

**NAME: SOLUTION**

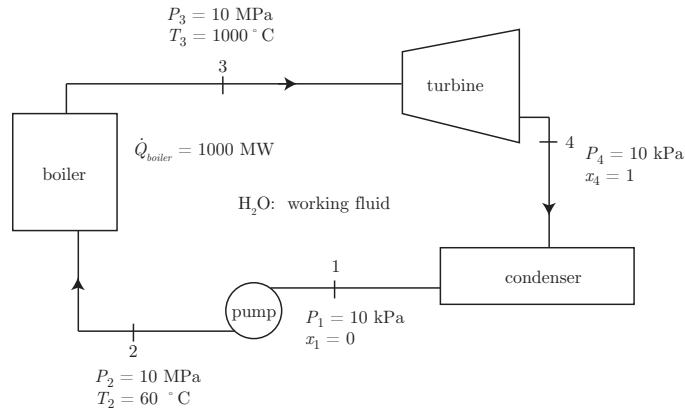
AME 20231, Thermodynamics

Examination 2

Prof. J. M. Powers

13 April 2021

1. (40) Consider the Rankine cycle below. Find



- the mass flow rate (kg/s),
- the work rate done by the turbine (kW),
- the work rate required to power the pump (kW),
- the overall thermal efficiency,
- a correctly oriented sketch, including the vapor dome and appropriate numerical values of  $P$  and  $v$ , of the cycle on a  $P - v$  diagram,

**Solution**

The tables give us

$$h_1 = 191.81 \frac{\text{kJ}}{\text{kg}}, \quad h_2 = 259.47 \frac{\text{kJ}}{\text{kg}}, \quad h_3 = 4611.04 \frac{\text{kJ}}{\text{kg}}, \quad h_4 = 2584.63 \frac{\text{kJ}}{\text{kg}}$$

$$v_1 = 0.001010 \frac{\text{m}^3}{\text{kg}}, \quad v_2 = 0.001013 \frac{\text{m}^3}{\text{kg}}, \quad v_3 = 0.05832 \frac{\text{m}^3}{\text{kg}}, \quad v_4 = 14.67355 \frac{\text{m}^3}{\text{kg}}$$

For the boiler we have

$${}_2q_3 = h_3 - h_2 = \left( 4611.04 \frac{\text{kJ}}{\text{kg}} \right) - \left( 259.47 \frac{\text{kJ}}{\text{kg}} \right) = 4351.57 \frac{\text{kJ}}{\text{kg}}$$

So we have

$${}_2\dot{Q}_3 = \dot{m} {}_2q_3$$

$$\dot{m} = \frac{{}_2\dot{Q}_3}{{}_2q_3} = \frac{10^6 \text{ kW}}{4351.57 \frac{\text{kJ}}{\text{kg}}} = \boxed{229.802 \frac{\text{kg}}{\text{s}}}$$

The specific turbine work is

$${}_3w_4 = h_3 - h_4 = \left( 4611.04 \frac{\text{kJ}}{\text{kg}} \right) - \left( 2584.63 \frac{\text{kJ}}{\text{kg}} \right) = 2026.41 \frac{\text{kJ}}{\text{kg}}$$

So the turbine power output is

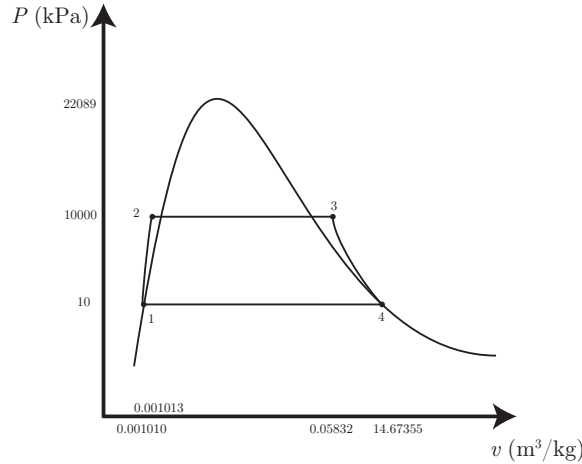
$${}_3\dot{W}_4 = \dot{m} {}_3w_4 = \left( 229.802 \frac{\text{kg}}{\text{s}} \right) \left( 2026.41 \frac{\text{kJ}}{\text{kg}} \right) = \boxed{465673 \text{ kW}}$$

