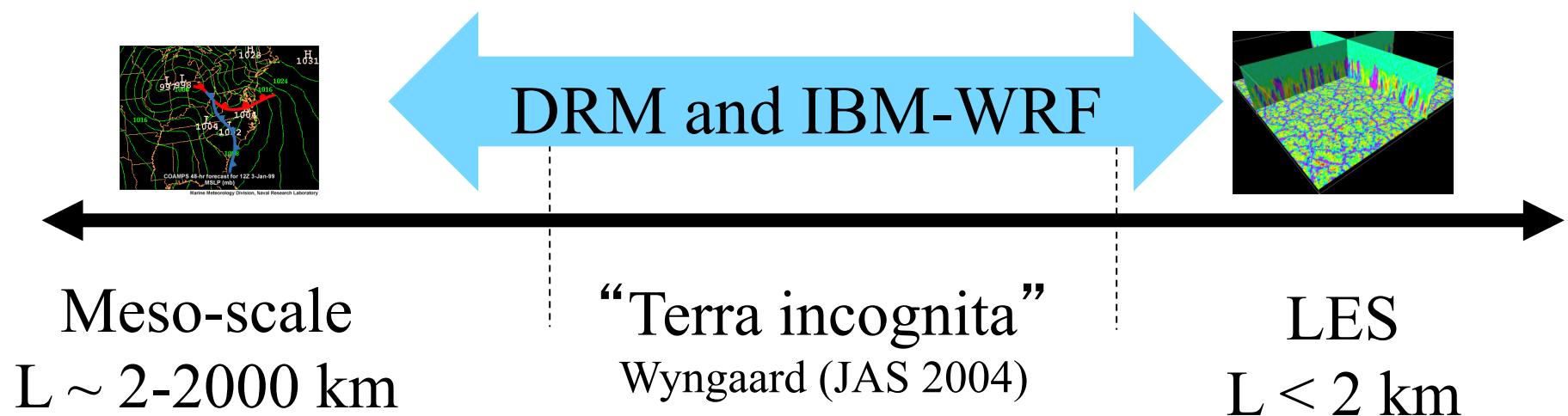
Granite Mountain – IBM test case



Granite Mountain, Utah

MATERHORN: addressing challenges in the “Terra incognita”

- Steep topography
- Turbulence modeling
- Land-surface fluxes – similarity theory



Ongoing work

- IBM log law
 - 3D implementation
 - Validation
- Granite Mountain
 - Semi-idealized
 - Real case
- Turbulence closure
- Owens Valley

