

# Verification and Validation of Premixed Laminar Flames

*Joseph M. Powers, Ashraf N. Al-Khateeb, Samuel Paolucci*

Department of Aerospace and Mechanical Engineering

University of Notre Dame, Notre Dame, Indiana

9<sup>th</sup> US National Congress on Computational Mechanics

San Francisco, California

25 July 2007



UNIVERSITY OF  
NOTRE DAME

# Objectives

- To give detailed evidence that a **mathematically verified** estimate for the finest length scale in a continuum model of a premixed laminar flame with detailed kinetics is  $\mathcal{O}(10^{-4} \text{ cm})$ .
- To show such a continuum model can be **macro-validated** by comparing predictions of flames speeds to observations, while noting  $10^{-4} \text{ cm}$ -scale structures are too fine for present-day combustion diagnostics.

# Mathematical Model

## Governing Equations

$$\begin{aligned}\frac{\partial \rho}{\partial \tilde{t}} &= -\frac{\partial}{\partial \tilde{x}}(\rho \tilde{u}), \\ \frac{\partial}{\partial \tilde{t}}(\rho \tilde{u}) &= -\frac{\partial}{\partial \tilde{x}}(\rho \tilde{u}^2 + p - \tau), \\ \frac{\partial}{\partial \tilde{t}}\left(\rho \left(e + \frac{\tilde{u}^2}{2}\right)\right) &= -\frac{\partial}{\partial \tilde{x}}\left(\rho \tilde{u} \left(e + \frac{\tilde{u}^2}{2} + \frac{p}{\rho} - \frac{\tau}{\rho}\right) + J^q\right), \\ \frac{\partial}{\partial \tilde{t}}(\rho Y_i) &= -\frac{\partial}{\partial \tilde{x}}(\rho \tilde{u} Y_i + J_i^m) + \dot{\omega}_i M_i, \quad i = 1, \dots, N - 1.\end{aligned}$$

## Constitutive Relations

$$J_i^m = \rho \sum_{\substack{k=1 \\ k \neq i}}^N \frac{M_i D_{ik} Y_k}{M} \left( \frac{1}{\chi_k} \frac{\partial \chi_k}{\partial \tilde{x}} + \left( 1 - \frac{M_k}{M} \right) \frac{1}{p} \frac{\partial p}{\partial \tilde{x}} \right) - D_i^T \frac{1}{T} \frac{\partial T}{\partial \tilde{x}},$$

$$J^q = q + \sum_{i=1}^N J_i^m h_i - \Re T \sum_{i=1}^N \frac{D_i^T}{M_i} \left( \frac{1}{\chi_i} \frac{\partial \chi_i}{\partial \tilde{x}} + \left( 1 - \frac{M_i}{M} \right) \frac{1}{p} \frac{\partial p}{\partial \tilde{x}} \right),$$

$$\dot{\omega}_i = \sum_{j=1}^J \nu_{ij} a_j T^{\beta_j} \exp \left( \frac{-\bar{E}_j}{\bar{R}T} \right) \left( \prod_{k=1}^N \bar{\rho}_k^{\nu'_{kj}} \right) \left( 1 - \frac{1}{K_{c,j}} \prod_{k=1}^N \bar{\rho}_k^{\nu_{kj}} \right)$$

$$q = -k \frac{\partial T}{\partial \tilde{x}},$$

$$p = \Re T \sum_{i=1}^N \frac{\rho Y_i}{M_i},$$

and others ...

## Dynamical System Formulation

- PDEs  $\longrightarrow$  ODEs

$$\frac{d}{dx}(\rho u) = 0,$$

$$\frac{d}{dx}(\rho u h + J^q) = 0,$$

$$\frac{d}{dx}(\rho u Y_l^e + J_l^e) = 0, \quad l = 1, \dots, L - 1,$$

$$\frac{d}{dx}(\rho u Y_i + J_i^m) = \dot{\omega}_i M_i, \quad i = 1, \dots, N - L.$$

- ODEs  $\longrightarrow$  DAEs

$$\mathbf{A}(\mathbf{z}) \cdot \frac{d\mathbf{z}}{dx} = \mathbf{f}(\mathbf{z}).$$

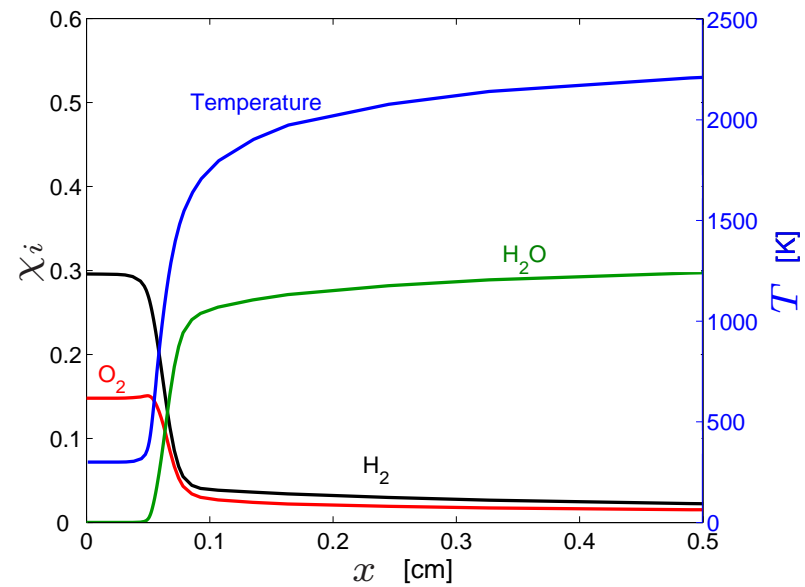
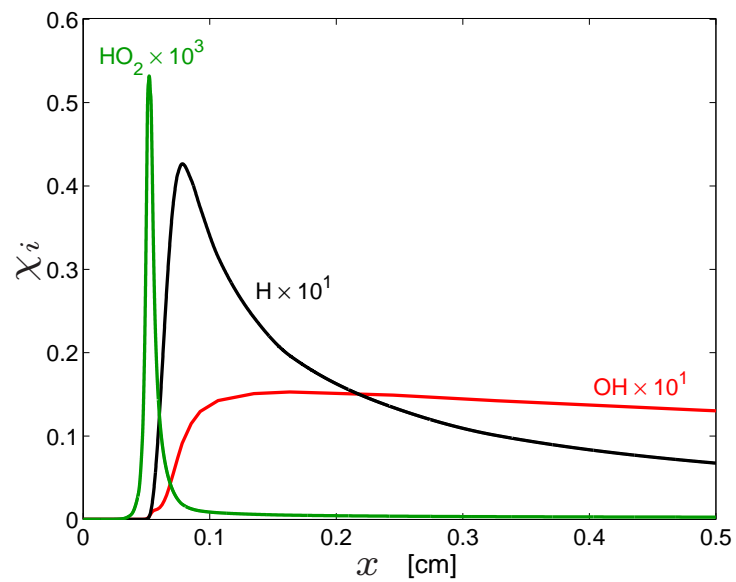
# Results