For the pump, we need the following work

$${}_1\dot{W}_2 = \dot{m}(h_1 - h_2) = \left(229.802 \frac{\text{kg}}{\text{s}}\right) \left(191.81 \frac{\text{kJ}}{\text{kg}}\right) - \left(259.47 \frac{\text{kJ}}{\text{kg}}\right) = \boxed{-15548.4 \text{ kW}}$$

So the thermal efficiency is

$$\eta = \frac{\dot{W}_{net}}{\dot{Q}_{in}} = \frac{(465673 \text{ kW}) - (15548.4 \text{ kW})}{10^6 \text{ kW}} = \boxed{0.450125}$$



2. (30) A chamber with initial volume  $V_1 = 1 \text{ m}^3$  contains air at  $P_1 = 100 \text{ kPa}$ ,  $T_1 = 300 \text{ K}$ . The air is constrained by a piston attached to a *linear spring*. The air is heated to  $T_2 = 3000 \text{ K}$ ,  $P_2 = 200 \text{ kPa}$ . Find the heat transfer  ${}_1Q_2$  assuming air is a
- calorically perfect ideal gas, (use Table A.5),
  - calorically imperfect ideal gas (use Table A.7.1).
  - Give a one-sentence, qualitative, physics-based interpretation as to why one estimate is different than the other.

### Solution

The ideal gas law gives us

$$\begin{aligned} \frac{P_2 V_2}{T_2} &= \frac{P_1 V_1}{T_1} \\ V_2 &= \frac{P_1 T_2}{P_2 T_1} V_1 \\ V_2 &= \frac{100 \text{ kPa} \cdot 3000 \text{ K}}{200 \text{ kPa} \cdot 300 \text{ K}} (1 \text{ m}^3). \\ V_2 &= 5 \text{ m}^3. \end{aligned}$$

Now we know that for a linear spring  ${}_1W_2 = \int_1^2 P dV$  gives us the area of a trapezoid, which is

$$\begin{aligned} {}_1W_2 &= \frac{P_1 + P_2}{2} (V_2 - V_1) \\ {}_1W_2 &= \frac{100 \text{ kPa} + 200 \text{ kPa}}{2} (5 \text{ m}^3 - 1 \text{ m}^3) \\ {}_1W_2 &= 600 \text{ kJ} \end{aligned}$$

The first law then gives us

$$U_2 - U_1 = {}_1Q_2 - {}_1W_2$$

$$\begin{aligned} {}_1Q_2 &= U_2 - U_1 + {}_1W_2 \\ {}_1Q_2 &= m(u_2 - u_1) + {}_1W_2 \end{aligned}$$

Now, we have

$$\begin{aligned} m &= \frac{P_1 V_1}{RT_1} \\ m &= \frac{(100 \text{ kPa})(1 \text{ m}^3)}{\left(0.287 \frac{\text{kJ}}{\text{kg K}}\right) (300 \text{ K})} \\ m &= 1.16144 \text{ kg} \end{aligned}$$

For a CPIG, we have  $u_2 - u_1 = c_v(T_2 - T_1)$ , and we take  $c_v = 0.717 \text{ kJ/kg/K}$ , so

$$\begin{aligned} {}_1Q_2 &= mc_v(T_2 - T_1) + {}_1W_2 \\ {}_1Q_2 &= (1.16144 \text{ kg}) \left(0.717 \frac{\text{kJ}}{\text{kg K}}\right) ((3000 \text{ K}) - (300 \text{ K})) + 600 \text{ kJ} \end{aligned}$$

$$\boxed{{}_1Q_2 = 2848.43 \text{ kJ}}$$

For the CIIG, we have from the tables  $u_2 = 2664.27 \text{ kJ/kg}$ ,  $u_1 = 214.36 \text{ kJ/kg}$ . So

$${}_1Q_2 = (1.16144 \text{ kg}) \left( \left(2664.27 \frac{\text{kJ}}{\text{kg}}\right) - \left(214.36 \frac{\text{kJ}}{\text{kg}}\right) \right) + 600 \text{ kJ}$$

$$\boxed{{}_1Q_2 = 3445.54 \text{ kJ}}$$

For diatomic molecules, more heat is needed because some energy goes to vibrational and rotational modes.

3. (30) A 1 kg block of silver and a 1 kg block of gold are within a closed, thermally insulated chamber. The silver has initial temperature  $T_S(0) = 1000 \text{ K}$ , and the gold has initial temperature  $T_G(0) = 300 \text{ K}$ . The two blocks come to a thermal equilibrium so that they have same final temperature.

