

Shock-Fitted Calculation of Unsteady Detonation in Ozone

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An ultra-fine, sub-micron discrete grid is used to capture the unsteady dynamics of a one-dimensional detonation in an inviscid $O - O_2 - O_3$ mixture. The ultra-fine grid is necessary to capture the length scales revealed by a complementary analysis of the steady detonation wave structure. For the unsteady calculations, shock-fitting coupled with a high order spatio-temporal discretization scheme combine to render numerical corruption negligible. As a result, mathematically verified solutions for a mixture initially of all O_3 at one atmosphere and 298.15 K have been obtained; the solutions are converging at a rate much faster than the sub-first order convergence rate of all shock-capturing schemes. Additionally, the model has been validated against limited experimental data. Transient calculations show that strongly overdriven waves are stable and moderately overdriven waves unstable.

I. Introduction

RECENTLY, a shock-fitting method¹ coupled with a high order spatial discretization² was used to fully capture the unsteady dynamics of an inviscid one-dimensional detonation for the case of pulsating detonations which obey simple one step kinetics.¹ The high accuracy of the method enabled the prediction of a rich set of bifurcation phenomena, including a transition to chaos at a rate consistent with the geometric progression characterized by Feigenbaum's constant. Formal grid convergence studies revealed that the error was converging at a rate approaching the fifth order error of the spatio-temporal discretization employed. The key to obtaining such results was the use of a shock-fitting technique so as to avoid the corrupting influences of common shock-capturing methods. Convergence rates for shock-capturing methods are at or below first order, even if nominally high order methods are used in smooth regions of the flow.²

Here, we extend this approach by introducing a more realistic detailed kinetics model, which introduces additional length scales, relative to the one-step model. With an analysis of spatial eigenvalues, Powers and Paolucci³ have shown for inviscid hydrogen-air detonations that the length scales for steady Chapman-Jouguet (CJ) detonations can span over five orders of magnitude: near equilibrium, the smallest length scale is $\sim 10^{-5}$ cm and the largest is $\sim 10^0$ cm; away from equilibrium, the breadth can be larger. Resolving this wide range of scales, necessary for a mathematically verified and scientifically repeatable calculation, poses a daunting challenge. Adaptive methods^{4,5} can be used effectively when extended to the viscous regime, but for inviscid flows, there remain fundamental difficulties in formally adapting a grid to a shock discontinuity.

The fine reaction scales can be attributed to the fact that constitutive laws for detailed kinetics models are a manifestation of an averaged representation of a molecular collision model in which the fundamental length scale is the mean free path.^{6,7} This suggests that collision-based mass, momentum, and energy diffusion, which has a role at such fine scales, should be modeled as well. However, we choose here to defer such calculations to the future, and in this paper introduce only resolved detailed kinetics coupled with advective

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transport. Certainly, there is an extensive literature (*cf.* Fedkiw, *et al.*,⁸ Oran, *et al.*,⁹ Hu, *et al.*,¹⁰ Wang, *et al.*,¹¹ Walter and da Silva,¹² He and Karagozian,¹³ or Tsuboi, *et al.*¹⁴) which makes the same inviscid assumption. Notably, Tsuboi, *et al.*, in their recent calculations that required significant super-computer resources, employ grids sizes near 10^{-4} *cm* for their three-dimensional unsteady calculations of detonations in hydrogen-air, and report strong sensitivity of wave dynamics to the fineness of the grid. Consequently, we believe assessment of the common inviscid approach, stripped here from the method-dependent distortions of numerical diffusion, is a useful exercise, even if one ultimately wants to consider models with more physical richness.

In this paper, we consider an ozone-based mixture, $O - O_2 - O_3$, in which, relative to hydrogen-air, there are fewer reactions, and the range of length scales is smaller ($\sim 10^5$ for hydrogen-air, $\sim 10^3$ for ozone). This reduction of the number of reactions, and more importantly, the range of scales, enables the resolved computation to be completed in a reasonable time. Kinetics for this system are well characterized,¹⁵⁻¹⁷ and limited experimental data for ozone detonation are available.¹⁸ We give a brief synopsis of the mathematical model and computational method. This is followed by a validation of the model by comparison of the predictions of steady state detonation waves with experimental data. We then perform unsteady simulations at two different levels of overdrive. The stronger overdrive yields a stable solution which converges to the independent predictions of the steady wave model. The weaker overdrive induces an unstable, galloping detonation. We close with brief conclusions.

