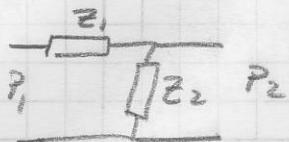


Problem 1



Part a) S-parameters:

$$S_{11} = \frac{V_1^-}{V_1^+} \Big|_{V_2^+=0} \rightarrow \text{Port 2 terminated with } Z_0$$

$$\Rightarrow Z_{in} = Z_1 + (Z_2 // Z_0)$$

$$S_{11} = \frac{Z_1 + (Z_2 // Z_0) - Z_0}{Z_1 + (Z_2 // Z_0) + Z_0} = \frac{(Z_1 - Z_0)(Z_2 + Z_0) + Z_2 Z_0}{(Z_1 + Z_0)(Z_2 + Z_0) + Z_2 Z_0}$$

$$S_{22} = \frac{V_2^-}{V_2^+} \Big|_{V_1^+=0} \rightarrow \text{Port 1 terminated with } Z_0$$

$$Z_{in} = Z_2 // (Z_1 + Z_0)$$

$$S_{22} = \frac{[Z_2 // (Z_1 + Z_0)] - Z_0}{[Z_2 // (Z_1 + Z_0)] + Z_0} = \frac{Z_2 (Z_1 + Z_0) - Z_0 (Z_1 + Z_2 + Z_0)}{Z_2 (Z_1 + Z_0) + Z_0 (Z_1 + Z_2 + Z_0)}$$

$$S_{21} = \frac{V_2^-}{V_1^+} \Big|_{V_2^+=0} \quad V_2 = V_2^- + V_2^+ \xrightarrow{V_2^+=0} V_2 = V_2^-$$

Port 2 terminated with Z₀

$$S_{21} = \frac{V_2^-}{V_1^+} = \frac{V_2^-}{V_1^+} \cdot \frac{V_1^+}{V_1^+}$$

$$\frac{V_2^-}{V_1^+} = \frac{Z_2 // Z_0}{Z_1 + (Z_2 // Z_0)} = \frac{Z_2 Z_0}{Z_1 (Z_2 + Z_0) + Z_2 Z_0}$$

$$\frac{V_1^+}{V_1^+} = \frac{V_1^+ + V_1^-}{V_1^+} = \frac{V_1^+ / (1 + S_{11})}{V_1^+} = 1 + S_{11}$$

$$S_{21} = [1 + S_{11}] \frac{Z_2 Z_0}{Z_1 (Z_2 + Z_0) + Z_2 Z_0}$$

$$S_{12} = S_{21} \text{ by reciprocity}$$

Part b)

$$Z_1 = 30\Omega, Z_2 = 25\Omega, Z_0 = 50\Omega$$

$$S_{11} = \frac{(30-50)(25+50) + 25 \cdot 50}{(30+50)(25+50) + 25 \cdot 50} = 0.0909$$

$$S_{22} = -0.1273, \quad S_{21} = 0.5455, \quad S_{12} = 0.5455$$

$$S = \begin{bmatrix} 0.0909 & 0.5455 \\ 0.5455 & -0.1273 \end{bmatrix}$$

Part c)

Port 2 terminated in 50Ω ($= Z_0$)

$$VSWR = \frac{1+|P|}{1-|P|}, \quad P = S_{11} + \frac{S_{12}S_{21}Z_L}{1-S_{22}Z_L}$$
$$Z_L = \frac{Z_L - Z_0}{Z_L + Z_0} = 0 \quad \text{for } Z_L = Z_0$$

$$\Rightarrow |P| = 0.0909$$

$$\underline{VSWR = 1.2}$$

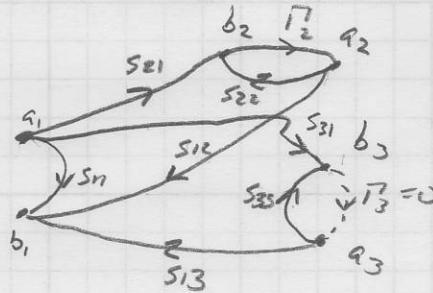
Problem 2

Part a) Reciprocal? Yes - $S = S^T$.

Part b) Input return loss:

$$RL = -20 \log_{10} |P| \text{ (dB)}$$

$T = \frac{b}{a_1} \rightarrow$ Flow graph approach:



$$I_2 = \frac{0 - Z_0}{0 + Z_0} = -1 \text{ (short)}$$

$$I_3 = \frac{Z_0 - Z_0}{Z_0 + Z_0} = 0 \text{ (open)}$$

First-order loops: $I_2 S_{22}$

$T = \frac{b_1}{a_1} \rightarrow$ Paths: $s_{11}, s_{21} I_2 s_{12}$

$$T = \frac{b_1}{a_1} = \frac{s_{11}[1 - I_2 s_{22}] + s_{21} I_2 s_{12}}{1 - I_2 s_{22}} = s_{11} + \frac{s_{21} I_2 s_{12}}{1 - I_2 s_{22}} = 0.00536 - j0.0166 = 0.0174 \angle -72^\circ$$

$$RL = -20 \log_{10} 0.0174 = -35.2 \text{ dB}$$

Part c)

Input impedance?