- (a) Find the equilibrium temperature.  
 (b) Taking as a crude model for the heat transfer rate *from* silver to gold

$$\dot{Q} = \left(0.001 \frac{\text{kW}}{\text{K}}\right) (T_S - T_G),$$

find the time constant of equilibration.

### Solution

For this problem, there is no work, so  $\dot{W} = 0$ . For the silver and gold blocks, we have from the first law

$$\frac{dU_S}{dt} = -\dot{Q}, \quad \frac{dU_G}{dt} = \dot{Q}$$

Adding the two we see

$$\frac{d}{dt}(U_S + U_G) = 0$$

That is to say the thermal energy of the combined system is conserved. So

$$U_S + U_G = (U_S + U_G)|_{t=0}$$

Using the relation for a solid with constant specific heat that  $U$  is proportional to  $mcT$ , we can say

$$m_S c_S T_S + m_G c_G T_G = m_S c_S T_{S_0} + m_G c_G T_{G_0}$$

For us  $m_S = m_G = m$ , so we could say

$$c_S T_S + c_G T_G = c_S T_{S_0} + c_G T_{G_0}$$

So at a general time, we could say

$$T_G(t) = \frac{c_S(T_{So} - T_S(t)) + c_G T_{Go}}{c_G}$$

$$T_G(t) = \frac{c_S}{c_G}(T_{So} - T_S(t)) + T_{Go}$$

At the equilibrium state,  $T_S = T_G = T_E$ , so

$$c_S T_E + c_G T_E = c_S T_{So} + c_G T_{Go}$$

$$T_E = \frac{c_S T_{So} + c_G T_{Go}}{c_S + c_G}$$

$$T_E = \frac{\left(0.24 \frac{\text{kJ}}{\text{kg K}}\right) (1000 \text{ K}) + \left(0.13 \frac{\text{kJ}}{\text{kg K}}\right) (300 \text{ K})}{\left(0.24 \frac{\text{kJ}}{\text{kg K}}\right) + \left(0.13 \frac{\text{kJ}}{\text{kg K}}\right)}$$

$$\boxed{T_E = 754.054 \text{ K}}$$

We can rewrite the first law for silver as

$$m c_S \frac{dT_S}{dt} = -h(T_S - T_G)$$

$$m c_S \frac{dT_S}{dt} = -h \left( T_S - \left( \frac{c_S}{c_G} (T_{So} - T_S) + T_{Go} \right) \right)$$

$$m c_S \frac{dT_S}{dt} = -h \left( T_S \left( 1 + \frac{c_S}{c_G} \right) - \left( \frac{c_S}{c_G} T_{So} + T_{Go} \right) \right)$$

$$\frac{dT_S}{dt} = -\frac{h}{m c_S} \left( T_S \left( 1 + \frac{c_S}{c_G} \right) - \left( \frac{c_S}{c_G} T_{So} + T_{Go} \right) \right)$$

By inspection, the time constant is

$$\tau = \frac{m c_S}{h \left( 1 + \frac{c_S}{c_G} \right)} = \frac{(1 \text{ kg}) \left( 0.24 \frac{\text{kJ}}{\text{kg K}} \right)}{\left( 0.001 \frac{\text{kW}}{\text{K}} \right) \left( 1 + \frac{0.24 \frac{\text{kJ}}{\text{kg K}}}{0.13 \frac{\text{kJ}}{\text{kg K}}} \right)} = \boxed{84.32 \text{ s}}$$

As an aside, we can divide top and bottom by  $c_S$  to rewrite  $\tau$  as

$$\tau = \frac{m}{h \left( \frac{1}{c_S} + \frac{1}{c_G} \right)}$$

Defining  $c_{hm}$  as the *harmonic mean specific heat*:

$$c_{hm} = \frac{2}{\frac{1}{c_S} + \frac{1}{c_G}}$$

we could say

$$\tau = \frac{m c_{hm}}{2h}$$

One can solve for the differential equations and get

$$T_S(t) = (754.054 \text{ K}) + (245.946 \text{ K}) \exp(-t/(84.32 \text{ s}))$$

$$T_G(t) = (754.054 \text{ K}) - (454.054 \text{ K}) \exp(-t/(84.32 \text{ s}))$$