## Steady Laminar Premixed Hydrogen-Air Flame

- $N = 9$  species,  $L = 3$  atomic elements, and  $J = 19$  reversible reactions,
- Stoichiometric Hydrogen-Air:  $2H_2 + (O_2 + 3.76N_2)$ ,
- $p_o = 1 \text{ atm}$ ,
- CHEMKIN and IMSL are employed.

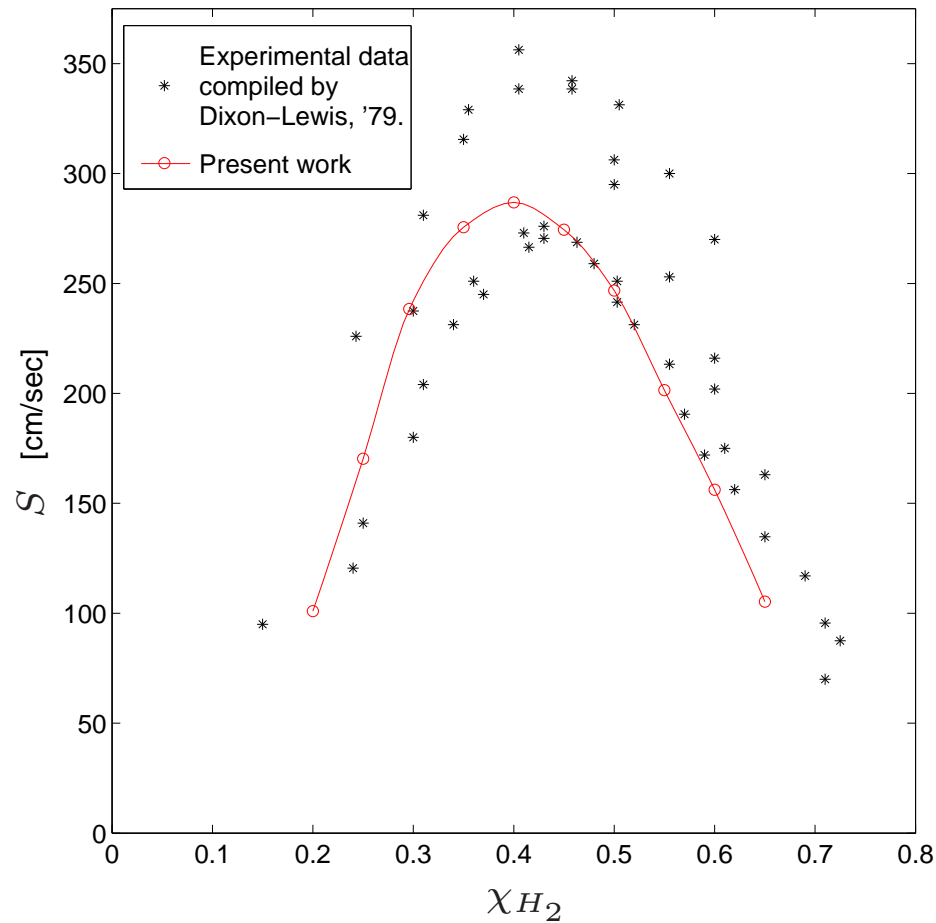
## Macro-Mathematical Verification

- Good “picture norm” agreement with Smooke *et al.*, ‘83.



