

# A theoretical study for one-dimensional modeling for VOC in a catalytic converter

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Combustion Theory and Modeling

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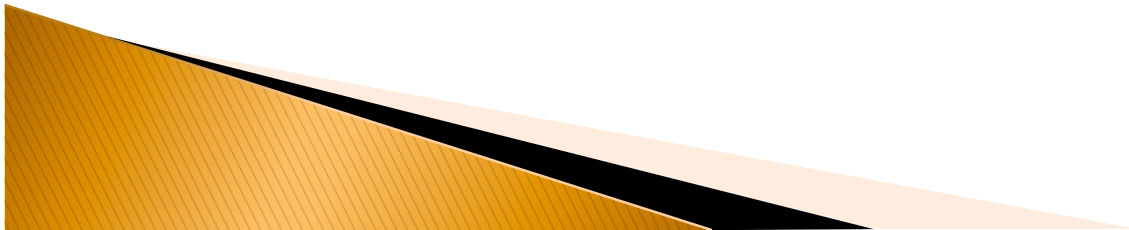
Srivastave V.K.



# The Problem

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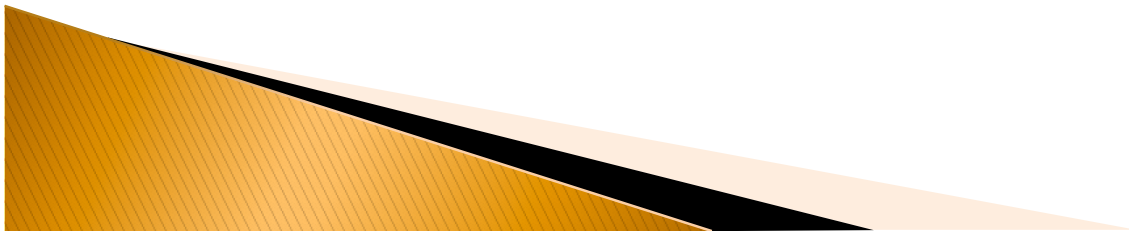
- ▶ VOC – (volatile organic compound)
  - produced from vehicular emissions
  - exposure–health risks
    - deteriorate air quality
    - damage crops
  - Ex. CO, NO<sub>x</sub>, aldehydes
  - increasing restrictions of the emissions of these compounds



# Catalytic Combustion

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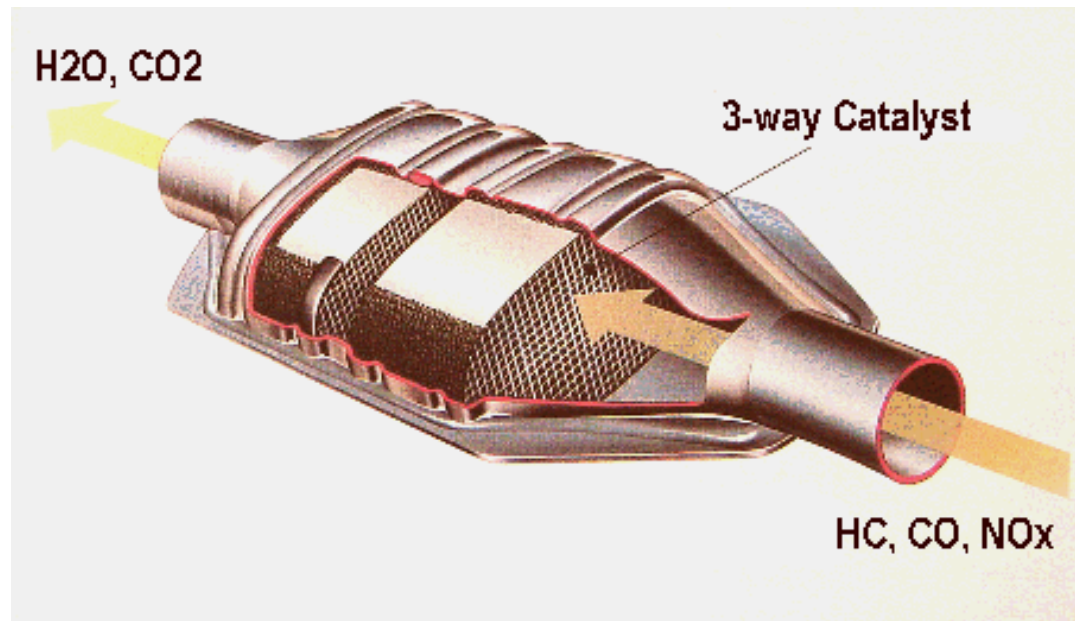
- ▶ Thermal combustion of pollutants requires high temp and produces harmful products
- ▶ Catalyst lowers required combustion temp
- ▶ Products are  $\text{H}_2\text{O}$  and  $\text{CO}_2$
- ▶ Combustion occurs on the surface of the catalyst
- ▶ Process is highly efficient