$$P = \frac{Z_{in} - Z_0}{Z_{in} + Z_0} \Rightarrow P(Z_{in} + Z_0) = Z_{in} - Z_0$$

$$Z_{in} = Z_0 \frac{1+P}{1-P}$$

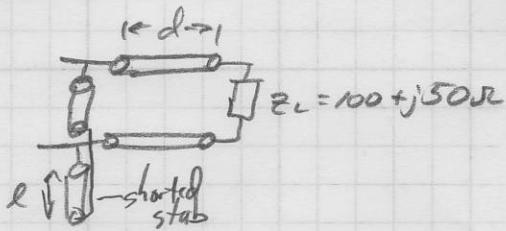
$$P = 0.0174 \angle -72^\circ$$

$$\Rightarrow Z_{in} = 50.5 - j1.68 \Omega = 50.53 \angle -1.9^\circ$$

Problem 3

Shunt-stub matching network:

All lines have
 $Z_0 = 50 \Omega$



$$\Rightarrow z_L = \frac{Z_L}{Z_0} = 2 + j$$

$$y_L = \frac{1}{z_L} = 0.4 - j0.2$$

Terminated line input impedance:

$$Z_{in} = Z_0 \frac{Z_L + jZ_0 \tan \beta d}{Z_0 + jZ_L \tan \beta d}$$

normalized:

$$Z_{in} = \frac{z_L + j \tan \beta d}{1 + j z_L \tan \beta d}$$

$$y_{in} = \frac{1 + j z_L \tan \beta d}{z_L + j \tan \beta d}$$

At end of "d" line, $y_{in} = 1 + j b$

$$\Rightarrow 1 + j b = \frac{1 + j(2 + j) \tan \beta d}{2 + j + j \tan \beta d}$$

$$(1 + j b)(2 + j(1 + \tan \beta d)) = 1 - \tan \beta d + j 2 \tan \beta d$$

Real part:

$$2 - b(1 + \tan \beta d) = 1 - \tan \beta d$$

Imag. part:

$$j 2b + j(1 + \tan \beta d) = j 2 \tan \beta d$$

2 eq., 2 unknowns (b , $\tan \beta d$)

$$\text{From Imag. part: } b = \frac{\tan \beta d - 1}{2}$$

From Imag. part:

$$2 - \frac{\tan \beta d - 1}{2}(1 + \tan \beta d) = 1 - \tan \beta d$$

$$\frac{5}{2} - \frac{1}{2} \tan^2 \beta d = 1 - \tan \beta d$$

$$\frac{1}{2} \tan^2 \beta d - \tan \beta d - \frac{3}{2} = 0$$

$$\tan \beta d = \frac{1 \pm \sqrt{1 + 4 \cdot \frac{1}{2} \cdot \frac{3}{2}}}{1} = 1 \pm 2 = -1, 3.$$

Two solutions

$$\tan \beta d = 3 \rightarrow b = 1$$

$$\tan \beta d = -1 \rightarrow b = -1$$

$$\tan \beta d = 3 \rightarrow \text{atan } 3 = \beta d = \frac{2\pi}{\lambda} d$$

$$\Rightarrow \frac{d}{\lambda} = \frac{\text{atan } 3}{2\pi} = 0.199$$

$$\tan \beta d = -1 \rightarrow \frac{d}{\lambda} = -0.125 \Rightarrow \frac{d}{\lambda} = 0.375 \text{ for length } > 0 \\ (\text{periodic } \sqrt{\text{period}} \lambda/2)$$

Stub design:

$$y_h = 1+jb \rightarrow \text{so stub provides } -jb$$

$$y_{h\text{stab}} = \frac{1+jz_t \tan \beta l}{z_t + j \tan \beta l}, \quad z_t = \text{stub termination impedance}$$

$$\text{short: } z_t = 0$$

$$y_{h\text{stab}} = \frac{1}{j \tan \beta l}$$

$$\text{For } d = 0.199\lambda \rightarrow b = +1 \Rightarrow y_{h\text{stab}} = -j \rightarrow \tan \beta l = 1 \\ l = 0.125\lambda$$

$$\text{For } d = 0.375\lambda, b = -1 \rightarrow y_{h\text{stab}} = +j \rightarrow \tan \beta l = -1 \\ l = -0.125 + 0.5 = 0.375\lambda$$

Solutions:

$$d_1 = 0.199\lambda, \quad l_1 = 0.125\lambda$$

OR

$$d_2 = 0.375\lambda, \quad l_2 = 0.375\lambda$$

Bonus

match 150Ω to 50Ω with series line

$\rightarrow \lambda/4$ transformer

$$Z_1 = \sqrt{Z_0 \cdot Z_L} = \sqrt{50 \cdot 150} = 86.6\Omega$$

$$\text{length} = \lambda/4$$

For lines available,

$$R=0, G=0 \rightarrow \text{lossless}$$

$$L = 8nH/cm$$

$$C = ?$$

$$Z_1 = 86.6\Omega = \sqrt{\frac{R+j\omega L}{G+j\omega C}} = \sqrt{\frac{L}{C}} \quad \text{for } R, G = 0$$

$$\Rightarrow C = \frac{L}{Z_1^2} = 1.07 \mu F/cm = C$$

Length of $\lambda/4$ transformer? (in physical units, e.g. cm)

$$\text{Propagation constant } \gamma = \sqrt{(R+j\omega L)(G+j\omega C)} = \alpha + j\beta$$

$$R, G = 0 \rightarrow \gamma = j\beta = j\omega\sqrt{LC}$$

$$\beta = \omega\sqrt{LC} = \frac{2\pi}{\lambda}$$

$$\lambda = \frac{2\pi}{\omega\sqrt{LC}} = \frac{1}{f\sqrt{LC}}$$

$$f = 10 \text{ GHz}, L = 8nH/cm, C = 1.07 \mu F/cm$$

$$\Rightarrow \lambda = 1.0825 \text{ cm}$$

$$\Rightarrow \text{length of line} = \frac{\lambda}{4} = 0.271 \text{ cm}$$