## Macro-Experimental Validation

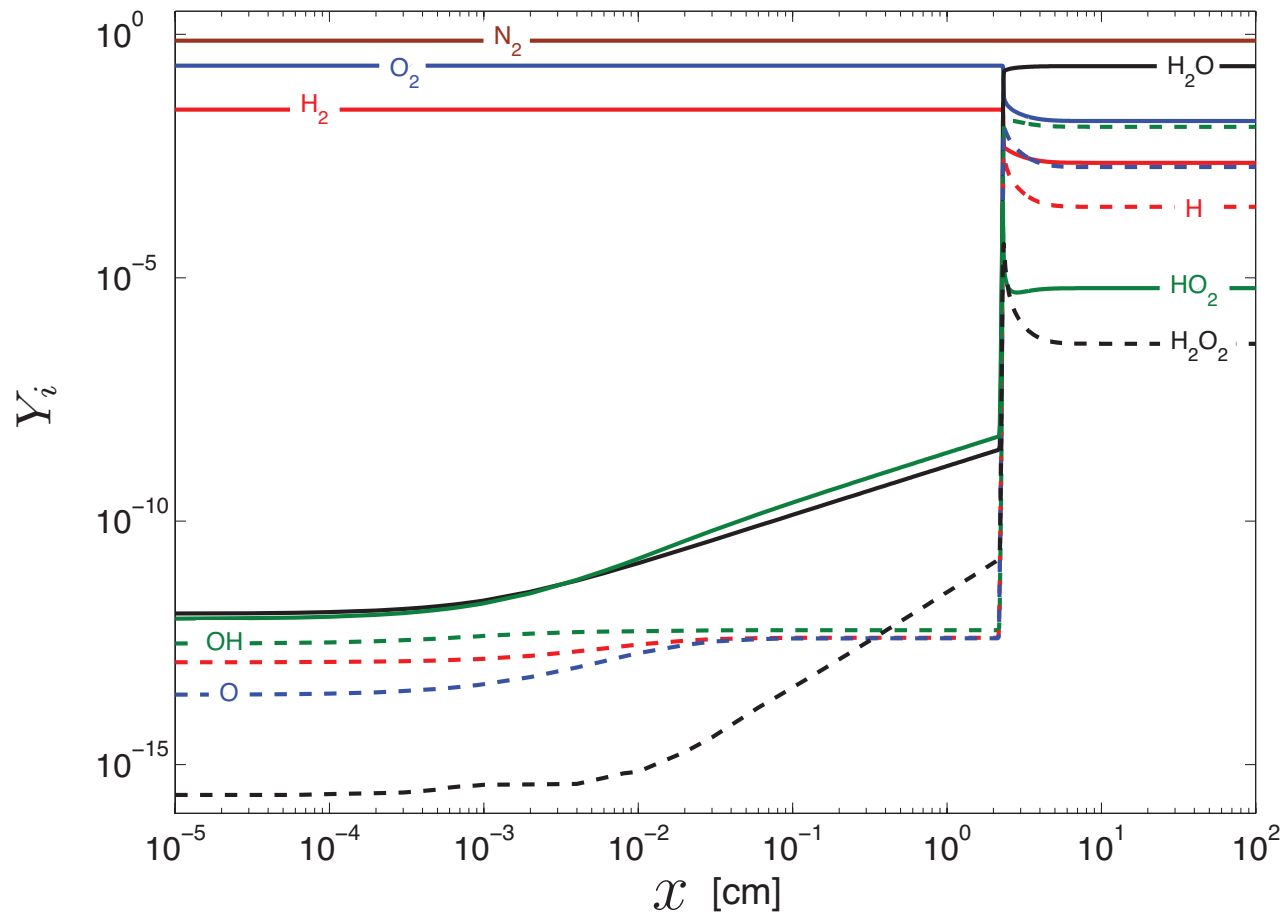
- Good agreement with flame speed data (Dixon-Lewis, '79).





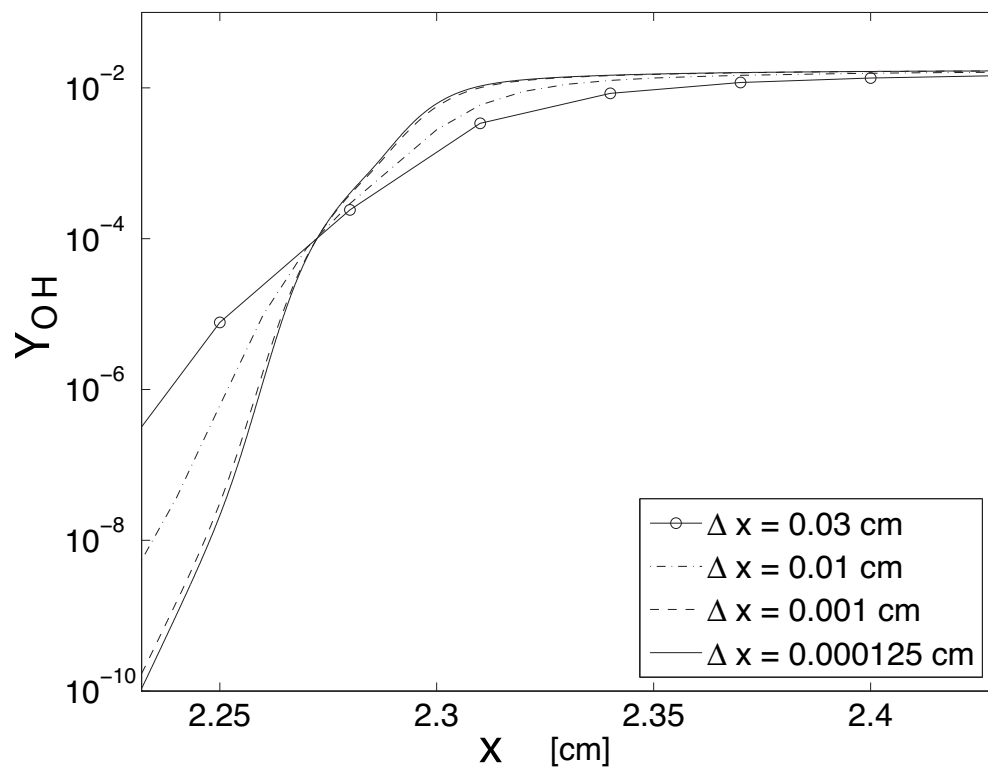
# Micro-verification: log-log plot reveals structure at $10^{-4}$ cm