# Catalytic Converter

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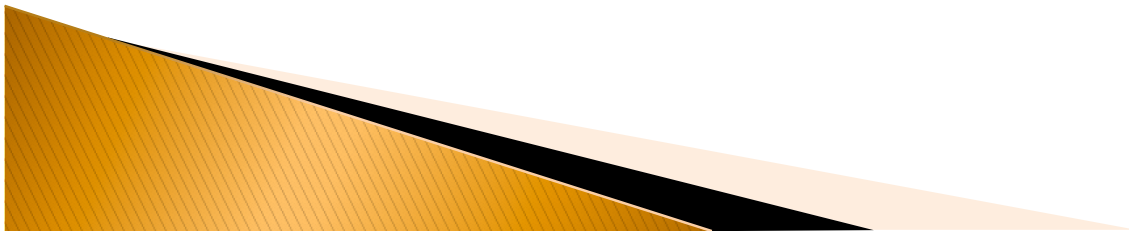
- ▶ Monolithic Catalysts
  - “honeycomb catalysts”
  - Platinum and Palladium serve as catalyst



# Purpose

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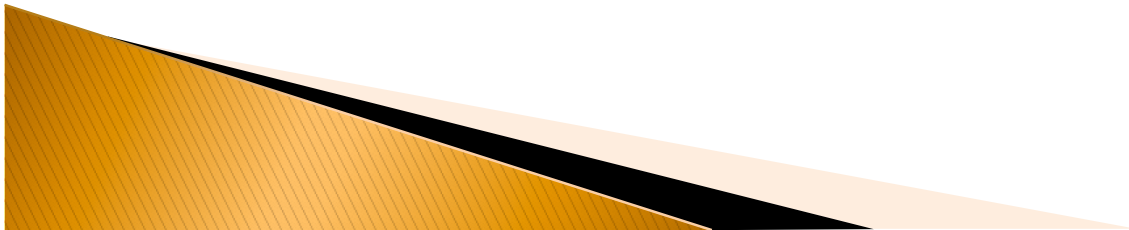
- ▶ Create a mathematical model of a monolithic catalyst in the warm up period
- ▶ Model
  - Combustion of acetaldehyde ( $\text{CH}_3\text{CHO}$ )
  - Platinum as catalyst
  - Utilize one dimensional unsteady state model mass and energy balance eqn. for solid and gas phases
  - Solve using the Backward Implicit Method



# Assumptions

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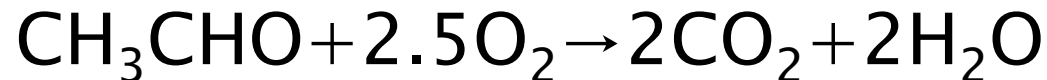
- Negligible axial diffusion in gas phase.
- Noble metal (catalyst) concentration was kept constant and the catalyst does not deactivate.
- Monolith is cylindrical with circular cross-section channels.
- Gas phase concentration, temperature, velocity and the solid temperature are uniform across the monolith cross-section at any axial position.
- The heat released by the catalytic reactions inside the washcoat was totally transported to the gas phase by convection.
- Heat transfer by radiation within channels and also heat exchange between the substrate and the surroundings at both inlet and an outlet face of the monolith is neglected.
- Non-uniform flow distribution inside the converter is neglected, as one single channel represents the entire monolith.
- Reactor operates in laminar flow region, with fully developed flow in greater part of the reactor and therefore the reacting species are transferred to the wall by molecular diffusion.