II. Mathematical Model

The governing equations are the one-dimensional reacting Euler equations for a mixture of calorically imperfect ideal gases which react via mass action kinetics. They are of the form

$$\frac{\partial q_i}{\partial t} + \frac{\partial f_i(q_j)}{\partial x} = g_i(q_j), \quad (1)$$

where Eq. (1) represents the conservation of mass, linear momentum, and energy, as well as the evolution of molecular species. These are supplemented by a standard set of constitutive equations to complete the system. Full details of the model equations have been previously published.³ Here q_i is a vector of state variables, f_i is a flux of the state variables, and g_i is a reaction source, also a function of the state variables. Time is t , and x is the distance coordinate. Equation (1) is valid in smooth regions of the flow, and represents a set of hyperbolic partial differential equations. The set admits discontinuities propagating at speed D . Equation (1) is not valid across such a discontinuity and must be supplemented by a set of Rankine-Hugoniot jump conditions, which take the form

$$D(t) = \frac{f_i^s - f_i^o}{q_i^s - q_i^o}, \quad (2)$$

where D is the time-dependent shock speed, s denotes the shocked state, and o the unshocked state.

We employ a three step, three species (O, O_2, O_3) model. The reaction mechanism is that of Hirschfelder, *et al.*¹⁵ as used later by Margolis¹⁶ and Singh, *et al.*,¹⁷ each of whom provide numerical values of rate constants.



Here M represents an inert third body, taken to have a collision efficiency of unity.

III. Computational Method

For spatially dependent steady wave calculations, a double precision FORTRAN-77 code has been developed and linked with the International Mathematical and Statistical Libraries (IMSL) routines DFDJAC for Jacobian evaluation, DEVLRG for eigenvalue estimation, a double precision version of the public domain edition of the CHEMKIN package^{19,20} to obtain kinetic rates and thermodynamics properties, and the standard LSODE²¹ solver to yield highly accurate solutions to the governing ordinary differential equations. Typical run times on a Linux-based desktop computer were ten seconds.

For transient calculations, the shock-fitting strategy of Henrick *et al.*¹ has been adapted to allow for an arbitrary number of chemical species as well as general equations of state, suitable to interface with the CHEMKIN package. The underlying numerical scheme is a method of lines with fifth order upwind-central spatial and fifth order Runge-Kutta temporal discretization. Special one-sided differences were utilized near the shock, as well as a shock state being enforced as a boundary condition. Typical run times on Macintosh desktop computer were two hours.

IV. Results

Here, we report a series calculations for ozone detonations with an initial mass fraction composition of $Y_{O_3} = 1$, $Y_{O_2} = 0$, $Y_O = 0$ at 298.15 K and 1.01325×10^6 dyne/cm².

IV.A. Validation for steady near-CJ wave

For such a system, Streng, *et al.*¹⁸ report an observed *CJ* velocity of $1.863 \times 10^5 \pm 2 \times 10^3$ cm/s. From equilibrium thermochemistry using no kinetics, they calculated a equilibrium temperature, equilibrium pressure, and detonation wave speed of 3340 K, 3.1188×10^7 dyne/cm², and 1.878×10^5 cm/s, respectively.

Using the method of Powers and Paolucci,³ for steady waves, one can employ conservation of mass, momentum, energy, atomic elements to reduce the system to two ordinary differential equations. These are solved from the shock state to the equilibrium end state. This results in an equilibrium temperature, equilibrium pressure, and detonation wave speed of 3571.4 K, 3.4111×10^7 dyne/cm², and 1.936555×10^5 cm/s, respectively. Our mixture required a detonation velocity slightly above the *CJ* velocity, so as to avoid sonic singularities within the reaction zone. This slight overdrive, as well as uncertainties in the equations of state used in the study of Streng, *et al.* likely explain the small discrepancies.

IV.B. Stable Strongly Overdriven

We next consider a strongly overdriven case in which the overdrive is such that the steady detonation speed is 2.5×10^5 cm/s.

IV.B.1. Steady Structure

Again with the method of Powers and Paolucci,³ the spatial distribution of dependent variables can be calculated; additionally, the spatial eigenvalues of the local Jacobian matrix can be found, and local length scales predicted. Because the system can be reduced to two coupled ordinary differential equations, there are two fundamental length scales in play. These length scales are attributable to the combined effects of advection and reaction. The length scale analysis reveals that in the near post-shock zone of the detonation, the fine and coarse scales are 6.4×10^{-8} and 2.7×10^{-7} cm, respectively. Near equilibrium, the fine and coarse scales are 2.9×10^{-7} and 5.8×10^{-4} cm, respectively. Figure 1 shows a plot of the evolution of the magnitudes of the resulting two length scales of the system. The two length scales coincide near $x = 10^{-6}$ cm. This is due to the spatial eigenvalues becoming complex conjugate pairs, with equal real parts, in this thin zone. The length scales here were based on the real part of the eigenvalues only. One could easily adjust the figure in this zone to include the length scale of oscillation, manifested in the imaginary component of the eigenvalue; this would have limited value.