- mass fractions versus distance

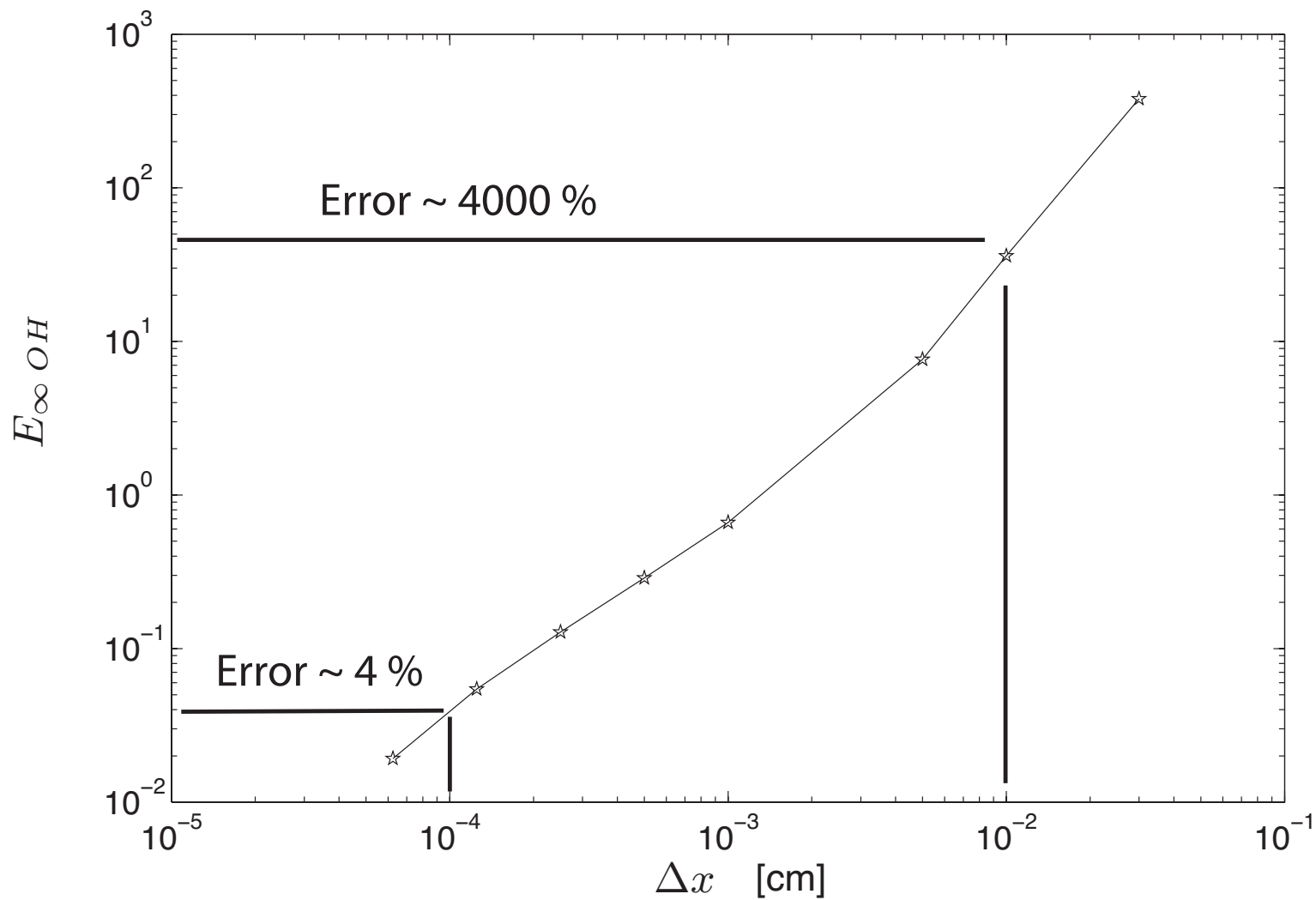


## Variation of grid shows physical scales are at $O(10^{-4})$ cm

- 4000% error in  $Y_{OH}$  when  $\Delta x = 10^{-2}$  cm!
- 4% error in  $Y_{OH}$  at  $\Delta x \sim 10^{-4}$  cm.