# Kinetics

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- ▶ Reaction

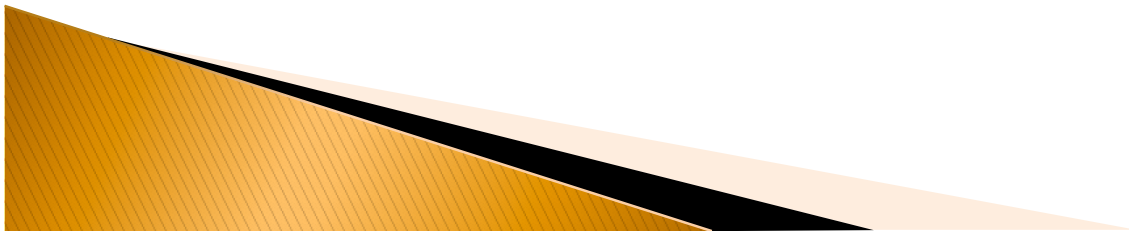


- Irreversible

- ▶ Reaction rate

$$(-r)_{\text{VOC}} = k_0 \exp(-E/RT_s) C_i$$

- Pre-exponential Factor:  $k_0 = 46.18 \text{ m/s}$
- Activation Energy:  $E = 36,374 \text{ J/mol}$





# Equations

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- ▶ Mass balance in gas phase:

$$v \left( \frac{\partial C_g}{\partial x} \right) + k_g S (C_g - C_s) = \left( \frac{\partial C_g}{\partial t} \right)$$

- ▶ Mass balance in solid phase:

$$a(-r)_{VOC} = k_g S (C_g - C_s)$$

- ▶ Energy balance in gas phase:

$$-v \rho_g C p_g \left( \frac{\partial T_g}{\partial x} \right) - h S (T_g - T_s) = \rho_g C p_g \left( \frac{\partial T_g}{\partial t} \right)$$

- ▶ Energy balance in solid phase:

$$\rho_s C p_s \left( \frac{\partial T_s}{\partial t} \right) = a(-\Delta H)(-r)_{VOC} + h S (T_g - T_s) + \lambda_s \left( \frac{\partial^2 T_s}{\partial x^2} \right)$$





# Boundary Conditions

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- ▶ Entering acetaldehyde concentration through time:

$$C_g(0, t) = C_g^0$$

- ▶ Entering gas temp through time:

$$T_g(0, t) = T_g^0$$

- ▶ Catalyst temp at  $t=0$ :

$$T_s(x, 0) = T_s^0$$

- ▶ Converter entrance:

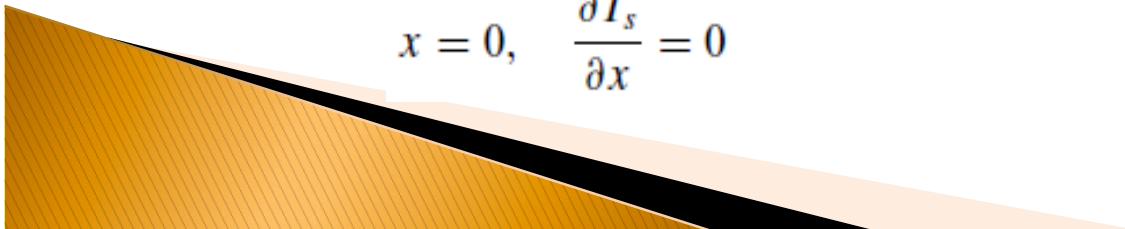
$$x = 0, \quad \frac{\partial T_s}{\partial x} = 0$$

- ▶ Converter exit:

$$x = L, \quad \frac{\partial T_s}{\partial x} = 0$$

$$x = L, \quad \frac{\partial C_g}{\partial x} = 0$$

$$x = L, \quad \frac{\partial T_g}{\partial x} = 0$$



# Results

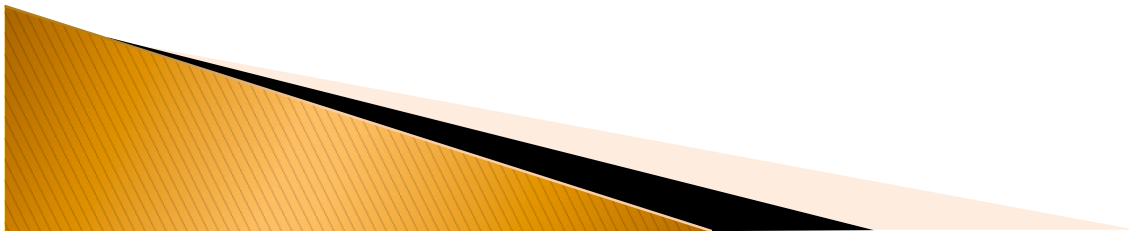
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- ▶ Calculated values:

- Acetaldehyde concentration
- Gas temperature
- Solid Catalyst Temperature

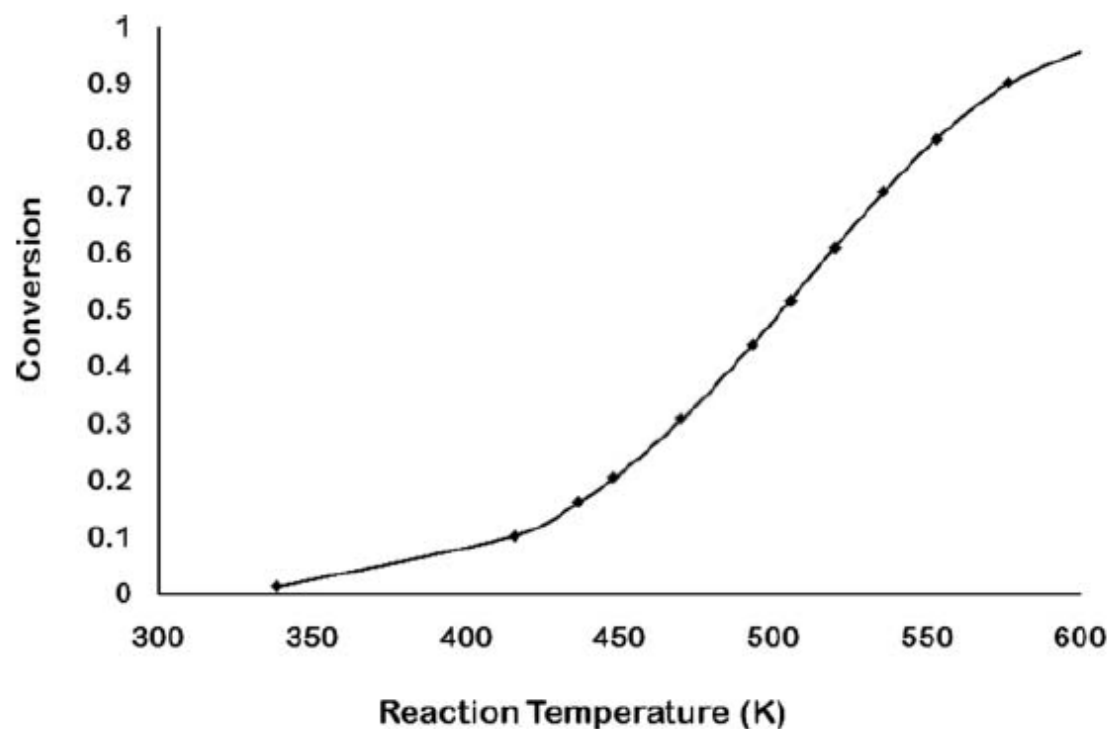
- ▶ Findings:

- Temperature of the converter slowly raised
- Reaction started when converted reached operating temperature
- Decrease in acetaldehyde due to reaction
  - Decrease to 1.000 to .200 (dimensionless)



# Conversion of Acetaldehyde with time

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2. Conversion of acetaldehyde (100 ppm) with respect to reaction temperature.

# Concentration Variation along length

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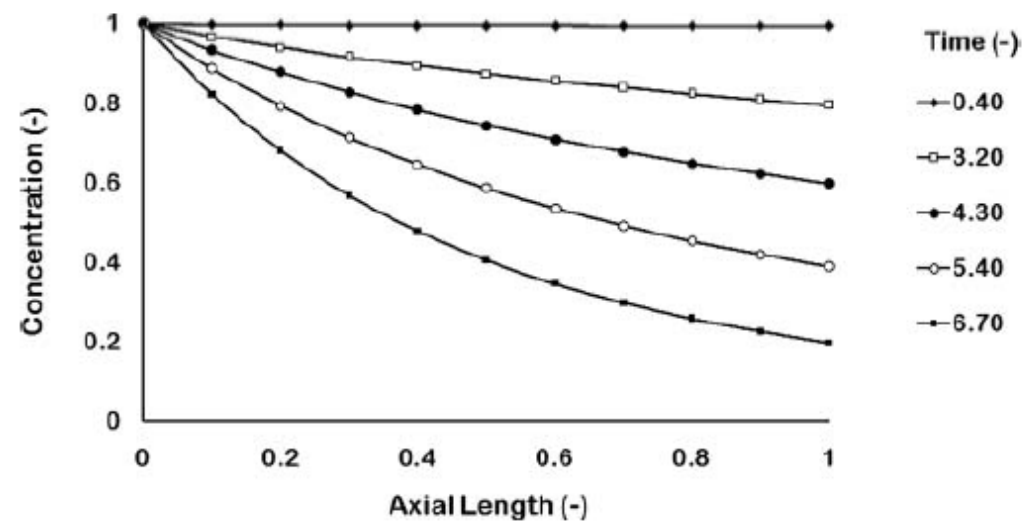


Figure 3. Concentration variation of acetaldehyde (100 ppm) at 723 K along the axial length.