In the zone extremely near the shock, $x < 10^{-8}$ cm, the continuum model predicts power law growth of the *O* and *O*₂ species mass fraction, as seen in Figure 2. This growth modulates at the beginning of the induction zone, near $x = 5 \times 10^{-8}$ cm, which correlates well with the finest length scale in this region. The induction zone terminates near $x = 1.8 \times 10^{-7}$ cm. At this point, vigorous reaction commences. The system first relaxes to a partial equilibrium at $x = 4 \times 10^{-6}$ cm, stays on a plateau for a few decades, and relaxes to final equilibrium near $x = 10^{-3}$ cm. The global length scale is well estimated by the longest length scale predicted by the spatial eigenvalue analysis.

Plots of temperature and pressure versus distance are shown in Figures 3 and 4, respectively. Here the two disparate length scales are most clearly manifested in the initial relaxation process commencing near $x = 10^{-7}$ cm and the final relaxation commencing near $x = 10^{-4}$ cm. It appears that the main temperature rise around $x = 10^{-7}$ cm is attributable to *O*₃ converting to *O*₂ over the short length scale. All species then are in a partial equilibrium over several decades of length until a final, smaller temperature drop occurs

around $x = 10^{-4}$ cm, which close examination reveals may be due to O_3 and O coming into final equilibrium. The final temperature and pressure are 4285.8 K and 9.2554×10^7 dyne/cm², respectively.

It is lastly noted that in all plots for clarity, we give predictions, formally admitted by the continuum model, down to length scales slightly below 10^{-9} cm. Of course, the continuum model is only physically valid down to length scales at or above the mean free path scale, which for this system can be roughly estimated to be $\sim 10^{-7}$ cm. This correlates well with the finest length scale prediction from the spatial eigenvalue analysis. One can argue, with some justification, that at such fine length scales, one should account for physical diffusive transport. Here, we simply note that there is a long history of solving reactive Euler equations with detailed kinetics, and that there is value in seeing what such models predict when the distortion of numerical diffusion is rendered small by use of fine grids.

IV.B.2. Transient Behavior

Performing time-dependent shock-fitted computations on this strongly overdriven detonation reveals that the one-dimensional detonation is stable. The calculation was initialized with the highly resolved steady solution of the previous section. Figure 5 shows the computed detonation velocity versus time for three spatial resolutions. For this stable case, the steady solution is the exact solution for all time; any differences between the steady solution and that obtained with the transient code are consequences of the slightly coarser (but still ultra-fine) grid used in the transient calculation. This can also serve as a test problem for verification of the numerical scheme. It is demonstrated in Figure 5 that under resolution, the solution tends towards the exact solution of $D(t) = 2.5 \times 10^5$ cm/s. Furthermore, the solution is very accurate; relative percent errors in the detonation velocity at $t = 10^{-9}$ s are, from lowest to highest resolution, 0.44%, 0.1% and 0.012%. The grids employed had spatial resolutions of $\Delta x = 1 \times 10^{-7}$, 5×10^{-8} , and 2.5×10^{-8} cm, with corresponding number of grid points of 1×10^4 , 2×10^4 , and 4×10^4 . The domain length was 10^{-3} cm. Although these errors are diminishing superlinearly, the point of asymptotic convergence in error has yet to be reached.

IV.C. Unstable Moderately Overdriven

We next consider a moderately overdriven case, in which the overdrive is such that the steady detonation speed is 2.0×10^5 cm/s, if transients were suppressed.

IV.C.1. Steady Structure

By suppressing transients, and solving for formally steady structures, one obtains predictions similar in character those for the strongly overdriven case. The near shock length scales of evolution are 2.32×10^{-7} cm and 4.24×10^{-6} cm. Near equilibrium, the length scales relax to 1.71×10^{-6} cm and 5.54×10^{-3} cm. The induction zone is 1.85×10^{-6} cm, and the final temperature and pressure are 3728.7 K and 4.5368×10^7 dyne/cm², respectively.

