# **Electroabsorption Modulators**

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# **Optical Modulation**

#### Direct modulation

#### Output frequency shifts with drive signal

- Carrier induced (chirp)
- Temperature variation due to carrier modulation

#### Limited extinction ratio

Indirect or External modulation

#### Electro-optic modulation

- Change optical path length with applied electric field
- Electroabsorption modulation
  - Change amount of light absorbed with applied electric field
- Finite insertion loss (6-7 dB)

# **Advantages of EA modulator**

- Zero biasing voltage
- Low driving voltage
- Low/negative chirp
- High speed
- Lesser polarization dependence
- Integration with DFB laser
- Allows a single optical power source to be used for large number of information carrying beams

## **Electroabsorption modulator**

#### Mechanisms

Franz-Keldysh effect

Observed in conventional bulk semiconductors

#### Quantum-confined Stark effect (QCSE)

- Quantum well structures
- Both of these electroabsorption effects are prominent near the bandgap of semiconductors

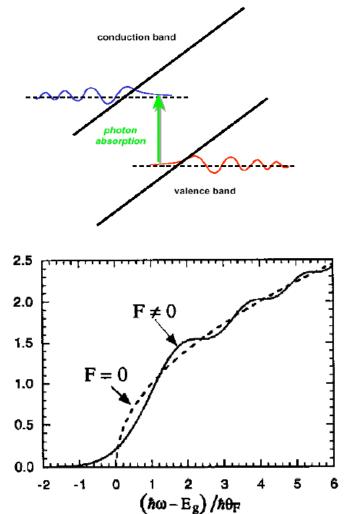
## **Franz-Keldysh effect**

Tunneling allows overlap of electron and hole wavefunctions for photon energy less than bandgap

$$\alpha = K(E')^{1/2} (8\beta)^{-1} \exp\left(\frac{-4}{3}\beta^{3/2}\right)$$

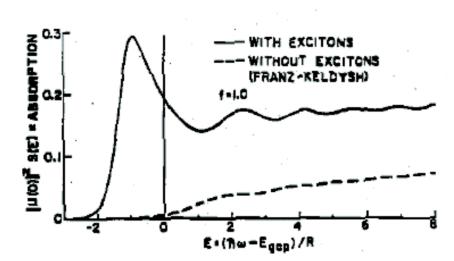
where,

$$E' = \left(\frac{q^2 E^2 \hbar^2}{2m_r^*}\right)^{1/3}$$
$$\beta = \frac{\varepsilon_g - \hbar\omega}{E'}$$



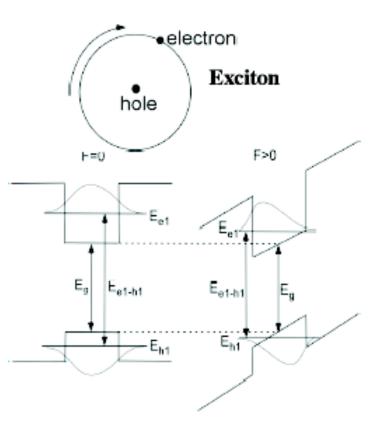
# Excitonic electroabsorption (Stark effect)

- Excitonic effects gives rise to a step-like rise in absorption spectra
- Formation of excitons manifests themselves as a series of sharp resonances near the bandgap energy
- Formed in very pure semiconductors at low temperatures
- Excitons can be very easily field ionized



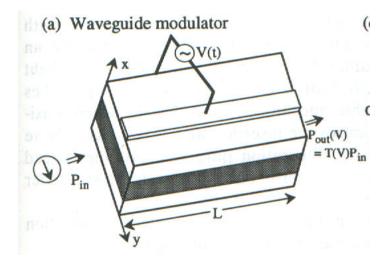
# **Quantum Confined Stark Effect**

- Quantum well increases the overlap of electron and hole wavefunctions
- Electric field reduces overlap and results in a corresponding reduction in absorption and luminescence
- Exciton absorption peak is not greatly broadened because of confinement

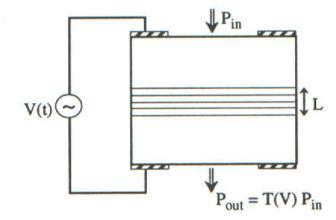


## **Device structure**

- Primary materials for EA modulators are III-V semiconductors
- PIN structure
- Transmission type does not lead to high enough extinction ratio
- Waveguide type more commonly used - has higher optical confinement

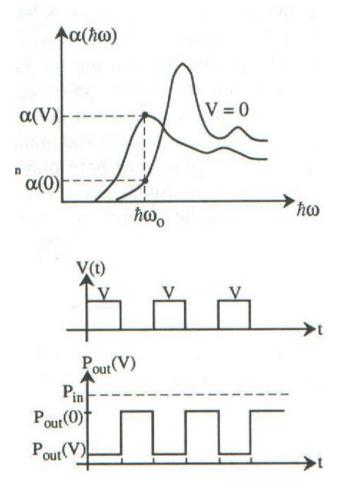


(b) Transverse transmission modulator



# **Design considerations**

- Operation principle
- Contrast ratio
- Insertion loss
- Modulation efficiency
- Chirp considerations and efficiency
- Packaging and integration



## **Extinction Ratio**

$$R_{on/off} = \frac{P_{out}(V_{on} = 0)}{P_{out}(V_{off} = V)} = \frac{e^{-\alpha(0)L}}{e^{-\alpha(V)L}}$$
$$R_{on/off}(dB) = 10\log(R_{on/off}) = 4.343 \cdot [\alpha(V) - \alpha(0)]L$$

- BER directly effected by extinction ratio
- Contrast ratio can be made as large as possible by increasing the length of the modulator. But propagation loss then becomes an issue.