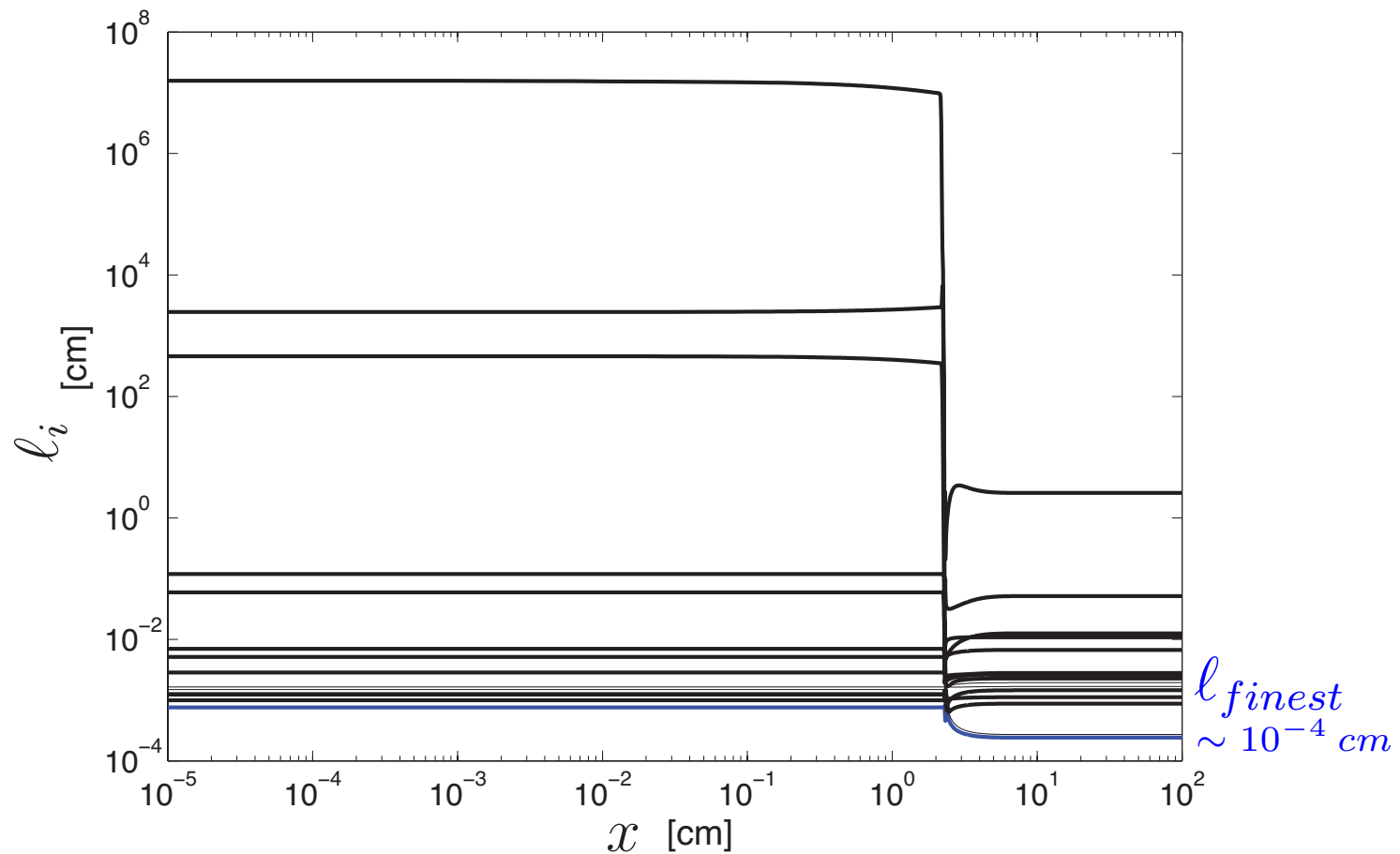


**Grid convergence shows physical scales are at  $O(10^{-4})$  cm**



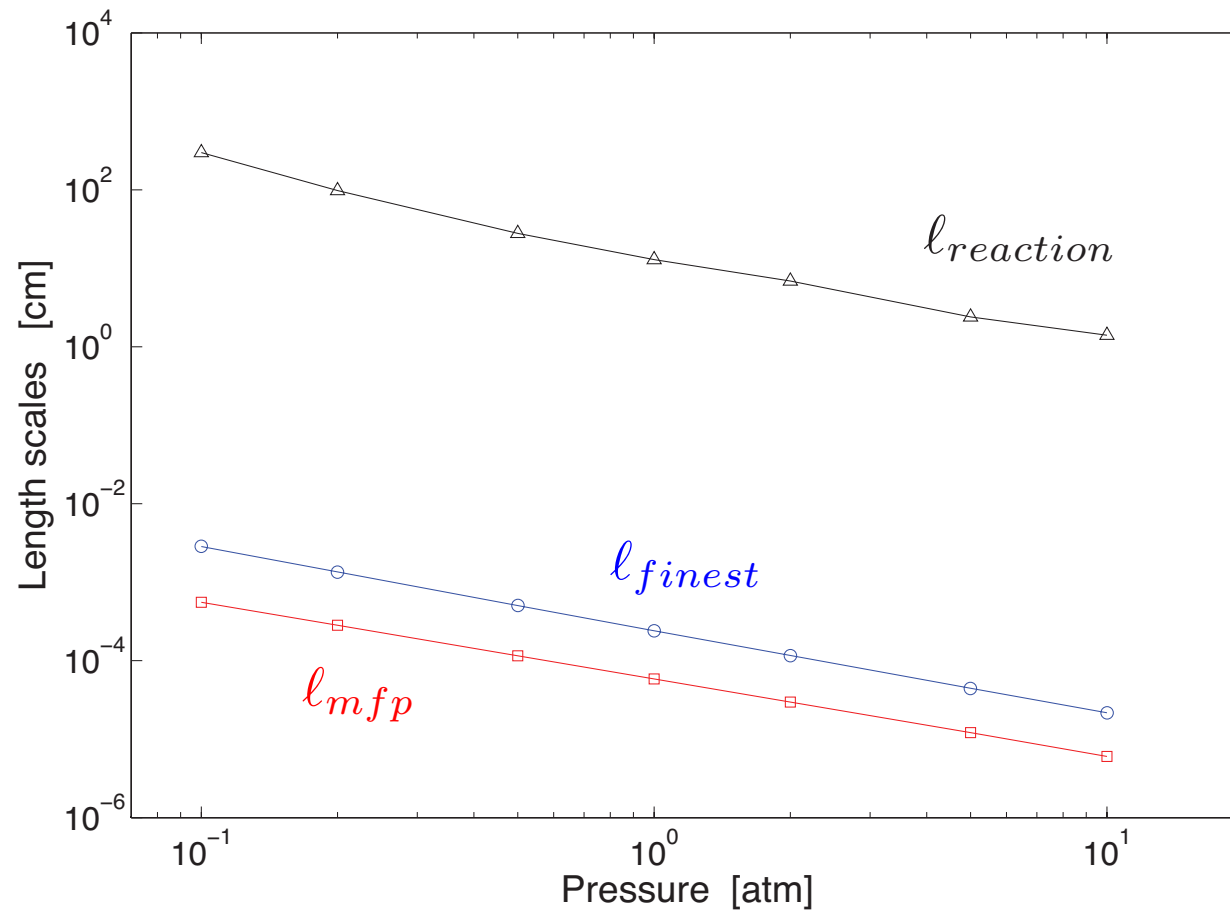
**Spatial eigenvalue analysis shows scales are  $O(10^{-4})$  cm**

- Found from generalized eigenvalues of  $\mathbf{A}(\mathbf{z}) \cdot d\mathbf{z}/dx = \mathbf{f}(\mathbf{z})$ .