IV.C.2. Transient Behavior

In contrast to the strongly overdriven case, the moderately overdriven case of $D = 2.0 \times 10^5$ cm/s is unstable. The small numerical perturbations initially grow exponentially, before inducing severe non-linear oscillations. The calculation stops at $t = 3.29 \times 10^{-9}$ s because the severe temperatures which result are out of the range of validity of the caloric equation of state. Figure 6 shows the computed detonation velocity versus time.

V. Conclusions

It has been demonstrated that mathematically verified unsteady detonation dynamics can be predicted when sub-micron structures, admitted by continuum detailed kinetics models, are captured with ultra-fine grids. Furthermore, shock-fitting coupled with high order spatio-temporal discretization assures negligible numerical corruption of solutions to the underlying partial differential equations. Predicted detonation dynamics for the detailed kinetics of ozone are qualitatively similar to previously studied one-step models.¹ It is also noted that at these fine length scales, which are comparable to molecular mean free paths, diffusion will play a role and should be included in future work.

Acknowledgments

This work was performed under the auspices of the United States Department of Energy.

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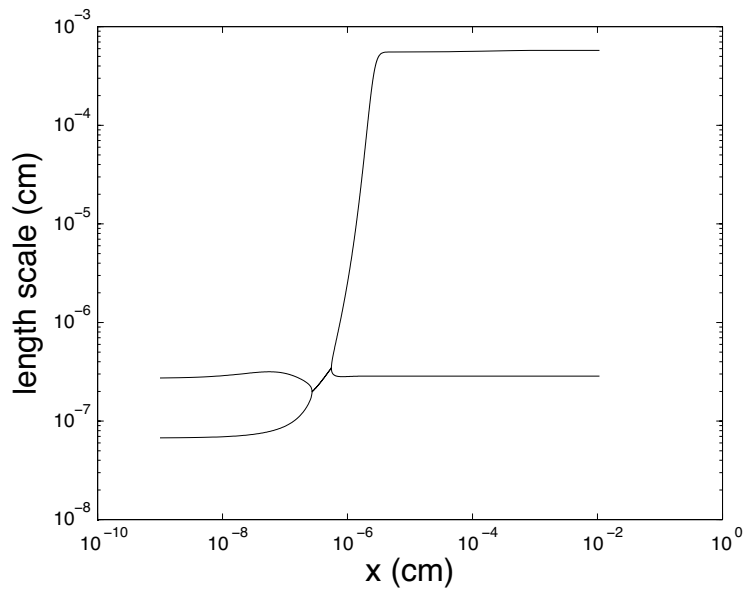


Figure 1. Reaction length scales versus distance in steady strongly overdriven ozone detonation.

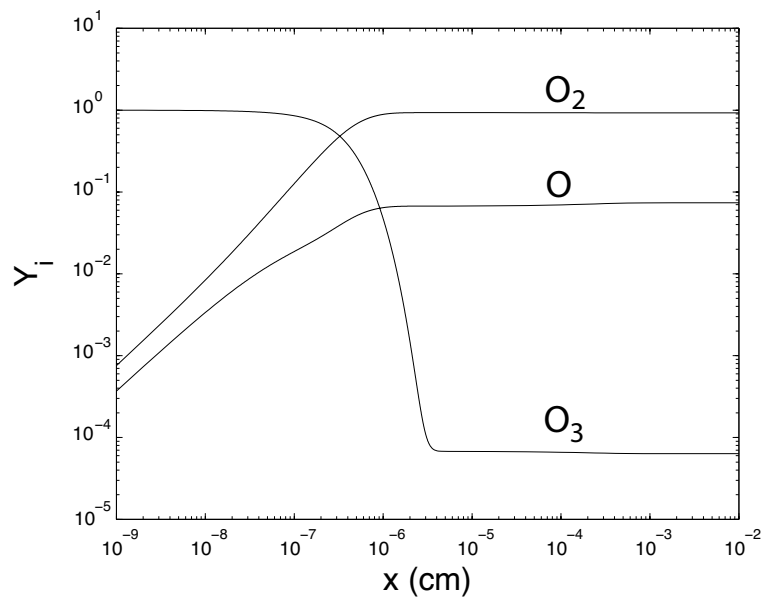


Figure 2. Species mass fraction versus distance in steady strongly overdriven ozone detonation.