## **Insertion loss**

#### Absorptive loss

- Longer the modulator, larger the insertion loss.
- Trade-off with Extinction Ratio

Loss = 
$$\frac{P_{in} - P_{out}(V = 0)}{P_{in}} = 1 - e^{-\alpha(0)L}$$

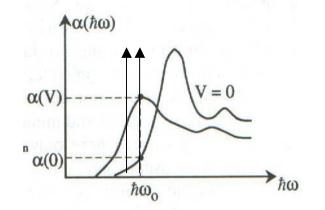
- Single mode fiber coupling loss
  - Waveguide coupler can be used to reduce coupling loss
  - Can be as good as 1 dB
  - Typical numbers are 5-6 dB

# **Modulation efficiency**

 Modulation efficiency quantifies how much voltage do we need to modulate the optical signal.

$$\frac{R_{on/off}}{\Delta V} = 4.343 \frac{\left[\alpha(V) - \alpha(0)\right]L}{\Delta V} = 4.343 \frac{\Delta \alpha}{\Delta F}$$

Smaller detuning will increase the modulation efficiency. However, it also results in a larger insertion loss.



# Chirp

Frequency sweep imposed as a result of power change

$$\alpha_{e} = -\frac{2\omega}{c} \frac{\Delta n_{r}}{\Delta g} = -\frac{4\pi}{\lambda} \frac{\Delta n_{r}}{\Delta g}$$

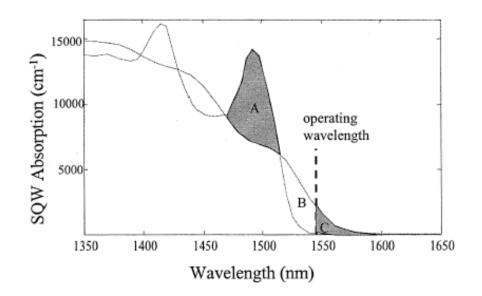
 Imaginary part of refractive index is related to optical absorption coefficient by,

$$\alpha = \frac{2\omega}{c}k = \frac{4\pi}{\lambda}k$$

Kramers-Kronig relation

$$\Delta n = \frac{\hbar c}{\pi} P \int_{0}^{\infty} \frac{\Delta \alpha}{E^{2} - (\hbar \omega)^{2}} dE$$

### **Chirp Engineering**



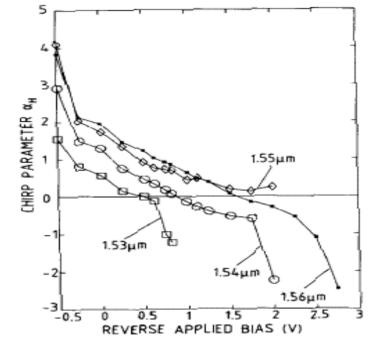
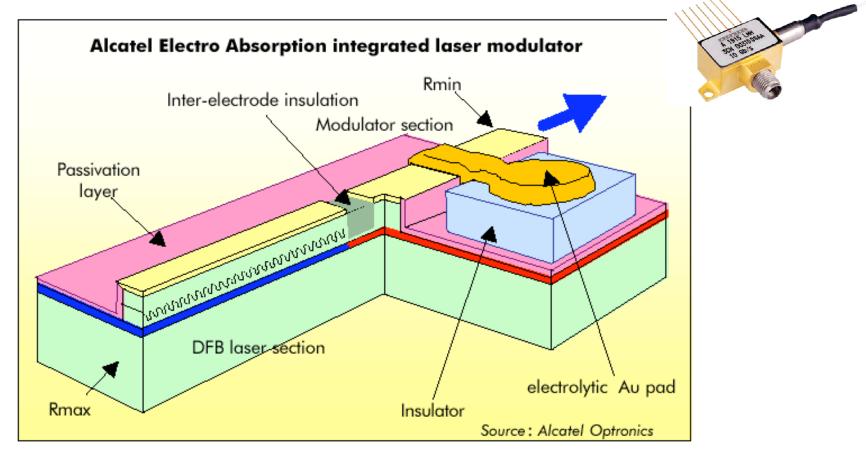


Fig. 15. Illustration of index change due to QCSE. The absorption changes in area B contribute to positive  $\Delta$  n, while the absorption changes in areas A and C contribute to negative  $\Delta n$ .

 $\Delta n = \frac{\hbar c}{\pi} P \int_{0}^{\infty} \frac{\Delta \alpha}{E^{2} - (\hbar \omega)^{2}} dE \qquad \Delta f_{FWHM} = \frac{\alpha_{e}}{2I} \frac{dI}{dt}$ 

## Integration



• 10Gb/s module,  $I_{th} = 20mA$ ,  $P_{max} = 4mW$  @80mA, extinction ratio = 15dB for -2.5V

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- G. L. Li and P. K. L. Yu, J. Lightwave Tech., Sep 2003