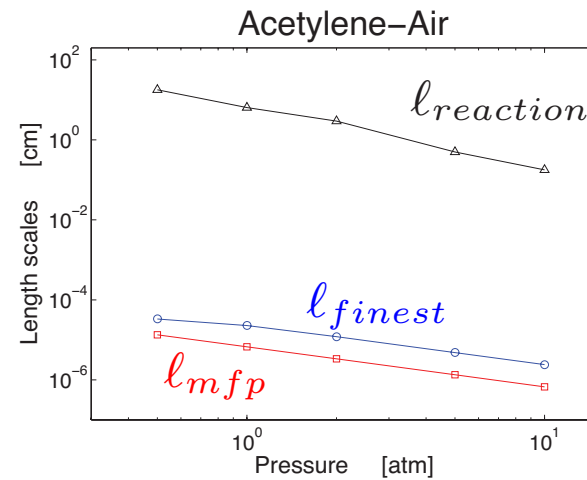
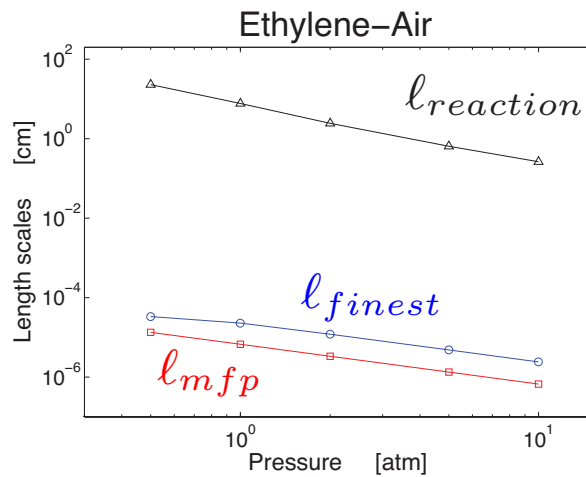
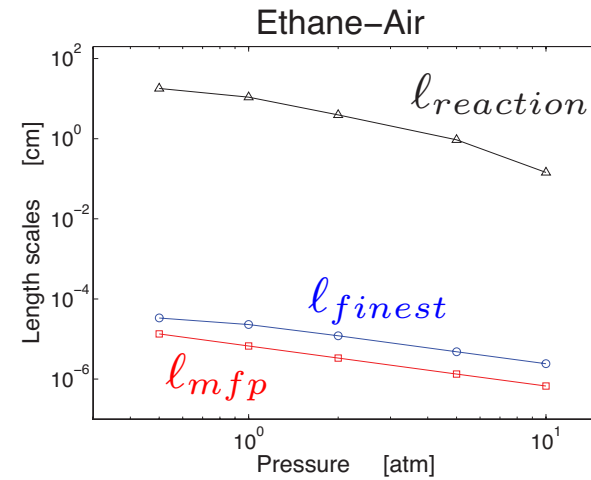
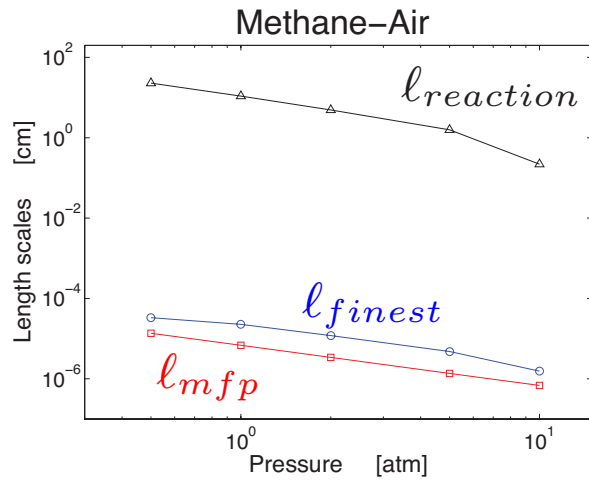