# Exit Concentration with respect to time: with varying inlet temperatures

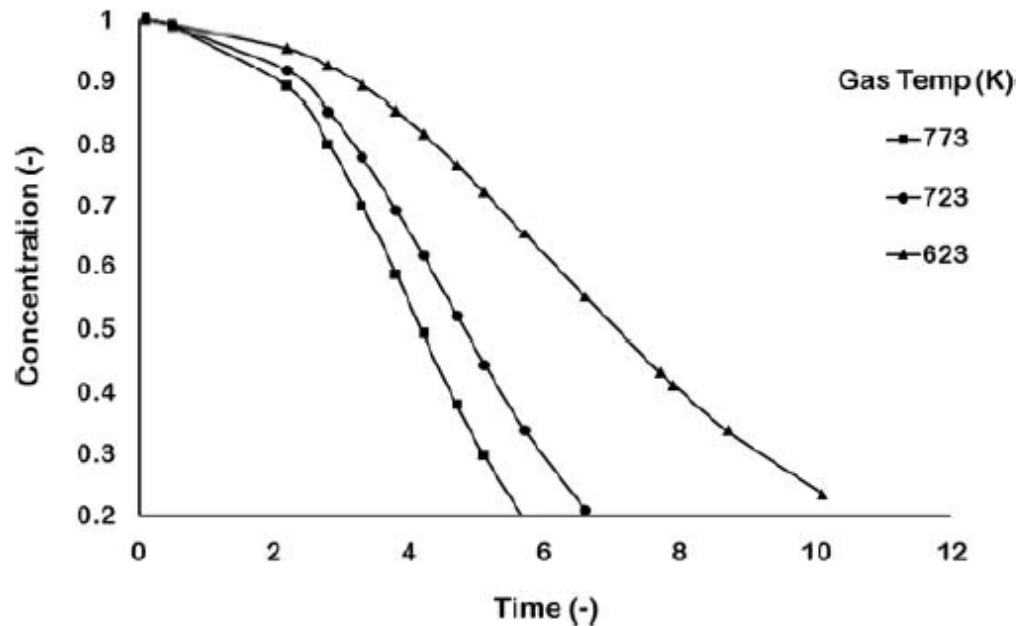


Figure 4. Exit concentration variation of acetaldehyde (100 ppm) with respect to time for different gas inlet temperatures.

# Exit Concentration of Acetaldehyde with Aged and New Catalyst

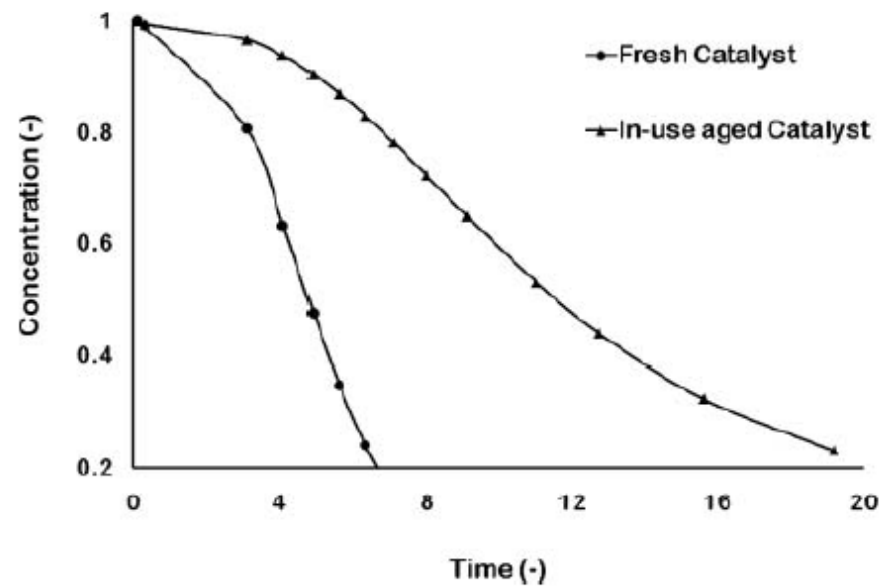


Figure 5. Exit concentration variation for acetaldehyde gas (100 ppm) at 723 K with time for fresh and in use aged catalyst.