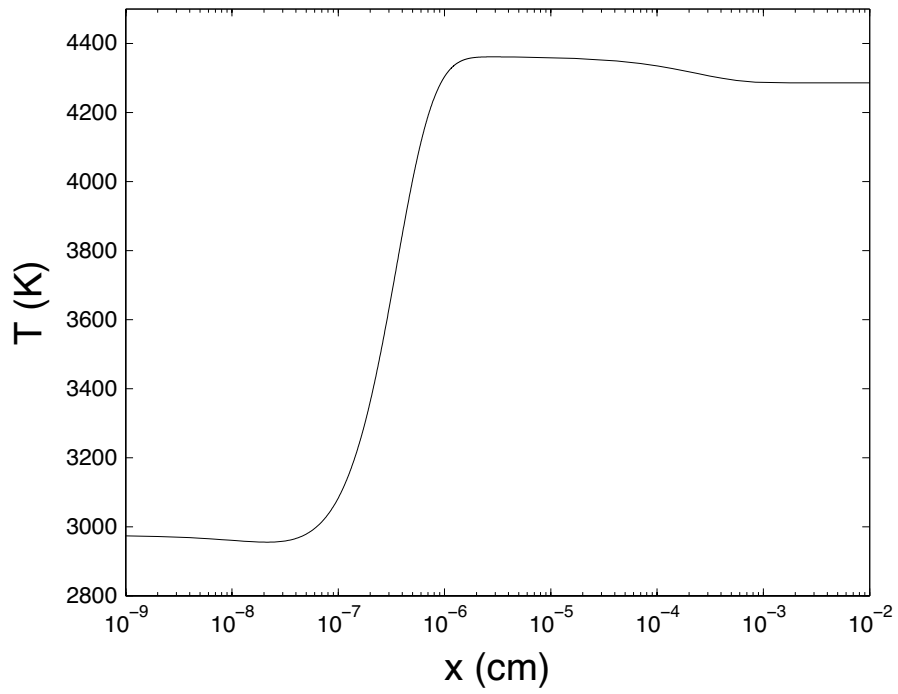


Figure 3. Temperature versus distance in steady strongly overdriven ozone detonation.

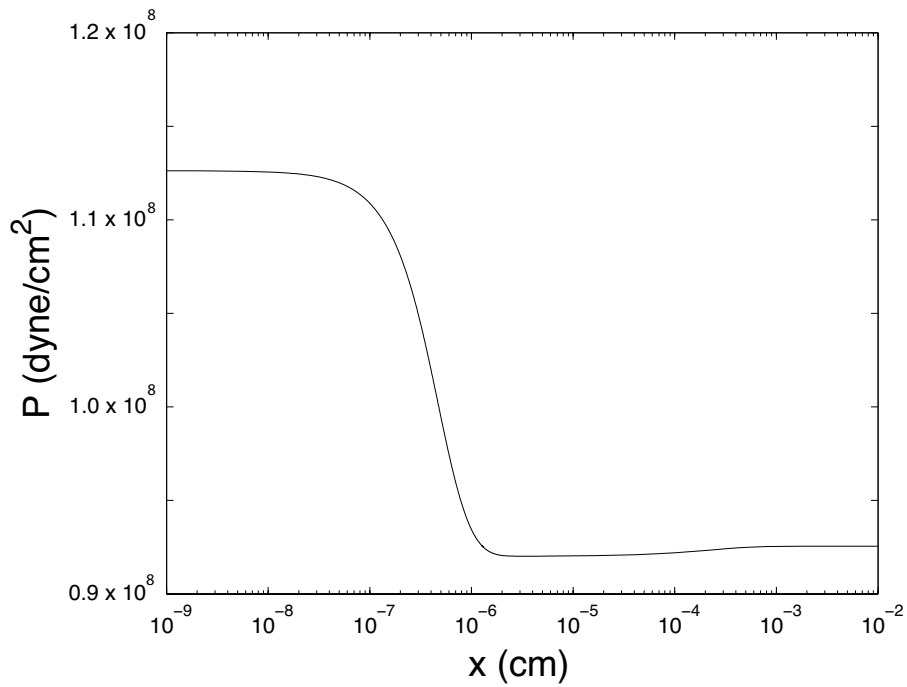


Figure 4. Pressure versus distance in steady strongly overdriven ozone detonation.