## Mean free path estimates shows scales are $O(10^{-4})$ cm

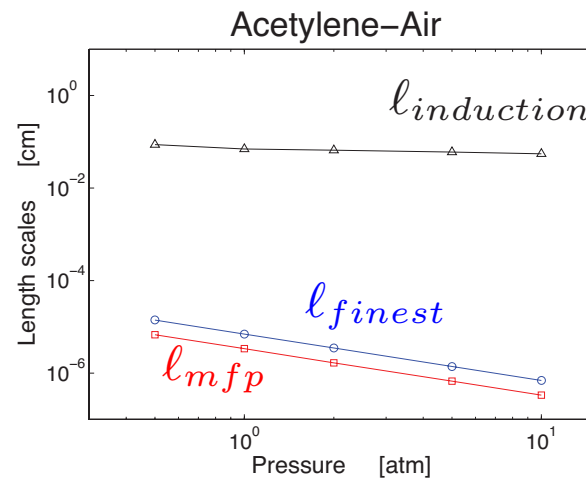
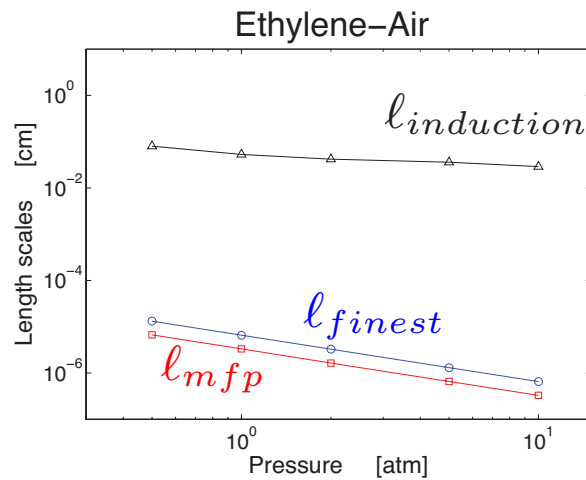
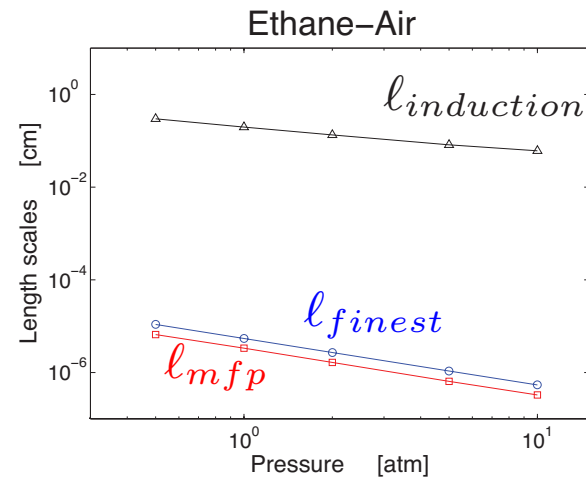
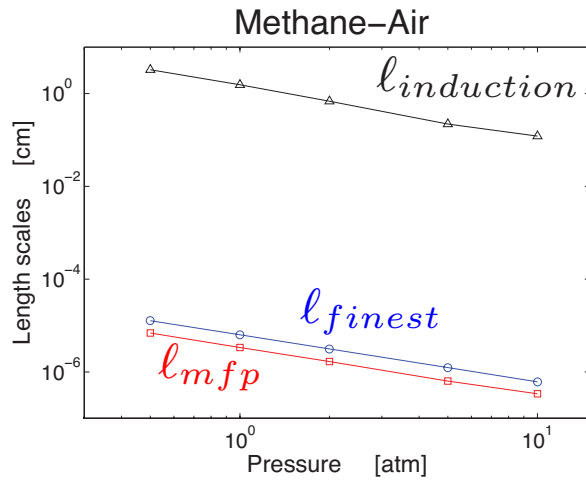
- $\ell_{mfp} = \frac{M}{\sqrt{2N}\pi d^2\rho}$ , the cutoff scale for continuum theory.



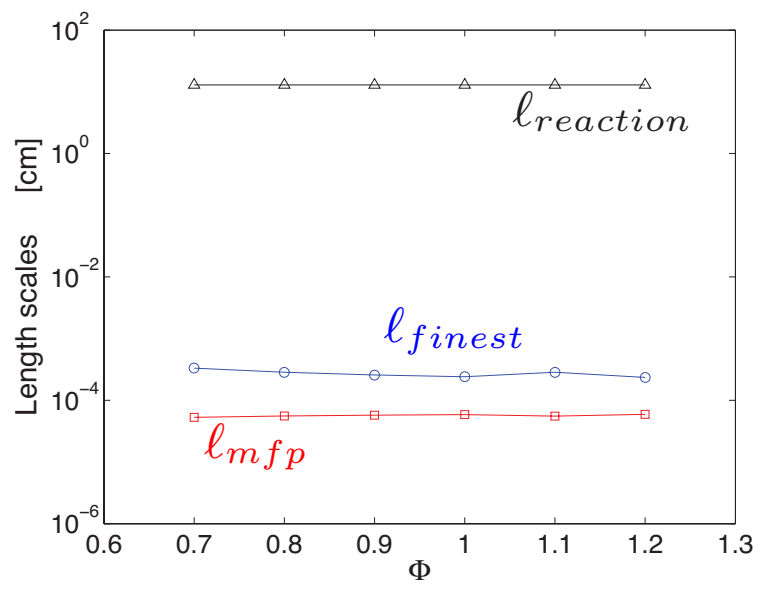
# Hydrocarbon deflagration has scales at $10^{-4}$ cm



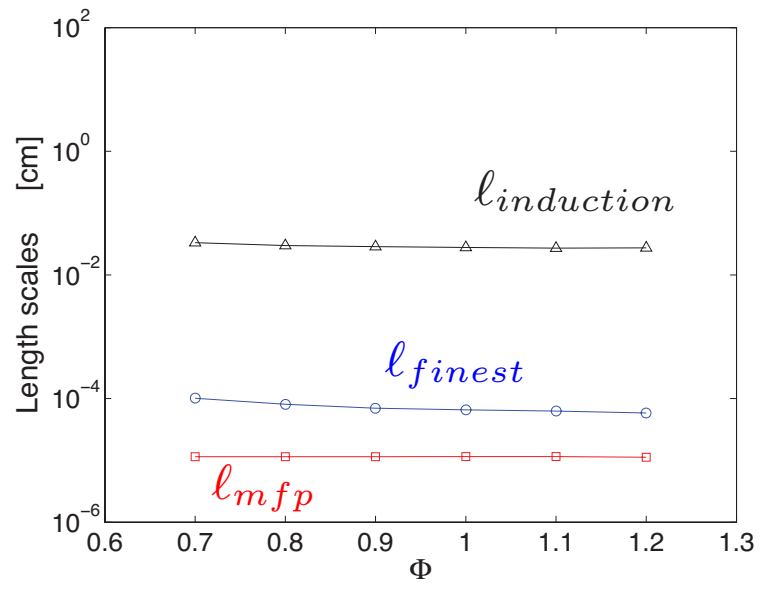
# Hydrocarbon detonation has scales at $10^{-4}$ cm