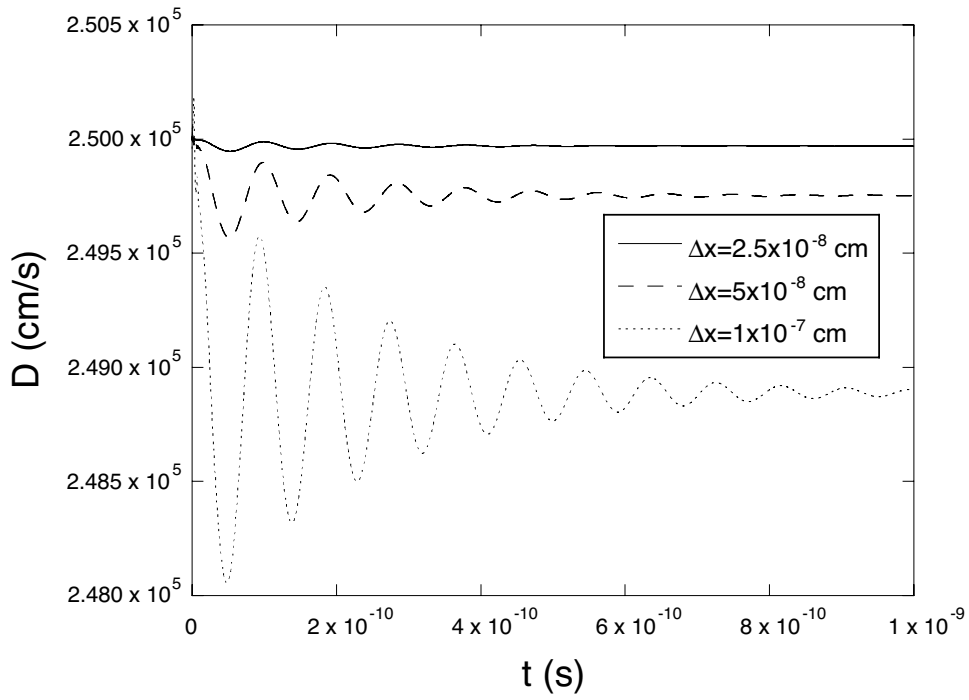


Figure 5. Computed shock velocity versus time in unsteady strongly overdriven ozone detonation.

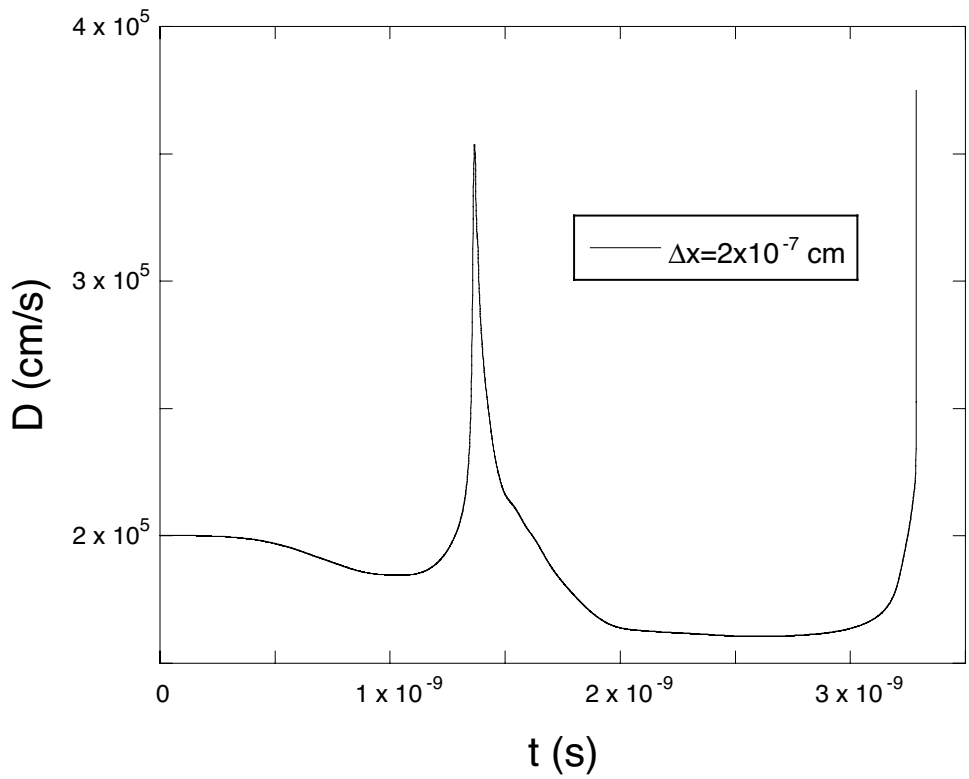


Figure 6. Computed shock velocity versus time in unsteady moderately overdriven ozone detonation.