# Variable equivalence ratio gives scales at $10^{-4}$ cm



(a) Laminar premixed flame



(b) Chapman-Jouguet detonation



Independent unsteady calculations show scales are  $O(10^{-4})$  cm

For recent DNS of unsteady hydrogen-air flames...

“The domain is 4.1 mm in each of the two spatial directions. A uniform grid spacing of 4.3 microns was required to resolve the ignition fronts...”

J. H. Chen, *et al.*, “Direct numerical simulation of ignition front propagation in a constant volume with temperature inhomogeneities. I. Fundamental analysis and diagnostics,” *Combustion and Flame*, 145:128-144, 2006.

# Comparison with Other Published Results

Ref.	Mixture molar ratio	$\Delta x, (cm)$	$\ell_{finest}, (cm)$	$\ell_{mfp}, (cm)$
1	$1.26H_2 + O_2 + 3.76N_2$	$2.50 \times 10^{-2}$	$8.05 \times 10^{-4}$	$4.33 \times 10^{-5}$
2	$CH_4 + 2O_2 + 10N_2$	unknown	$6.12 \times 10^{-4}$	$4.33 \times 10^{-5}$
3	$0.59H_2 + O_2 + 3.76N_2$	$3.54 \times 10^{-2}$	$4.35 \times 10^{-5}$	$7.84 \times 10^{-6}$
4	$CH_4 + 2O_2 + 10N_2$	$1.56 \times 10^{-3}$	$2.89 \times 10^{-5}$	$6.68 \times 10^{-6}$

1. Katta V. R. and Roquemore W. M., 1995, *Combustion and Flame*, **102** (1-2), pp. 21-40.
2. Najm H. N. and Wyckoff P. S., 1997, *Combustion and Flame*, **110** (1-2), pp. 92-112.
3. Patnaik G. and Kailasanath K., 1994, *Combustion and Flame*, **99** (2), pp. 247-253.
4. Knio O. M. and Najm H. N., 2000, *Proc. Combustion Institute*, **28**, pp. 1851-1857.

## The modified equation for a model problem

$$\frac{\partial \psi}{\partial t} + a \frac{\partial \psi}{\partial x} = \nu \frac{\partial^2 \psi}{\partial x^2},$$

$$\frac{\psi_i^{n+1} - \psi_i^n}{\Delta t} + a \frac{\psi_i^n - \psi_{i-1}^n}{\Delta x} = \nu \frac{\psi_{i+1}^n - 2\psi_i^n + \psi_{i-1}^n}{\Delta x^2},$$

$$\frac{\partial \psi}{\partial t} + a \frac{\partial \psi}{\partial x} = \left( \nu + \underbrace{\frac{a\Delta x}{2} \left( 1 - \frac{a\Delta t}{\Delta x} \right)}_{\text{leading order numerical diffusion}} \right) \frac{\partial^2 \psi}{\partial x^2}$$

$$+ \underbrace{\frac{a\Delta x^2}{6} \left( -1 + \left( \frac{a\Delta t}{\Delta x} \right)^2 + 6 \frac{\nu\Delta t}{\Delta x^2} \right)}_{\text{leading order numerical dispersion}} \frac{\partial^3 \psi}{\partial x^3} + \dots$$

- Discretization-based terms alter the dynamics.
- Numerical diffusion could suppress physical instability.

- To solve for the steady structure

$$a \frac{d\psi}{dx} = \nu \frac{d^2\psi}{dx^2},$$

$$\text{Exact solution} \Rightarrow \psi = C_1 + C_2 \exp\left(\frac{ax}{\nu}\right).$$

- Analogous to what has been done in our work

$$\lambda = [0 \quad a/\nu],$$

$$\Rightarrow \ell_{finest} = \nu/a.$$

- The required grid resolution is  $\Delta x < \nu/a$ .
- This grid size guarantees that the steady parts of the dissipation and dispersion errors in the model problem are small.

## Implications for combustion

- Equilibrium quantities are insensitive to resolution of fine scales.
- Due to non-linearity, errors at **micro-scale** level may alter the **macro-scale** behavior.
- The sensitivity of results to fine scale structures is not known *a priori*.
- Lack of resolution may explain some **failures**, e.g. DDT.
- Linear stability analysis:
  - Requires the fully resolved steady state structure.
  - For one-step kinetics, *Sharpe, '03* shows failure to resolve steady structures leads to quantitative and qualitative errors in premixed laminar flame dynamics.

# Conclusions

- Verification of one-dimensional steady flames require  $10^{-4}$  *cm*-level resolution.
- Result holds for multi-dimensional unsteady flows (Chen, 2006).
- The finest length scales are fully reflective of the underlying physics and not the particular mixture, chemical kinetics mechanism, or numerical method.
- The required grid resolution can be easily estimated *a priori* by a simple mean-free-path calculation.
- Validation of steady one-dimensional flame speeds is not difficult.
- Validation of complex flame dynamics will likely require  $10^{-4}$  *cm* resolution.